29799 SW Town Center Lo Phone: 503.682.496 Web: www.ci.v	LSONVILLE OREGON Pop E, Wilsonville, OR 97070 50 Fax: 503.682.7025 vilsonville.or.us	Planni Development Final action on development application on development within 120 days in accordance wi A pre application conference is no application. Please visit the City' Pre-Application Meeting Date: Incomplete applications will not all of the required materials are	ng Division Permit Application lication or zone change is required th provisions of ORS 227.175 ormally required prior to submittal of an s website for submittal requirements
Applicant:	and a second	Authorized Representativ	ve:
Name: Remo Douglas		Name: Keith Liden	
Company West Linn-Wil	sonville School Dist.	Company, Keith Liden P	lanning Consultant
22210 SV	W Stafford Road	4012 SW/ 36th Place	
Mailing Address: <u>22210 00</u>		Mailing Address:	OP 07221
City, State, Zip: I Ualatin, C	JK 9/002	City, State, Zip: Portland,	
Phone: 503.673.7988 Fax: NA		Phone: 503.757.5501	Fax: NA
_{E-mail:} douglasr@wlwv.k12.or.us		_{E-mail:} keith.liden@gn	nail.com
Property Owner:		Property Owner's Signat	ure;
_{Name:} Same		\cap \cap	1)
		1-14	
Company:		Printed Name: Remo Dou	iglas Date: 9-16-20
Mailing Address:		Applicant's Signature: (if	different from Property Owner)
City, State, Zip:			
Phone:	Fax:		
E-mail:		Printed Name:	Date:
Site Location and Descrip	tion: 1055 SW Wilsonville Ro	ad	
Project Address if Available:			Suite/Unit
Project Location:			
Tax Map #(s): 22A	Tax Lot #(s):	OCou	nty: 🗆 Washington 📱 Clackamas
Request: Minor remodeling to the exis detached greenhouse classr	ting 86,613 sf middle school i oom; 3) New front building en	ncluding:1) 1,760 sf storage/r try & admin. offices; and 4) el	estroom addition; 2) 1,288 sf ectronic reader board sign.
Project Type: Class I 🛛	Class II 🛛 Class III 🛔		Dublic Cecility
Residential	Commercial	🗆 Industrial	Other: PUDIIC FACILITY
Application Type(s):		0	
Annexation Final Plat	Appeal Major Partition	Comp Plan Map Amend Minor Partition	Parks Plan Review Request to Modify
Plan Amendment	Imajor Farmon Planned Development	Preliminary Plat	Conditions
Request for Special Meeting	Request for Time Extension		Site Design Review
SROZ/SRIR Review	Staff Interpretation	Stage I Master Plan	□ Stage II Final Plan
Type C Tree Removal Plan	Tree Permit (B or C)	Temporary Lise	□ Variance
□ Villebois SAP	U Villebois PDP	Villebois FDP	\Box Other (describe)
Tone Man Amendment	Waiver(s)	Conditional Lice	
- Sone map runchament			Exhibit B1 DB20-0046 et sec

WOOD MIDDLE SCHOOL Stage I and II Site Design Review, Class III Sign Permit and Waiver

September 17, 2020

APPLICATION SUMMARY

For Site Design Review approval to construct an addition and detached greenhouse for Wood Middle School along with replacement of selected windows and entryways. In addition, a Class III Sign Permit and waiver is requested to install an electronic reader board on an existing monument sign.

GENERAL INFORMATION

Location

11055 SW Wilsonville Road (3S 1W, Section 22A, Tax Lot 500). Its location is shown in Figure 1.

Comprehensive Plan and Zoning Designation

The plan designation is Public, and the zoning is PF - Public Facilities.

Applicant and Owner

Remo Douglas West Linn-Wilsonville School District 22210 SW Stafford Road Tualatin, OR 97062 Phone: 503.673.7988 E-mail: douglasr@wlwv.k12.or.us

Applicant's Representatives

Keith Liden, AICP 4021 SW 36th Place Portland, OR 97221 Phone: 503.757.5501 E-mail: <u>keith.liden@gmail.com</u> Rebecca Grant Associate Director IBI Group 907 SW Harvey Milk Street Portland, OR 97205 Phone: 503.419.1606 E-mail: <u>rebecca.grant@IBIGroup.com</u>

Identification	Description
G0000	Cover Page
G1201	Site Plan
A1100	Floor Plan - Existing
A1101	Floor Plan - Proposed
A1401	Overall Roof Plan
A2201	Sector/Enlarged Elevations
A2202	Sector/Enlarged Elevations
A2203	Sector/Enlarged Elevations
A5110	New Electronic Reader Board at Existing Monument Sign
A8001	Materials Board
C1100	Existing Conditions and Demolition Plan
C1210	Preliminary Site and Utility Plan
C1230	Grading and Erosion Control Plan
E0301	Site Plan – Lighting
Attachment A	Preliminary Storm Drainage Report, Wood MS Remodel
Attachment B	Wall Mount Light Fixture Specifications
Attachment C	Reader Board Sign Specifications

Plan Sheets and Supporting Information





Source: Metro

BACKGROUND INFORMATION

Site Description

The site is developed with Wood Middle School, including an 86,613 square foot building, driveway, parking, and play fields as shown on Sheets C1100 and G1201. The entire site is 38.65 acres, and it is shared with Boones Ferry Primary School, which is located in the western portion of the property. Two driveways provide access to the property. The eastern driveway primarily serves Wood Middle School, and the western driveway serves both schools and the CREST Center.

Improvements on the property include parking, athletic fields, playgrounds, and lawn. There are two monument signs along the Wilsonville Road frontage to identify Wood Middle School and Boones Ferry Primary School to the west. A sign is located at each of the two driveway entrances to the school property. A Significant Resource Overlay Zone (SROZ) is located on the northern edge of the property (Sheet C1100).

Surrounding Area Description

The plan and zoning designations and current land use of the surrounding area are summarized in Table 1.

Table 1 Land Use Summary

Properties in the Vicinity	In	Plan	Zone	Land Use
	City?	Designation	Designation	
Subject Property				
3S 1W 22A, TL 500 (38.65	Yes	Public	PF – Public Facility	Wood Middle and
acre school site owned by				Boones Ferry Primary
school district)				Schools
Surrounding Properties				
Northwest	No	Clackamas Co	County EFU	Graham Oaks Nature
		Agriculture		Park
	Vaa	M/ilee eville	DDD Diamand	Cingle femily
East/Northeast	res	Wilsonville -	PDR – Planned	
		Residential	Residential	residences, open space
South	Voc	Wilconvillo Dublic		Single family
South	res	wilsonville - Public	City – PF, PDR	single family
				residences
Southwest	Yes	Public	PF	Graham Oaks Nature
				Park
West	No	Clackamas Co	County EFU	Graham Oaks Nature
		Agriculture		Park

PROPOSED IMPROVEMENTS

The District proposes several improvements to the middle school.

Administration Area Relocation

Relocate the administration area to the building perimeter with a secure vestibule entry. This will include new window openings to accommodate relocated offices that match existing windows. The building footprint and floor area will not change with these improvements (Sheets G1201, A1101, A2202 and A8001).

Classroom Relocation and New Makerspace Classroom

Classrooms that are displaced by the relocated administrative offices will be moved to the vacated administration offices footprint. This will include provision of a new maker space classroom (Sheet A1101). This will not affect the building floor area or the enrollment capacity of the school. The maker space is an educational support space. It is not a teaching station and will not increase capacity.

New Storage Room and Concessions

The district proposes to construct a building addition including a single occupant restroom, storage room, and concession stand near the performing arts classrooms, gymnasiums, and the track and athletic field (Sheets G1201, A1101 and A2201). This building addition will be approximately 1,760 square feet and a maximum height of 15 feet. Because it is located within a corner of the building, its front yard setback is greater than that of the existing building (Sheet G1201). As illustrated on Sheets A2201 and A8001, the finish materials will match the existing exterior.

New Instructional Greenhouse

A new instructional greenhouse of approximately 1,288 square feet is also proposed to be located southeast of the existing building and west of the existing parking lot on the east side of the property. This building addition will have a maximum height of approximately 14.5 feet with a setback of over 150 feet to the eastern property line (Sheet G1201). The base of the greenhouse will be finished with the same brick as the exterior of the middle school building (Sheet A2203).

New Rain Garden and Landscaping Restoration

To accommodate the additional stormwater runoff generated by the two building additions, new hardscaping, and utility improvements totaling 8,133 square feet, a new rain garden is proposed on the west side of the school building (Sheet C1210). The sizing and design of the rain garden is explained in the Preliminary Storm Drainage Report, Wood MS Remodel by 3J Consulting (Attachment A). In addition, disturbed landscaped areas shall be restored as indicated on Sheet C1210.

Rooftop Mechanical Equipment

The replacement of rooftop equipment is proposed. The replacement mechanical rooftop units will be in the same location as the existing units. The existing units are not screened and are not visible from the ground. The new rooftop mechanical unit on the addition will be screened and will not be visible from the ground (Sheets A1401, A2201 and A8001).

Exterior Lighting

The existing exterior lighting for the site is proposed to remain unchanged with the exception of three new exterior wall-mounted fixtures for the new storage room and concessions addition (Sheet E0301). They are intended to illuminate the new building doorways, and they will have virtually no impact on the overall exterior light levels for the school.

Although they are exempt from exterior lighting requirements, the light fixtures selected satisfy the prescriptive method described in Section 4.199 of the development code. As noted on Sheet

E0301, the fixtures will be 15 watts with the light directed downward with a 45-degree beam angle. The full specifications for the fixtures are provided with this application (Attachment B).

Monument Sign – Electronic Reader Board

The District proposes to modify the monument sign for Wood Middle School at the southeast corner of the property by replacing the existing manual reader board with an electronic reader board of the same size. The remainder of the sign is proposed to remain the same as illustrated on Sheet A5110, with an overall height of 6 feet, approximately 24 square-foot reader board, and total sign area of approximately 36 square feet. The nearest residence is over 100 feet to the east, and it is buffered by a solid fence and vegetation. Residences are also located on the south side of Wilsonville Road.

The electronic reader board sign is proposed to have the following operating characteristics:

- A design for text only that will not display graphics or animations. Text will be displayed in one color of red with a maximum potential brightness of 4,500 nits (for comparison, a home TV brightness is up to 1,500 nits), which is within the standard recommendation for brightness levels of outdoor displays (see Attachment C).
- The replacement of the existing manual reader board sign with an electronic one will allow for real-time updates to the signage outside the school, an example of how this may be helpful would be in the event of inclement weather or cancellation of scheduled events.

A waiver to the provisions of Section 4.156.06(.01) D. is requested to allow a sign capable of digitally changeable copy.

CONSISTENCY WITH THE WILSONVILLE ZONING CODE

The relevant criteria are listed followed by findings, which demonstrate that the application is consistent with the code requirements. The findings are organized to first address criteria relevant to the building additions and modifications followed by criteria related to the Class III sign waiver.

Building Improvements

4.136 PF – Public Facility Zone.

(.02) K. Uses Permitted Outright. Public schools are listed as a permitted use in the PF Zone.

(.04) Dimensional Standards. The proposed school meets the applicable standards in this section because:

- The property is over 60 acres, exceeding the minimum 1-acre lot size.
- The existing front yard setback of over 290 feet will not be affected.
- The existing rear and side yard setbacks greatly exceed the city's minimum standards, and the proposed greenhouse reduce the eastern side yard setback slightly. However, the minimum side yard setback of 10 feet will be exceeded by a distance of over 150 feet.

- The minimum street frontage is over 1,700 feet, exceeding the 75-foot minimum standard.
- The maximum height standard of 35 feet will be met by the building addition (maximum height of 15 feet) and the greenhouse (maximum height of 14.5 feet).

(.05) Off-Street Parking. In previous land use approvals, the school was found to satisfy the applicable standards in this section. The parking standards will continue to be satisfied because no change is proposed for the existing parking, and the proposed improvements will not create additional school capacity or cause an increase in staff.

(.06) Signs. The proposed monument sign modification and related waiver are addressed later in this narrative.

(.07) Corner Vision. In previous land use approvals, the school was found to satisfy the applicable standards in this section. The driveway locations and design will not be amended as part of this application. In addition, the existing monument sign will only be modified to feature an electronic reader board, and its dimensions and location will remain unchanged, retaining adequate sight distance.

(.08) B Special Regulations. This code section states that minor changes to an approved master plan, which "do not have off-site impact or increase visitor capacity may be reviewed by the Planning Director." The proposed improvements to the middle school qualify as a minor change to an approved master plan because they will not increase enrollment capacity, and they will simply improve the condition, security, and usability of the existing facilities for school programs and the general public.

4.139 Significant Resource Overlay Zone (SROZ).

The provisions of this code section are not applicable because the SROZ, which is located along the northern edge of the property, will be avoided.

4.140 Planned Development Regulations.

(.09) J. 1. Location and design are consistent with the Comprehensive Plan. Previous planning actions by the city along with previous development approvals for this site have all been completed in a manner deemed by the city to be consistent with its Comprehensive Plan and implementing ordinances.

(.09) J. 2 b. Essential government service. As an essential government service (defined in Section 4.001(256)), schools are exempt from meeting the Level of Service D requirement. A traffic impact study waiver has been requested from the City Engineer because the volume of traffic generated by the primary and middle schools will not be increased by these improvements.

4.154 General Regulations – On-site Pedestrian Access and Circulation.

(.01) On-site Pedestrian Access and Circulation. This section contains a number of standards in Subsection B, which are satisfied by the proposed improvements because:

- 1. The existing pedestrian pathway system will not be changed, and it will continue to provide the same level of connectivity and convenience.
- 2. The connections will continue to be as safe and direct as found on the site presently.
- 3. Vehicles and pedestrians will continue to be separated.
- 4. Crosswalks will be retained to allow safe and convenient locations for pedestrians to cross the internal driveway system.
- 5. The walkways will continue to be paved.
- 6. Wayfinding will continue to be clear and obvious.

4.155 Parking, Loading, and Bicycle Parking.

The existing school complex was designed in a manner consistent with the criteria of this section. The proposed improvements will not alter, reduce, or affect the existing parking, loading, or bicycle parking in any way.

4.171 Protection of Natural and Other Features.

(.02) General Terrain Preparation. This section contains a number of standards in Subsections A, B and C, which are satisfied by the proposed improvements because:

- The two work areas, which change the building coverage, are the storage/concessions addition and the detached greenhouse. To accommodate stormwater runoff associated with these new impervious areas, a new detention and treatment facility is proposed near the western building entrance. No natural features, terrain, floodplains, or similarly significant areas will be affected.
- 2. During construction, all building and other code requirements will be satisfied.
- 3. As noted above, this project will only affect small areas of existing lawn surrounding the school, and sensitive areas, trees, and other natural features will not be affected or compromised.

(.03) - (.11) Remaining Subsections. The remaining subsections are not relevant because the proposed improvements will not be located in hazard, wooded, sensitive, or culturally significant areas.

4.175 Public Safety and Crime Prevention.

The provisions of this section call for appropriate design and lighting to deter crime. The existing school complex was designed in a manner consistent with these criteria. The secure building entry is proposed to enhance the security of students, staff, and the public. Finally, the doorways for the storage, restroom, and concessions addition will have wall mounted fixtures to create safe evening conditions.

4.176 Landscaping, Screening and Buffering.

(.02) Landscaping and Screening Standards. Because the improvements are well within the 38+ acre site, the general landscaping standards are required. The standards in this section will continue to be satisfied because only a minor amount of the existing landscaping will be disturbed by the proposed storage/concessions and greenhouse additions.

(.03) Landscaped Area. The school site continues to have well over a minimum of 15% of the area devoted to landscaping.

(.04) Buffering and screening. The school building is well screened from surrounding properties by virtue of distance, fences, and existing landscaping. Also, the district proposes to use exterior materials and finishes that are consistent with the existing building exterior. The proposed improvements will have a minimal impact on the existing landscaping, and replacement landscaping is proposed for affected areas.

(.05) Sight-Obscuring Fence or Planting. This section is not relevant because this type of screening is not necessary or required.

(.06) Plant Materials. This section specifies the minimum sizes and coverage for new landscaping. This section is not relevant because only small areas of existing lawn will be affected and replaced following construction.

(.07) Installation and Maintenance. The installation requirements will be followed, and an irrigation system is currently available.

(.08) Landscaping on Corner Lots. Not applicable because this is not on a corner lot.

(.09) Landscape Plans. This section requires landscape plans. The re-landscaping is shown on the civil engineering sheets, and it will include restoration of lawn following construction. The small rain garden shall be planted according to city requirements.

(.10) Completion of Landscaping. The district shall continue to maintain landscaping as required by this section.

(.11) Street Trees Not Typically Part of Site Landscaping. This section segregates street trees from other landscaping requirements. Because no existing street trees will be affected, this section is not relevant.

(.12) Mitigation and restoration plantings. The only disturbed areas will be the small lawn areas and the new stormwater detention and treatment facility. All will be restored as shown on Sheet C1210.

4.177 Street Improvement Standards

This section is not applicable because the property currently satisfies the requirements of this section, and no changes are proposed to the Wilsonville Road frontage or the existing access.

4.179 Mixed Solid Waste and Recyclables Storage

This section is not applicable because the property currently satisfies the requirements of this section, and no changes are proposed to the current solid waste and recycling, which is all handled for both schools at Boones Ferry Primary School. Although no change is proposed to these facilities or the access to them, city staff requested that the District contact Republic Services to review the proposal and comment. This was done in August, a case number was assigned

(#110189258), and company representatives contacted the District on September 16th to review the existing facilities. It is anticipated that a response from Republic Services will be forthcoming.

4.199 Outdoor Lighting

4.199.20 Applicability. The outdoor lighting requirements are not applicable to the three exterior fixtures because they are required exit lighting for the exterior doors to the storage/concession addition. (Subsection (.02) F.).

4.300 Underground Utilities

The property currently satisfies the requirement of this section to have underground utilities. No above ground utilities are proposed.

4.400 Purpose – Site Design Review.

(.01) Discourage excessive uniformity and poor design. The school property has proven to be a significant community asset. The design of the building and site improvements will not be affected except for what is proposed in this application.

(.02) A number of objectives are noted in the purpose section. These are addressed below:

- A. Proper function. As noted above, the current site plan was approved by the city because of its appropriate and functional design. The proposed improvements simply build upon this design by retaining all of its current functionality and adding additional security.
- *B. Encourage originality, flexibility, and innovation.* The design of the school and these facility enhancements demonstrate the district's commitment to innovation, improved instructional methods, and continuing to improve the site's value to its students and the community.
- *C. Discourage drab, inharmonious developments.* The existing facility was approved by the city, and it has proven to be an excellent design, which now will be further improved with the additions and exterior upgrades and finishes.
- D. Conserve the city's beauty. The architectural integrity of the facility will be maintained by matching the architectural style and exterior finishes to be consistent with the existing school.
- *E. Promote businesses and industry.* A quality education program is the cornerstone for attracting business and industry to a community. These improvements demonstrate the district's continued commitment to provide a safe and functional facility that meets community needs.
- *F. Property values.* The proposed improvements will be well within the property and should not have any negative impact on surrounding properties or their value. In fact, the proposed improvements are supported by the community to provide schools that are safe functional, and support quality educational programs and activities.

- *G. Adequate public facilities.* School enrollment capacity is currently sufficient and these improvements will not increase that capacity. Therefore, the proposed improvements will essentially have no impact on public facilities and services because the overall use of the site will not increase.
- *H. Pleasant environments.* The existing landscaping open space on the site will be retained or enhanced, maintaining the visual appeal for the neighborhood.
- *I. Foster civic pride.* In addition to education, the school serves as a community center, fostering civic pride. In particular, these enhancements will provide improved security and educational opportunities for the community.
- *J.* Sustain comfort, health, tranquility and contentment of residents. Quality educational and recreational facilities are certainly a contributing factor to achieving this objective.

4.421 Criteria and Application of Design Standards.

(.01) Evaluation Standards. The standards of this section are addressed below:

- A. Preservation of landscape. The general appearance of the landscape will be retained, and landscaped areas within and immediately surrounding the building addition and greenhouse will be restored.
- B. Relation of proposed building to the environment. This standard is satisfied because the areas of work are a significant distance from any natural or environmentally sensitive areas.
- *C. Drives, parking and circulation.* Pedestrian, bicycle, vehicle, bus, and emergency access have been successfully accommodated by retaining separate and convenient routes for pedestrians and bicyclists on site. The proposed improvements will have no impact on circulation.
- *D. Surface water drainage.* As described in this application, the storm drainage system is designed to accommodate stormwater runoff related to the new artificial field.
- *E.* Utility service. All on-site utilities will continue to be placed underground.
- *F. Advertising features.* No advertising features are proposed. The existing and proposed reader board elements of the monument sign have been, and will continue to be, solely intended to keep the community informed regarding school activities and events.
- *G.* Special features. The proposed improvements will not affect existing special facilities on the site. As noted above, the locations of the building additions are a significant distance from any environmentally sensitive areas.

(.03) Guidance by the purpose statement. The purpose statement in Section 4.400 is also used to evaluate development proposals. The purpose statement and related objectives are addressed above.

4.430 Mixed Solid Waste and Recycling Areas.

The standards of this section are not relevant because these facilities have been previously approved by the city, and no changes are proposed. Waste and recycling are handled for both schools in one shared location at Boones Ferry Primary School. The existing driveway and circulation system will not be modified or affected in any way by the proposed improvements. The waste hauler will continue to have appropriate access.

4.450 Installation of Landscaping.

The proposed landscaping associated with the rain garden and replacement lawn following construction shall be installed subject to city approval. The District has demonstrated a long-standing commitment to properly maintain its facilities, including landscaping. This level of maintenance shall continue.

Class III Sign Waiver

4.156 Signs

4.156.02(.06) Class III Sign Permits. The city staff indicated that because an electronic reader board sign is not permitted, Section 4.156.02(.06) Class III Sign Permit applies to this application because approval of a waiver is required.

4.156.02(.05) E. This section contains three criteria that must be satisfied:

- 1. The proposed signage is compatible with surrounding developments or uses. The modified monument sign continues to be consistent with the original design approved by the city. It will enhance daytime identification of school events and notices in a manner that will continue to be complementary to the building's architecture and exterior finish materials. Other than the replacement of the manual reader board with an electronic one, the materials and the finish of the sign will remain as it is today.
- 2. The proposed signage will not create a nuisance. The sign will continue to complement the materials and colors of the school building façade. Because the sign will be a significant distance from any nearby residences, it will have no detrimental impact on surrounding properties.
- 3. Pay special attention to the interface between signs and other site elements. The Wood Middle School and Boones Ferry Primary School campus landscaping and signs were carefully designed by the District and approved by the DRB. The proposed modified monument sign will continue to be consistent with design and location of the original.

4.156.02(.08) A. Waivers

As noted above, the reader board portion of the existing sign is proposed to be replaced with an electronic changeable copy sign. This section lists four criteria that must be satisfied to receive a waiver:

- 1. Improved sign design and functionality. The sign design and location will be very similar to the previously approved monument sign. The only difference is the replacement of the manual reader board with an electronic one. The electronic display offers significant advantages by allowing easy message changes and regulation of the sign's operation.
- 2. Signs that are more compatible and complementary than signs allowed without the waiver. The sign design and location will remain unchanged. The electronic reader board display will have a similar visual appearance to the previously approved manual reader board backlit display. It will not have graphics or flashing displays of any kind.
- 3. The waiver will result in a sign or signs that improve, or at least do not negatively impact, public safety, especially traffic safety. The current sign location will be retained, allowing for proper visibility near the intersection of the parking lot driveway and Wilsonville Road. As noted above, the electronic display will not be overly bright, animated, or distracting in any way that could compromise traffic safety.
- 4. Sign content is not being considered when determining whether or not to grant a waiver. The sign content will obviously change with each school announcement. The primary consideration should be the proposed absence of any graphics or animation (proposed reader board will not even have this capability), which could become detrimental to surrounding properties or traffic safety.

CONCLUSION

The proposed improvements satisfy all of the relevant criteria for Site Design Review and sign waiver approval as demonstrated above.



First American Title Insurance Company of Oregon

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		Prepared By:		
		Customer Service Department		
1		1700 SW Fourth Avenue - Portland, Oregon 97201-551		
		Phone: (503) 222-3651 Fax: (503) 790-7872		
	OWNERSHIP IN	FORMATION		
Owner	West Linn-Wils Sch Dist#3j	Ref Parcel Number : R31W22A 00500 T: 03S R: 01W S: 22 Q: 253 Parcel Number : 00817272		
CoOwner Site 4.1.1				
Sile Address	11055 SW Wilsonville Rd Wilsonville 97070			
Mail Adaress	11055 SW Wilsonville Rd Wilsonville Or 97070			
Telephone	: Owner: 503-682-0101 Tenant:	County : Clackamas (OR)		
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Subdivision/Plat	s our schools	Total : \$4,631,940		
Veighborhood Cd	- W/575	% Improved : 94		
Land Use	401 Treat Treat La 11	98-99 Taxes		
legal	NZA WOOD MEDDIE 2000	Exempt Amount: \$4,631,940		
	OPD 2560 1070 FADLAUGE 2 710 116694	Exempt Type : Other		
	1 1 70	Levy Code : 003023		
	1-1-79	Millage Rate : 17.2306		
	PROPERTY CHARA	CTERISTICS		
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athrooms :	Ist Floor SF	Stories :		
ireplace :	Above Ground SE	Garage SF :		
eat Type :	Upper Finished SF	Lot Acres : 19.24		
terior Material:	Unfin Unner Ston	Lot SF : 838,094		
cterior Finish :	Upper Total SF	Year Built : 1980		
	Finished SF	Year Appraised : 1995		
oor Cover	Basement Fin SF	Appraisal Area : 5		
oor Cover		School District : 003		
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This title information has been furnished, without charge, in conformance with the guidelines approved by the State of Oregon Insurance Commissioner. The Insurance Division cautions intermediaries that this service is designed to benefit the ultimate insureds. Indiscriminate use only benefiting intermediaries will not be permitted. Said services may be discontinued. No liability is assumed for any errors in this report.





AGREEMENT

THIS AGREEMENT made and entered into this <u>7th</u> day of <u>February</u>, 1979, by and between ROBERT STETZEL. hereinafter called "Seller" and WEST LINN SCHOOL DISTRICT NO. 3 J, CLACKAMAS COUNTY, hereinafter called "Buyer".

The parties agree as follows:

SALE AND DESCRIPTION:

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Seller agrees to sell and Buyer agrees to purchase the following described real property located in Clackamas County, Oregon:

See Exhibit "A" attached hereto and incorporated herein by this reference.

PRICE AND TERMS:

The purchase price of the property, which Buyer agrees to pay is \$161,616 payable as follows:

(1) The sum of \$2,000 which has previously been paid as option money.

(2) The sum of \$44,616 which is paid upon execution hereof.

(3) The remaining balance of \$115,000 shall; be paid in annual installments of not less than \$23,000 each; plus interest at the rate of seven percent (7%) per annum on the unpaid balances, the first of such installments to be paid on the 16th day of January, 1980, and subsequent installments to be paid annually until the entire purchase price,

Page 1. AGREEMENT

BCARD, CALDWELL, CARNING, BOWERMAR & SCHULTE A PROFESSIONAL CORMONATION ATTOMICTS AT LAW P 0 BOY 647 - 710 CENTE STREET OREGON CITY CREEDN

79 5357

including both principal and interest, is paid in full. The entire purchase price may be paid at any time.

TAXES AND OTHER PUBLIC CHARGES:

Taxes for the current tax year shall be prorated as of the date of this agreement. Buyer agrees to pay and assume all future public liens, charges, taxes and assessments hereafter made upon said premises.

POSSESSION:

Buyer shall have the right to the possession of the foregoing premises as of the date of this agreement. Seller shall have the right to cultivate and remove any growing crops upon the premises to and including the 15th day of July, 1979.

CONVEYANCES:

Upon the payment of the entire purchase price of the property as provided herein and performance by the Buyer of all of the other terms, conditions and provisions hereof, Seller shall forthwith execute and deliver to Buyer a warranty deed conveying the property aforesaid to Buyer, Buyer's heirs, successors, or assigns forever, free and clear of all liens and encumbrances except those now of record and those placed upon the property or suffered by the Buyer subsequent to the date of this agreement.

TITLE INSURANCE:

Seller agrees, at Seller's own expense and within ten (10) days from the date of this agreement, to furnish unto

Page 2. AGREEMENT

HIBBARD, CALDWELL, CABRING, BOREWAR & KUUL A PROFESSIONAL CORPORATION ATTORNEY AT LAW P D PO3 467 - 7HD CENTER STREET OREGON CITY ORTGON the Buyer, a Purchaser's policy of title insurance in an amount equal to the purchase price showing marketable title in and to said premises in the Seller as of the date of this agreement save and except the usual printed exceptions and building and zoning restrictions.

ENTIRE AGREEMENT:

This written agreement constitutes the entire agreement between the parties relating to the subject matter hereof. It supersedes prior memoranda, earnest money agreements, options and all other prior documents made by the parties in connection with the transaction described herein. All oral agreements and understandings of the parties respecting the subject matter of the agreement have been integrated herein. It is the intention of the parties that no other agreement, written or oral, concerning the subject matter of this agreement, shall be effective nor binding upon either Seller or Buyer unless set forth herein or specifically referred to herein.

DEFAULT AND FORECLOSURE:

In the event the Buyer shall fail to perform any of the terms of this agreement, time of payment and performance being of the essence, the Seller shall, at Seller's option, subject to the requirements of notice as herein provided, have the following rights:

(a) To foreclose this agreement by strict foreclosure;(b) To declare the full unpaid balance of the purchaseprice immediately due and payable;

Page 3. AGREEMENT NIBBARD, CALDWILL CANNING, BOWTPHAR & SCHULS A PROFESSIONAL CORPORATION ATTORNETS AT LAW P. O. BOD SAF - THO CHIFF STREET (c) To specifically enforce the terms of this agreement by suit in equity;

Buyer shall not be deemed in default for failure to perform any covenant or condition of this agreement, other than the failure to make payments as provided for herein, until notice of said default has been given by Seller to Buyer and Buyer shall have failed to remedy said default within thirty (30) days after the giving of the notice.

If the Buyer shall fail to make payments as herein provided and said failure shall continue for more than thirty (30) days after the payment becomes due, Buyer shall be deemed in default and Seller shall not be obligated to give notice to Buyer of a declaration of said default.

ATTORNEYS FEES:

In the event suit or action shall be brought by either of the parties hereto for the enforcement of any of the covenants or conditions on the part of either of the parties to be kept or performed, or in case suit or action is instituted by the Seller to foreclose this agreement, the unsuccessful party agrees to pay to the successful party in such litigation, such sum as the court may adjudge reasonable as attorneys fees to be allowed the successful party in such suit or action, including any appeal therefrom.

NOTICES:

Notice for all the purposes of this agreement shall be deemed to have been given by the deposit in the mails of a

> ESSIONAL COMPONAT ATTOMALS AT LAM 847 - 210 CENTRA AT MEGDA CITA DECOM

Page 4. AGREEMENT

certified letter containing said notice and addressed to 716 Uine Mugle du., Hurder Marker Robert Stetzel, 11265 S.W. Wilsonville Road, Wilsonville, 91/15 Oregon 97070 with respect to the Seller, and to West Linn School District, Administration Building, West Linn, Oregon 97068 with respect to the Buyer.

WAIVER OF PROVISIONS:

The failure on the part of the Seller at any time to require performance by the Buyer of any provisions hereof shall, in no way, affect Seller's right hereunder to enforce the same nor shall any waiver by the said Seller of any breach of any provisions hereof be held to be a waiver of any succeeding breach of any provision as a waiver of the provision itself.

UNTIL A CHANGE IS REQUESTED, ALL TAX STATEMENTS SHALL BE SENT TO THE FOLLOWING ADDRESS: West Linn School District, Administration Building, West Linn, Oregon 97068.

IN WITNESS WHEREOF the parties have hereunto set their hands the day and year first hereinabove written

SELLER:

Stetz Robert

BUYER:

WEST LINN SCHOOL DISTRICT NO. 3 J, CLACKAMAS COUNTY

Superintendent

Page 5. AGREEMENT

BISD CALDWILL CANNING BOWISHAN & SCHUL A PROFISSIONAL COMPONATION Attronets at Law P 0 BOI #87 - The Chain Street One Can Scity Detgon

STATE OF OREGON SS County of Clarks

Samming

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On this 1 day of Junuary, 1979, pers appeared ROBERT STETZEL and acknowledged the foregoing , 19**79, personally** instrument to be his voluntary act and deed.

Notary Public for Oregon

My commission expires: 3

1 1940 STATE OF OREGON SS County of Clarkamas

lineary, 1979, personally On this 1 day of who, being duly sworn appeared Coal <u>/μ</u> elsus says that he is the Superintendent of WEST LINN SCHOOL DISTRICT NO. 3 J, CLACKAMAS COUNTY, and that said instrument was signed and sealed by authority of its Board of Education; and acknowledged said instrument to be its voluntary act and deed.

Public for Oregon Notary My commission expires: 2/28/8

Tel ma

AFTER RECORDING, RETURN TO: Title Insurance Company of Oregon Escrow#443485 cg

Page 6. AGREEMENT



Order No. 443485

EXHIBIT "A"

Beginning at the section corner 15, 16, 21 and 22, Township 3 South, Range 1 West, W.M. in County of Clackamas, State of Oregon, and running thence North 89° 48' East 2790.00 feet along the North line of Section 22 to a point; thence feet to the true point of beginning of the parcel herein described; thence North 81° 00' East 370.00 feet; thence South 32° 55' East 1110.00 feet to a North 81° 00' East 370.00 feet; thence South 32° 55' East 1110.00 feet to a North 81° 00' East are set of the Wilsonville Highway; thence South 52° point on the Northwesterly line of the Wilsonville Highway a distance of 45' West along the Northwesterly line of said Wilsonville Highway a distance of 794 feet to the most Easterly corner of that certain tract of land as described in deed to Robert A Stetzel, et ux recorded April 14, 1966 in Book 672, Page 129 Deed Records; thence North 32° 55' West along the Northeasterly line of said Stetzel tract a distance of 620 feet, more or less, to a point of intersection of said Northeasterly line with the Easterly line of that certain intersection of said Northeasterly line with the Easterly line of that certain tract of land owned by the State of Oregon, thence North along said Easterly line a distance of 826 feet, more or less, to the true point of beginning.



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STATE OF OREGON) County of Clackman) *1. 1. George D. Poppen, County Clerk

0116

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FORM Ne. 633-WATTANTY DITO 150 KNOW ALL MEN BY THESE PRESENTS, That CEMMARD MATZEN and BLENDA W. hereinalter called the grantor, -(\$10.00) - Dollars, to grantor paid by ROBERT A. STETZEL and MELLIN R. STETZEL, hus nd wife. called the grantee. , hereins does hereby givent, bargain, sell and convey unto the said grantee and grantee's house successors and assigns, that certain real property, with the tenements, hereditaments and appurtenances thereunto belonging or appertaining, situated in the County of Clackaras and State of Oregon, described Beginning at the sontion corner 15, 16, 21 and 22, Township 3 South, Range 1 West, W.M. and running thence N 89° 48' E 2790.00 fect along the North line of Section 22 to a point; thence S 26° 00' E 106.32 feet to a point; thence N 61° 00' E 140.00 feet to the true point of beginning of the parcel horein described; thence 3 81° 00' E 370.00 feet; thence S 32° 55' E 1110.00 feet to a point on the northwesterly line of the Wilsonville Mighway; thence Southwesterly 1214.00 feet along the northwesterly line of Wilsonville Fighway; thence southwasterly line of property owned by the State of Wilsonville Fighway to a point on the easterly line of property owned by the State of Oregon; thence North 1606.00 feet along the easterly line of said State of Oregon property to the true point of beginning of the parcel herein described. To Have and to Hold the above described and granted premises unto the said grantee and grantes's heirs, successors and assigns forever. And said grantor hereby covenants to and with said grantee and grantee's heirs, successors and assigns, that grantor is lawfully seized in fee simple of the above granted premises, free from all encumbrances EXCEPT SUBJECT TO ensements, conditions and restrictions of public record; zoning and use restrictions; rights of the public in any portion within roads, and that grantor will warrant and forever defend the above granted premises and every part and parcel thereof against the lawful claims and demands of all persons whomsoever. In construing this deed and where the context so requires, the singular includes the plural. , 19 65 ... day of ... Feb. WITNESS grantor's hand and seal this 9 - Juchard Wie Jun (SEAL) Flenda W Firstaver (SEAL) (SEAL) (SEAL) Personally appeared the above named Gerhard Matzon and Flenda W. Matzen, husband and wife (ORS 93 490) STATE OF OREGON, County of Clackamas and acknowledged the loregoing instrument to be thoir voluntary act and deed. Before me 1.18 Notary Public for Oregon My commission expires ay Commission Common May 16, 1907 (SEAL) WARRANTY DEED Gerhard Matzon, ot ux 5280 τo -t. A. Stetzel, ot ux 0 RECORDING RETURN TO OREGON Gaorge of No 10 78 52808

AMERIC

First American Title Insurance Company of Oregon

Clackamas (OR) ared For: Prepared By: Customer Service Department 1700 SW Fourth Avenue - Portland, Oregon 97201-5512 Phone: (503) 222-3651 Fax: (503) 790-7872 **OWNERSHIP INFORMATION** Hull Joan B Ref Parcel Number : R31W22A 00600 T: 03S R: 01W S: 22 Q: 253 ·ess 11265 SW Wilsonville Rd Wilsonville 97070 Parcel Number :00817281 11265 SW Wilsonville Rd Wilsonville Or 97070 *ress* : Owner: 503-682-0397 е Tenant: County : Clackamas (OR) Current ingo for Parker/Hull triangle piece by wood 4.14 m SALES AND LOAN INFORMATION ·ed : 03/16/93 Loan Amount : 93-16914 t# Lender е Loan Type : Quit Claim P Interest Rate : 100 Vesting Type **PROPERTY DESCRIPTION** ASSESSMENT AND TAX INFORMATION 2 & Grid : 744 J3 Land : \$50,180 : Tract: 227.01 Block: 5 Structure \$162,460 ient Type : 141 Sgl Family,R1-4,1-Story \$212,640 Total n/Plat % Improved : 76 hood Cd : W575 98-99 Taxes : \$2,653.34 541 Agr, Farm Land, Improved, Unzoned Exempt Amount : : UNZONED FARM - POTENTIAL ADDITIONAL Exempt Type TAX LIABILITY R V SHORT DLC TL Levv Code : 003023 : 1-3-1 ORD #16694 ORD 2560 MSD 1-... Millage Rate : 17.2306 **PROPERTY CHARACTERISTICS** : 3 Building SF : 2,370 Stories :1 : 2.00 1st Floor SF S : 2.370 Garage SF : Backed Above Ground SF : 2,370 Lot Acres : 2.99 : Forced Air-Oil Upper Finished SF Lot SF : 130,244 'aterial: Drywall Unfin Upper Story Year Built : 1966 *inish* : Tongue\groove Upper Total SF Year Appraised 1995 : Carpet er Finished SF : 2.370 Appraisal Area 5 Wood Shake Med Basement Fin SF School District : 003 Gable Basement Unfin SF е Utility District : Concrete n **Basement** Total SF

This title information has been furnished, without charge, in conformance with the guidelines approved by the State of Oregon Insurance Commissioner. The Insurance Division cautions intermediaries that this service is designed to benefit the ultimate insureds. Indiscriminate use only benefiting intermediaries will not be permitted. Said services may be discontinued. No liability is assumed for any errors in this report.





TIL-OUITCIAIN DIED Individual a Corporate ----and manager of these が大学 QUITCLAIM DEED AUSTIN L. HULL KNOW ALL MEN BY THESE PRESENTS, That ..., hereinalter called grantor, Ior tooAnnidention hereinalter stated, does hereinisgifterate and quitelaim unto at a said that the design of the same Colling and hereinalter called grantee, and unto grantee's heirs, successors and assigns all of the granter's right, title and interest in that certain real property with the tenements, hereditaments and appurtenances thereunto belouging or in any-wise appertaining, situated in the County of Clackamas, State of Oregon, described as follows, to-wit: A tract of land in Section 22, T.3S., R.1W., W.M., in the County of Clackamas, State of Oregon, described as follows: Beginning at the most southerly corner of that certain tract of land described in that Contract of Sale to Robert A. Stetzel, et ux, recorded January 20, 1965, in Book 652, Page 16, Deed Records, Clackamas County, Oregon, said point being on the northwesterly line of the Wilsonville Highway; thence Northeasterly along the northwesterly line of said Wilsonville Highway and the boundary line of said Stetzel tract, 420.0 feel; thence North 32 degrees 55' West parallel to the easterly line of said Stetzel tract, 620.0 feet, more or less, to a point of intersection with the westerly line of said Stetzel tract; thence Southerly along the easterly line of said Stetzel tract, 780.0 feet, more or less, to the point of beginning. OF SPACE INSUFFICIENT, CONSUME DISCRIPTION ON REVERSE SIDE To Have and to Hold the same unto the said granten and grantee's heirs, successors and assigns lorever. The true and actual consideration paid for this trensfer, stated in terms of dollars, is \$ Howor notical counidatestin 1400 nte of or includes other property or value fiven or prov ul interior Part of th tine consideration (indicate which). (The sentence between the symbols O, il not applicable, should be deleted, See ORS 93.030.) In construing this deed and where the context so requires, the singular includes the plural and all grammatical changes shall be implied to make the provisions hereat apply equally to corporations and to individuals. full CAROLYN J. WILLCUTS Forschally Propresed NYTARY PUBLIC ORECON MY COMMISSION EXPIRES OCT 24, 1995 WY COMMISSION EXPIRES OCT 24, 1995 (if sectured by a corporation, affin corporate seal) March 3 13 93 STATE OF OREGON, Countrol Marion Feb 8 1993. Personally appeared Donald L. HUII Personally appeared the above named Marilyn Johansen - is she h for himself and not one for the other president and that the latter is the and acknowledged the foregoing instrument to be her NOTIONAL DEPOCHAMAGE OF DOGUE NOTIONAL DEPOCHAMAGE OF DOGUE NOTIONAL PULLING DECAM NOTIONAL PULLING DOTORS 11 13 - 95 NY COMMICSION EXPRISES 013, 1295 volumary act and deed. Hise to the said harrament and signed and and each intthey acknowledged sold initiary to be its voluntary act and deed. and Belove and K. Keen (SEAL) Public for Orea Notary Public for Oregon My co AUSTIN L. HULL bittecov. ANGELA KAKEERE F HULL AND ADDACSA NOTARY PUBLIC OREGON My Commission Expires , Willight the willin instrunopalo JOAN B. HULL 11265 SW WILSONVILLE RD. ment was received for record on the WILSONVILLE, OR 97070 PPACE RESERVED FOR. ------JOAN 8. HULL. instrument/microfilm No. . 11265 SW WILSONVILLE RO. Record of Deeds of suid county. WILSONVILLE, OR 97070 Witness my hand and seal of County affixed. Until a choose a post the statements shall be sent to the following address 11265 SW WILSONVILLE RD. NAME HTLE WILSONVILLE, OR 97070 Br Deputy ---alter a talatation of 93 16914



ATTACHMENT A Preliminary Storm Report

PRELIMINARY STORM DRAINAGE REPORT

Wood MS Remodel 11055 SW Wilsonville Road Wilsonville, OR 97070

Planning DB No.: TBD

August 12, 2020

Prepared For:

West Linn-Wilsonville School District (WLWV) 22210 SW Stafford Rd Tualatin, OR 97062



Prepared By:

3J Consulting, Inc. 9600 SW Nimbus Avenue, Suite 100 Beaverton, Oregon 97008 Project No: 20617 PJP

COMMUNITY PLANNING ENGINEERING | WATER RESOURCES

TABLE OF CONTENTS

DESIGNER'S CERTIFICATION & STATEMENT1	
EXECUTIVE SUMMARY2	
PROJECT DESCRIPTION	í
EXISTING CONDITIONS	5
Existing Site	5
Existing Drainage3	6
Flood Map4	•
Soils4	,
Infiltration4	,
Existing Basin Areas	•
Existing Hydrology5	•
DEVELOPED CONDITIONS)
Developed Site & Drainage5	ł
Developed Basin Areas5	J
Developed Hydrology5)
Stormwater Management Strategy5	
Downstream Analysis	•
Conveyance Analysis7	
CONCLUSIONS	į
REFERENCES	j
TECHNICAL APPENDIX9	ł

LIST OF FIGURES

Figure 1	- Vicinity Ma	p	3
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LIST OF TABLES

Table 1 – Onsite Soils	4
Table 2 – Existing Basin Areas	4
Table 3 – Developed Basin Areas	5
Table 4 – Downstream Analysis Basin Areas	7

DESIGNER'S CERTIFICATION & STATEMENT

I hereby certify that this Preliminary Storm Drainage Report for Wood MS Remodel has been prepared by me or under my supervision and meets minimum standards of the City of Wilsonville and normal standards of engineering practice. I hereby acknowledge and agree that the jurisdiction does not and will not assume liability for the sufficiency, suitability, or performance of drainage facilities designed by me.



EXECUTIVE SUMMARY

The project site is located at 11055 SW Wilsonville Road, at the existing Wood Middle School in Wilsonville, Oregon (taxlot 31W22A 00500), and falls within the jurisdiction of the City of Wilsonville. The West Linn-Wilsonville School District (WLWV) proposes a 1,785-sf building addition, a 1,290-sf greenhouse, appurtenant hardscaping and utility improvements. In total, the project results in the creation or modification of 8,133 sf of impervious area.

Per the City of Wilsonville's Stormwater & Surface Water Standards (2015), this project is required to implement stormwater management facilities and a Rain Garden is proposed to meet compliance. This facility will manage an equivalent amount of impervious area elsewhere onsite. The Rain Garden was sized using the BMP Sizing Tool. An Operations & Maintenance Plan will be included with the Final Storm Drainage Report.

A Downstream Analysis was performed to demonstrate that the downstream system has capacity for the project site's runoff during the 25-yr storm event.

A Conveyance Analysis of the onsite storm drain system will be included with the Final Storm Drainage Report.

The purpose of this report is to accomplish the following:

- Describe existing and developed site conditions;
- Describe the proposed stormwater management strategy; and,
- Demonstrate compliance with the City of Wilsonville Stormwater & Surface Water Standards (2015).



PROJECT DESCRIPTION

The project site is located at 11055 SW Wilsonville Road, at the existing Wood Middle School in Wilsonville, Oregon (taxlot 31W22A 00500), and falls within the jurisdiction of the City of Wilsonville. The West Linn-Wilsonville School District (WLWV) proposes a 1,785-sf building addition, a 1,290-sf greenhouse, appurtenant hardscaping and utility improvements. In total, the project results in the creation or modification of 8,133 sf of impervious area. The project's current land use as a school will remain unchanged.

Per the City of Wilsonville's Stormwater & Surface Water Standards (2015), stormwater management facilities are required when a project creates or replaces more than 5,000 sf of impervious area. Due to the disturbed areas being distributed across the property, a Rain Garden is proposed to treat and manage runoff from an equivalent or greater amount of impervious area elsewhere onsite. The facility was sized via the WES BMP Sizing Tool and will be located near the greenhouse on the west side of the school and will manage runoff from a nearby parking area.



Figure 1 - Vicinity Map

EXISTING CONDITIONS

Existing Site

The existing site is Inza R. Woods Middle School.

Existing Drainage

The site generally drains from south to north with elevations ranging from 173-181 feet. Surface runoff drains to two main branches of an existing onsite storm drain system. Runoff from the property discharges at


multiple locations; however, the point of discharge relevant to this project is within Arrowhead Creek along the northern boundary of the property (See Technical Appendix: Exhibits – Developed Conditions).

The east portion of the site drains to conveyances, which flow to a Stormceptor Manhole for treatment. The southwest portion of the site drains to conveyances, which discharge to an onsite Dry Pond. Both the Stormceptor and Dry Pond discharge to an existing flow control manhole which releases flow to Arrowhead Creek to the north. Arrowhead Creek is natural and unlined.

Emergency Overflow

The existing onsite pond and flow control manhole are close to the property's local low point. In emergency situations, large flows would overtop the northern bank of pond and discharge directly into Arrowhead Creek. The crest of the pond is at elevation 173 and the school's finish floor elevation is at least 176.3. This project will not alter this emergency overflow route.

Flood Map

The site is located within Zone X (unshaded) per flood insurance rate map (FIRM) community-panel number 41005C0241D (See Technical Appendix: Exhibits – National Flood Hazard Layer FIRMette). FEMA's definition of Zone X (un-shaded) is an area of minimal flood hazard.

Soils

The soil types, as classified by the NRCS Web Soil Survey, are identified in Table 1 (See Technical Appendix: Exhibits – Hydrologic Soil Group).

Soil Type	Hydrologic Soil Group	Site Coverage (%)		
Aloha Silt Loam	C/D	92.8		
Dayton Silt Loam	D	7.2		

Table 1 – Onsite Soils

A majority of the site is underlain with C/D soils and the areas of coinciding with D soils are predominantly impervious are occupied by the onsite pond. Therefore, for simplicity, the site is modeled assuming C soils.

Infiltration

Infiltration testing was not performed because onsite soils are C and D types, which are unlikely to have measurable infiltration rates. Onsite infiltration rates are assumed to be 0 in/hr and the proposed stormwater facility will be lined.

Existing Basin Areas

The project will modify several areas on the property. Table 2 below quantifies the existing pervious and impervious areas affected by this project.

Existing Basin Areas	Area (sf)
Pervious	3,314
Impervious	6,401
Total Disturbed	9,715
	• •

Table 2 – Existing Basin Areas

The project also proposes trenching in pervious areas in which the cover will be replaced in kind; therefore, these pervious areas are not included in the total disturbed area.



Existing Hydrology

In compliance with City Standards, XPSTORM was used to perform the Santa Barbara Urban Hydrograph (SBUH) method to deterring the peak runoff rate for the 25-yr design storm (4.0" falling in 24 hours; NRCS Type IA distribution).

Curve Numbers

Runoff curve numbers (CN) were selected from Table 2-2 of the TR-55 Manual, which depend of land cover type and hydrologic soil group. CNs for pervious and impervious areas were determined to be 74 (lawn in good conditions, C soils) and 98, respectively. See Technical Appendix: Exhibits – CN.

Time of Concentration

Since the disturbed area is distributed and cumulatively small, the time of concentration was assumed to be 5 minutes.

25-yr Runoff Rate

The 25-yr peak runoff rate was evaluated to be 0.163 cfs (See Technical Appendix: Hydrographs – Existing).

DEVELOPED CONDITIONS

Developed Site & Drainage

The project proposes a building addition, greenhouse, Rain Garden, utility improvements, hardscaping and landscaping. A majority of the property will remain in place; general drainage patterns and the discharge location are maintained.

Developed Basin Areas

Table 3 below quantifies the developed pervious and impervious areas for this project.

Developed Basin Areas	Area (sf)
Pervious	1,582
Impervious	8,133
Total Disturbed	9,715

Table 3 - Developed Basin Areas

Developed Hydrology

The methodology and parameters used for determining the existing 25-yr peak runoff rate still apply, with basins areas only changing. The developed 25-yr peak runoff rate was evaluated to be 0.188 cfs (See Technical Appendix: Hydrographs – Developed).

Stormwater Management Strategy

Design Guidelines & Methodology

The City of Wilsonville requires the implementation of Low Impact Design (LID) facilities to manage runoff to accomplish the following:

- Treatment Water quality facilities shall be designed to capture and treat 80% of the average annual runoff volume to the MEP with the goal of 70% total suspended soils (TSS) removal.
- Flow Control The developed flow-duration curve shall be less than or equal to the predeveloped flow-duration curve for all storm events between the 42% of the 2-yr and 10-yr events.

To comply with these requirements, the BMP Sizing Tool was used to determine the minimum dimensions for the proposed BMP.



Proposed Facility

As mentioned previously, the project disturbs multiple areas on the property. To comply with City stormwater management requirements, a Filtration Rain Garden is proposed on the west side of the building to treat a contributing impervious area (CIA) greater than or equal to the cumulative impervious area created or modified by this project. The CIA to the Rain Garden is 9,434 sf, which exceeds the required 8,133 sf. The latter area requires a Rain Garden with a minimum area of 446 sf. The planned Rain Garden area is 480 sf (See Technical Appendix: WES BMP Sizing Report). For Flow Control compliance, the Rain Garden will have a low flow orifice with a 0.8" diameter.

Operations & Maintenance Plan

An Operations & Maintenance (O&M) Plan will be included with the Final Storm Drainage Report.

Downstream Analysis

Design Guidelines

Per City Standards, a downstream analysis must be performed to verify that the downstream system has the capacity to convey the 25-yr design storm. The proposed development area is 9,715 sf; the total contributing drainage area to the discharge location is 347,497 sf. As a result, the development area constitutes approximately 3% of the total contributing drainage area. Per City Standards, the downstream analysis will continue for one-quarter mile downstream of this projects discharge location (See Technical Appendix: Downstream Analysis – Wilsonville GIS).

Model Overview

In compliance with City Standards, XPSTORM was used to perform the Santa Barbara Urban Hydrograph (SBUH) method and dynamic wave routing for the hydrologic and hydraulic analyses, respectively. The downstream system was analyzed for the 25-yr design storm (4.0" falling in 24 hours; NRCS Type IA).

Basin Overview

Seven (7) basins, denoted as Basins A through G, were delineated for the Downstream Analysis (See Technical Appendix: Downstream Analysis – Basin Exhibit). This project affects Basin A & B, specifically increasing the impervious areas of Basin A and B by 72 sf (0.002 ac) and 1660 sf (0.04 ac), respectively.

Basins C, D and F are undeveloped, consisting of areas within the Graham Oaks Nature Park and the Park at Merryfield.

Basins E & G consists of single-family residential developments, as designated on wilsonvillemaps.com, which concurs with the current Wilsonville Comprehensive Plan. The minimum lot size measured within each basin was 7,500 sf (0.17 ac). For conservativeness, Basins E & G were modeled with an assumed impervious coverage of 65% (per the TR-55 Manual), which is typically associated with 0.125-ac lots (higher density).

Table 4 below outlines the hydrologic characteristics for each basin.



Basin	Total Area (ac)	lmp. Area (ac)	Pervious Area (ac)	Pervious CN	Tc (min)
A	4.18	3.08	1.10	79	5
В	3.80	2.67	1.14	79	5
С	102.7	0.00	102.7	73	75
D	2.68	0.00	2.68	73	35
E	5.44	3.53	1.90	78	5
F	9.39	0.00	9.39	73	46
G	23.94	15.56	8.38	73	15

Table 4 – Downstream Analysis Basin Areas

The curve numbers (CN) and times of concentration (Tc) are explained in the following subsections.

Curve Numbers

Runoff curve numbers (CN) were selected from Table 2-2 of the TR-55 Manual, which depend of land cover type and hydrologic soil group. The basins are underlain by soil types B, C and D (See Technical Appendix: Downstream Analysis – HSG). The basins have land cover types varying from lawn, woods-grass combination or woods. When basins are underlain by more than one soil type, a spatially weighted average CN was evaluated.

Despite the soil type, impervious areas are modeled with a CN of 98. Lawn areas coinciding with soils B, C and D are associated with CNs of 69, 79 and 84, respectively. Wood-grass combination areas coinciding with soils B, C and D are associated with CNs of 58, 72 and 79, respectively. Wood areas coinciding with soils B, C and D are associated with CNs of 55, 70 and 77, respectively. See Technical Appendix: Downstream Analysis – CN.

Time of Concentration

Each basin was assigned a reasonable time of concentration (Tc) based on basin size and imperviousness. Typically, smaller and more impervious Basins A, B and E were assigned a Tc of 5 minutes. The larger Basin G contains multiple single-family residential developments and some undeveloped/vacant lots; therefore, this basin was assigned a Tc of 15 minutes. The Tc's for undeveloped Basins C, D and F were evaluated to be 75, 35 and 46 minutes per TR-55 methodologies (See Technical Appendix: Downstream Analysis – Tc).

Downstream System Overview

As-builts documents were referenced to model the existing onsite pond and flow control manhole, which will remain in place (See Technical Appendix: As-Built Documents). The downstream system was modeled based on information collected from the City's GIS (wilsonvillemaps.com). For the portions of the downstream system in Arrowhead Creek, the reaches of the creek were modeled as triangular open channels. The side slopes of the channels were estimated based on cross sections taken along the creek using lidar-based data publicly available through the State of Oregon Department of Geology and Mineral Industries (DOGAMI). Chapter 8 of the ODOT Hydraulics Manual (2014) was referenced to select Manning's n coefficients for each conveyance.

Downstream Analysis Results

For the 25-yr design storm, all conveyances were determined to have sufficient capacity (See Technical Appendix: Downstream Analysis – Conveyance Data). The minimum freeboard in the downstream system was evaluated to be 2.06 ft.

Conveyance Analysis

Per City Standards, the onsite conveyance system shall be designed to convey and contain at least the peak runoff for the 25-yr design storm. Furthermore, structures must be demonstrated to provide a minimum of



1 foot of freeboard between the hydraulic grade line and the top of the structure or finish grade above pipe for the 25-yr developed peak rate of runoff. The Conveyance Analysis will be included with the Final Storm Drainage Report to demonstrate.

CONCLUSIONS

This report sufficiently describes the existing site conditions, developed site conditions and the proposed stormwater management strategy.

The proposed Rain Garden is sized to comply with the City's stormwater management requirements. An O&M Plan of the private stormwater BMP will be included with the Final Storm Drainage Report.

The Downstream Analysis demonstrated that the downstream system has sufficient capacity to convey runoff from the project site.

A Conveyance Analysis of the onsite storm drain system will be included with the Final Storm Drainage Report.

REFERENCES

- 1. *Stormwater & Surface Water Standards*. City of Wilsonville, June 2015
- 2. ODOT Hydraulics Manual. ODOT, April 2014
- 3. Urban Hydrology for Small Watersheds (Technical Release 55). USDA, June 1986



TECHNICAL APPENDIX

Exhibits

- National Flood Hazard Layer FIRMette
- Hydrologic Soil Group Clackamas County
- Curve Numbers
- Developed Conditions Exhibit
- Impervious Area Threshold Determination Form

Drawings

- Sheet C100 Existing Conditions & Demolition Plan
- Sheet C210 Preliminary Site & Utility Plan
- Sheet C230 Grading & Erosion Control Plan

Hydrographs

- Existing & Developed

WES BMP Sizing Report

Downstream Analysis

- Wilsonville GIS
- Hydrologic Soil Group (HSG)
- Curve Numbers (CN)
- Time of Concentration (Tc)
- Basin Exhibit
- XPSTORM Hydraulic Layout
- XPSTORM Runoff Data
- XPSTORM Conveyance Data

As-Built Documents

- As-built Plans SJO, July 2004
 - o Sheets C4.1, C5.1, C5.3 & C6.3
- "Wood Middle School Addition Stormwater Management Report" SJO, June 2004

Operations & Maintenance Plan – Will be Included with Final Drainage Report



EXHIBITS



National Flood Hazard Layer FIRMette



Legend



250

1,000

500

1,500

2,000

regulatory purposes.



Web Soil Survey National Cooperative Soil Survey



Hydrologic Soil Group

	1	1	1	
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
1A	Aloha silt loam, 0 to 3 percent slopes	C/D	6.6	79.6%
1B	Aloha silt loam, 3 to 6 percent slopes	C/D	1.1	13.1%
29	Dayton silt loam	D	0.6	7.2%
Totals for Area of Intere	est		8.3	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



Table 2-2aRunoff curve numbers for urban areas 1/

Cover description			Curve nu	umbers for	
Cover description	Average percent		-nyuroiogic	son group	
Cover type and hydrologic condition	impervious area 2^{\prime}	А	В	С	D
Fully developed urban areas (vegetation established)					
Open space (lawns, parks, golf courses, cemeteries, etc.) $\frac{3}{2}$:					
Poor condition (grass cover < 50%)		68	79	86	89
Fair condition (grass cover 50% to 75%)		49	69	79	84
Good condition (grass cover $> 75\%$)		39	61	74	80
Impervious areas:		00	01		00
Paved parking lots, roofs, driveways, etc.					
(excluding right-of-way)		98	98	98	98
Streets and roads:		00	00	00	00
Paved: curbs and storm sewers (excluding					
right-of-way)		98	98	98	98
Paved: open ditches (including right-of-way)		83	89	92	93
Gravel (including right-of-way)		76	85	89	91
Dirt (including right-of-way)		72	82	87	89
Western desert urban areas:					
Natural desert landscaping (pervious areas only) 4/		63	77	85	88
Artificial desert landscaping (impervious weed barrier,					
desert shrub with 1- to 2-inch sand or gravel mulch					
and basin borders)		96	96	96	96
Urban districts:					
Commercial and business		89	92	94	95
Industrial		81	88	91	93
Residential districts by average lot size:					
1/8 acre or less (town houses)		77	85	90	92
1/4 acre		61	75	83	87
1/3 acre		57	72	81	86
1/2 acre		54	70	80	85
1 acre		51	68	79	84
2 acres		46	65	77	82
Developing urban areas					
Newly graded areas					
(pervious areas only, no vegetation) 5/		77	86	91	94
Idle lands (CN's are determined using cover types					
similar to those in table 2-2c).					

¹ Average runoff condition, and $I_a = 0.2S$.

² The average percent impervious area shown was used to develop the composite CN's. Other assumptions are as follows: impervious areas are directly connected to the drainage system, impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition. CN's for other combinations of conditions may be computed using figure 2-3 or 2-4.

³ CN's shown are equivalent to those of pasture. Composite CN's may be computed for other combinations of open space

cover type.

⁴ Composite CN's for natural desert landscaping should be computed using figures 2-3 or 2-4 based on the impervious area percentage (CN = 98) and the pervious area CN. The pervious area CN's are assumed equivalent to desert shrub in poor hydrologic condition.

⁵ Composite CN's to use for the design of temporary measures during grading and construction should be computed using figure 2-3 or 2-4 based on the degree of development (impervious area percentage) and the CN's for the newly graded pervious areas.



WLWV SCHOOL DISTRICT

DISTURBED AREA BOUNDARY

BASIN W/ EQUIV. OR GREATER IMPERVIOUS AREA REQUIRING MANAGEMENT



PROPOSED RAIN GARDEN

PERVIOUS AREA =	1,582 SF
MPERVIOUS AREA =	8,133 SF
RBED AREA =	9,715 SF

RAIN GARDEN AREA = 480 SF



This Detail Drawing may not be altered or changed in any manner except by the City Engineer. It is the responsibility of the user to acquire the most current version.

IMPERVIOUS AREA THRESHOLD DETERMINATION FORM

1. TOTAL NEW AND REPLACED IMPERVIOUS AREA, SF:	Box 1	8,133
2. APPLY IMPERVIOUS REDUCTION METHODS:		
2a. Pervious Pavement, SF:	Box 2a	0
2b. Green Roof, SF:	Box 2b	0

<u>2c. Tree Credit</u> - Applies to NON single family residential developments only. NOTE: Maximum total tree credit allowed is 10% of the Impervious Area in BOX 1:

New Trees

To receive credit, trees must be planted in excess of Planning Division (landscaping) requirements. New evergreen trees must be at least 6 feet tall at the time of planting and new deciduous trees must be at least 2-inch caliper (diameter at 4 feet high). Trees must be planted within 25-feet of ground-level impervious surfaces. New trees cannot be credited against rooftop surfaces or pervious pavement. New trees must be selected from tree species included in Appendix A unless otherwise approved.

Number of new trees meeting criteria x 100 sf each, SF:

Box 2c 0

2d. Existing Tree Canopy

To receive credit, existing tree canopy must be preserved during and after construction (recorded on property deed). Existing trees cannot be credited against rooftop surfaces or pervious pavement. Minimum tree size to receive credit is 6-inch caliper. No credit will be given for existing trees located in vegetative buffers or other requirements of the Planning Division. Tree canopy is measured as the area under the tree drip-line and that is within 25 feet of ground-level impervious surfaces.

SF of existing tree canopy that meets criteria:	Box 2d 0
2e. Total Tree Credit (Box 2c + 2d), OR 10% of Box 1, whichever is SMALLER:	Box 2e 0
3. TOTAL IMPERVIOUS AREA REDUCTION, (Sum of Boxes 2a, 2b, and 2e), SF	Box 3 0
4. PROPOSED IMPERVIOUS AREA,(Box 1 minus Box 3), SF (compare to thresholds):	Box 4 8,133
Impervious Area Threshold Determination Form	CITY OF

Impervious Area Infestion Determination Form			CITY OF	N
DRAWING NUMBER: ST-6000	DRAWN BY: SR	SCALE: N.T.S.	WILSONVILLE	
FILE NAME: ST-6000.DWG	APPROVED BY: NK	DATE: 10/10/14	PUBLIC WORKS ST	FANDARDS

DRAWINGS













LEGEND

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STATES	TTU
0007	

PROPOSED ASPHALT PROPOSED CONCRETE PROPOSED CONCRETE SCORING PROPOSED STORM PIPE PROPOSED SANITARY PIPE PROPOSED WATER DOMESTIC SERVICE PROPOSED TELECOMMUNICATIONS LINE PROPOSED LAWN SEEDING SIGNIFICANT RESOURCE OVERLAY ZONE

CONSTRUCTION KEY NOTES

1 PROPOSED BUILDING ADDITION. SEE ARCHITECTURAL PLANS FOR INFORMATION. 2 PROPOSED ASPHALT PAVING.

3 PROPOSED CONCRETE SIDEWALK.

4 PROPOSED CURB.

5 PROPOSED CURB CUT FOR DRAINAGE - 5 FT WIDE

ADD ALTERNATE: PROPOSED DREENHOUSE. SEE ARCHITECTURAL PLANS FOR INFORMATION.
 ADD ALTERNATE: PROPOSED CONCRETE SIDEWALK.

WATER SYSTEM KEY NOTES

PROPOSED 2 1/2" DOMESTIC SERVICE LINE - 360 LF

2 PROPOSED CONNECTION TO EXISTING 4" WATER LINE.

3 PROPOSED DOMESTIC SERVICE DOUBLE CHECK VAULT.

DOMESTIC WATER POINT OF CONNECTION. SEE PLUMBING PLANS FOR CONTINUATION.

ADD ALTERNATE:
 PROPOSED 1* DOMESTIC SERVICE LINE - 7 LF

ADD ALTERNATE: ODMESTIC WATER POINT OF CONNECTION. SEE PLUMBING PLANS FOR CONTINUATION.

STORM DRAIN KEY NOTES

PROPOSED 8" STORM PIPE - 26 LF

2 PROPOSED 6" STORM PIPE - 22 LF

3 PROPOSED 4* PERFORATED FOUNDATION DRAIN PIPE.

(4) ROOF DRAIN POINT OF CONNECTION. SEE PLUMBING PLANS FOR CONTINUATION.

5 PROPOSED SWING CHECK VALVE.

PROPOSED WYE CONNECTION TO EXISTING PIPE.

PROPOSED INSERTA-TEE CONNECTION TO EXISTING 15" PIPE.

PROPOSED CONNECTION TO EXISTING CATCH BASIN.

9 PROPOSED 6" STORM PIPE - 67 LF

10 PROPOSED 6* STORM PIPE - 29 LF

(1) PROPOSED BEEHIVE OVERFLOW STRUCTURE WITH FLOW CONTROL ORIFICE. PROPOSED RAIN GARDEN - 490 SF. PLANTINGS PER CITY OF WILSONVILLE STORWMATER & SURFACE WATER DESIGN & CONSTRUCTION STANDARDS, APPENDIX A. WATER CONSUMPTION: LOW WATER USAGE AREA (+/- 1* PER WEEK)

(3) PROPOSED 6* PERFORATED STORM PIPE - 30 LF

ADD ALTERNATE: PROPOSED CONNECTION INTO EXISTING 8* STORM PIPE.

PROPOSED CONNECTION INTO EXISTING 8" STORM PIPE.
 ADD ALTERNATE:
 PROPOSED 6" STORM PIPE - 72 LF
 ADD ALTERNATE:
 PROPOSED 6" STORM CLEAN OUT.
 ADD ALTERNATE:
 ROOF DRAIN POINT OF CONNECTION. SEE PLUMBING PLANS FOR CONTINUATION.
 ROOF DRAIN POINT OF CONNECTION. SEE PLUMBING PLANS FOR CONTINUATION.

SANITARY SEWER KEY NOTES

1 PROPOSED 6" SANITARY SEWER PIPE - 307 LF

2 PROPOSED 6* SANITARY CLEAN OUT.

3 PROPOSED CONNECTION TO EXISTING 8" SANITARY SEWER PIPE. SANITARY SEWER POINT OF CONNECTION. SEE PLUMBING PLANS FOR CONTINUATION.

ADD ALTERNATE: PROPOSED 6" SANITARY SEWER PIPE - 4 LF

ADD ALTERNATE:
 SANITARY SEWER POINT OF CONNECTION. SEE PLUMBING PLANS FOR
 CONTINUATION.

UTILITY KEY NOTES

TELECOMMUNICATIONS 4" CONDUIT POINT OF CONNECTION TO EXISTING VAULT. SEE TECHNOLOGY PLANS FOR CONTINUATION.
 TELECOMMUNICATIONS 4" CONDUIT POINT OF CONNECTION TO BUILDING. SEE TELECOMMUNICATIONS FOR CONTINUATION.

LANDSCAPING GENERAL NOTES

RESEED ALL LAWN AREAS DISTURBED BY FOUNDATION AND HARDSCAPE CONSTRUCTION, UTILITY TRENCHING AND ALL OTHER CONSTRUCTION ACTIVITIES. WATER CONSUMPTION: LOW WATER WAGE AREA (+/- 1* PER WEEK)

SITE INFORMATION	
TOTAL SITE AREA	38.65 AC (1,683,594 SF)
EXISTING BUILDING AREA	86,613 SF
PROPOSED ADDITION AREA	1,760 SF
PROPOSED GREENHOUSE AREA	1,288 SF
TOTAL BUILDING AREA	89,661 SF







HYDROGRAPHS



25-yr Runoff Rates - Existing Conditions 25-yr Peak Flow = 0.163 cfs





WES BMP SIZING REPORT



WES BMP Sizing Software Version 1.6.0.2, May 2018

WES BMP Sizing Report

Project Information

Project Name	Inza Wood MS
Project Type	Addition
Location	11055 SW Wilsonville Rd, Wilsonville, OR 97070
Stormwater Management Area	0
Project Applicant	West Linn - Wilsonville School District (WLWV)
Jurisdiction	CCSD1NCSA

Drainage Management Area

Name	Area (sq-ft)	Pre-Project Cover	Post-Project Cover	DMA Soil Type	BMP
Pervious	1,582	Grass	LandscapeCsoil	С	Rain Garden
Impervious	8,133	Grass	ConventionalCo ncrete	С	Rain Garden

LID Facility Sizing Details

LID ID	Design Criteria	ВМР Туре	Facility Soil Type	Minimum Area (sq-ft)	Planned Areas (sq-ft)	Orifice Diameter (in)
Rain Garden	FlowControlA ndTreatment	Rain Garden - Filtration	Lined	446.2	480.0	0.8

Pond Sizing Details

1. FCWQT = Flow control and water quality treatment, WQT = Water quality treatment only

2. Depth is measured from the bottom of the facility and includes the three feet of media (drain rock, separation layer and growing media).

3. Maximum volume of the facility. Includes the volume occupied by the media at the bottom of the facility.

4. Maximum water storage volume of the facility. Includes water storage in the three feet of soil media assuming a 40 percent porosity.

DOWNSTREAM ANALYSIS







45° 17' 56" N

USDA





45° 18' 30" N

45° 17' 56" N

7/7/2020 Page 1 of 4



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
1A	Aloha silt loam, 0 to 3 percent slopes	C/D	74.0	29.4%
1B	Aloha silt loam, 3 to 6 percent slopes	C/D	46.0	18.3%
3	Amity silt loam	C/D	18.2	7.3%
29	Dayton silt loam	D	16.9	6.7%
53B	Latourell loam, 3 to 8 percent slopes	В	0.5	0.2%
84	Wapato silty clay loam	C/D	4.6	1.8%
86A	Willamette silt loam, 0 to 3 percent slopes	В	29.4	11.7%
86B	Willamette silt loam, 3 to 8 percent slopes	В	18.1	7.2%
91A	Woodburn silt loam, 0 to 3 percent slopes	С	0.6	0.2%
91B	Woodburn silt loam, 3 to 8 percent slopes	С	24.7	9.8%
91C	Woodburn silt loam, 8 to 15 percent slopes	С	17.2	6.8%
2310F	Woodburn silt loam, 20 to 55 percent slopes	С	1.1	0.4%
Totals for Area of Inter	rest		251.4	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

Table 2-2aRunoff curve numbers for urban areas 1/

Correct description			Curve nu	umbers for	
Cover description			hydrologic	soil group	
	Average percent				
Cover type and hydrologic condition	impervious area 2/	А	В	С	D
Fully developed urban areas (vegetation established)					
Open space (lawns, parks, golf courses, cemeteries, et	c.) <u>3</u> /:				
Poor condition (grass cover < 50%)		68	79	86	89
Fair condition (grass cover 50% to 75%)		49	69	79	84
Good condition (grass cover > 75%)		39	61	74	80
Impervious areas:					
Paved parking lots, roofs, driveways, etc.					
(excluding right-of-way)		98	98	98	98
Streets and roads:					
Paved; curbs and storm sewers (excluding					
right-of-way)		98	98	98	98
Paved; open ditches (including right-of-way)		83	89	92	93
Gravel (including right-of-way)		76	85	89	91
Dirt (including right-of-way)		72	82	87	89
Western desert urban areas:					
Natural desert landscaping (pervious areas only) 4	/	63	77	85	88
Artificial desert landscaping (impervious weed bar	rier,				
desert shrub with 1- to 2-inch sand or gravel m	ulch				
and basin borders)		96	96	96	96
Urban districts:					
Commercial and business		89	92	94	95
Industrial		81	88	91	93
Residential districts by average lot size:					
1/8 acre or less (town houses)		77	85	90	92
1/4 acre		61	75	83	87
1/3 acre		57	72	81	86
1/2 acre		54	70	80	85
1 acre		51	68	79	84
2 acres		46	65	77	82
Developing urban areas					
Newly graded areas					
(nervious areas only no vegetation) ^{5/}		77	86	91	94
(pervious areas only, no vegetation) =			00	01	υı
Idle lands (CN's are determined using cover types					
similar to those in table $2-2c$).					

¹ Average runoff condition, and $I_a = 0.2S$.

² The average percent impervious area shown was used to develop the composite CN's. Other assumptions are as follows: impervious areas are directly connected to the drainage system, impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition. CN's for other combinations of conditions may be computed using figure 2-3 or 2-4.

³ CN's shown are equivalent to those of pasture. Composite CN's may be computed for other combinations of open space

cover type.

⁴ Composite CN's for natural desert landscaping should be computed using figures 2-3 or 2-4 based on the impervious area percentage (CN = 98) and the pervious area CN. The pervious area CN's are assumed equivalent to desert shrub in poor hydrologic condition.

⁵ Composite CN's to use for the design of temporary measures during grading and construction should be computed using figure 2-3 or 2-4 based on the degree of development (impervious area percentage) and the CN's for the newly graded pervious areas.

Table 2-2c Runoff curve numbers for other agricultural lands 1/

Cover description		Curve numbers for hydrologic soil group			
Cover type	Hydrologic condition	А	В	С	D
Pasture, grassland, or range—continuous forage for grazing. 2/	Poor Fair Good	68 49 39	79 69 61	86 79 74	89 84 80
Meadow—continuous grass, protected from grazing and generally mowed for hay.	—	30	58	71	78
Brush—brush-weed-grass mixture with brush the major element. ${}^{\mathcal{Y}}$	Poor Fair Good	48 35 30 4⁄		77 70 65	83 77 73
Woods—grass combination (orchard or tree farm). $5/$	Poor Fair Good	57 43 32	73 65 58	82 76 72	86 82 79
Woods. 🤄	Poor Fair Good	45 36 30 4⁄	66 60 55	77 73 70	83 79 77
Farmsteads—buildings, lanes, driveways, and surrounding lots.	—	59	74	82	86

 1 $\,$ Average runoff condition, and I_a = 0.2S.

Poor: <50%) ground cover or heavily grazed with no mulch.
 Fair: 50 to 75% ground cover and not heavily grazed.

Good: > 75% ground cover and lightly or only occasionally grazed.

Poor: <50% ground cover.

3

Fair: 50 to 75% ground cover.

Good: >75% ground cover.

 4 $\,$ Actual curve number is less than 30; use CN = 30 for runoff computations.

⁵ CN's shown were computed for areas with 50% woods and 50% grass (pasture) cover. Other combinations of conditions may be computed from the CN's for woods and pasture.

⁶ Poor: Forest litter, small trees, and brush are destroyed by heavy grazing or regular burning. Fair: Woods are grazed but not burned, and some forest litter covers the soil. Good: Woods are protected from grazing, and litter and brush adequately cover the soil.



TIME OF CONCENTRATION (DOWNSTREAM ANALYSIS)

PROJECT NO.: 20617 BY: PJP DATE: 7/8/2020

SHEET FLOW								
INPUT Basin C Basin D						sin F		
Surface Description	Туре	7	Туре	9	Туре	9		
	Grass (Ber	mudagrass)	Woods (Lt_	Underbrush)	Woods (Lt_	Underbrush)		
Manning's "n" Roughness Coefficient	0.41		0.40		0.40			
Initial Area Flow Length, L	300	ft	300	ft	300	ft		
2-Yr 24 Hour Rainfall, P ₂	2.5	in	2.5	in	2.5	in		
Land Slope, s	0.035	ft/ft	0.075	ft/ft	0.090	ft/ft		
OUTPUT	CALCU	JLATED	CALCU	ILATED	CALCU	JLATED		
Travel Time	0.80	hr	0.57	hr	0.53	hr		
SHA	LLOW CON	CENTRATE	D FLOW					
INPUT	VA	LUE	VA	LUE	VA	LUE		
Surface Description	Unp	aved	Unp	aved	Unp	aved		
Flow Length, L	2360 ft		60 ft		980 ft			
Watercourse Slope*, s	0.005 ft/ft		0.010 ft/ft		0.005 ft/ft			
OUTPUT	CALCULATED		CALCULATED		CALCULATED			
Average Velocity, V	1.14	ft/s	1.61	1.61 ft/s		ft/s		
Travel Time	0.575	0.575 hr 0.010 hr		0.239 hr				
	CHAN	NEL FLOW						
INPUT	VA	LUE	VA	LUE	VA	LUE		
Cross Sectional Flow Area, a	0	ft ²	0	ft ²	0	ft ²		
Wetted Perimeter, P _w	0	ft	0	ft	0	ft		
Channel Slope, s	0	ft/ft	0	ft/ft	0	ft/ft		
Manning's "n"	0.	.24	0.	24	0.	24		
Flow Length, L	0	ft	0	ft	0	ft		
OUTPUT	CALCU	JLATED	CALCU	ILATED	CALCU	JLATED		
Average Velocity	0.00	ft/s	0.00	ft/s	0.00	ft/s		
Hydraulic Radius, r = a / P _w	1.00 ft		1.00	ft	1.00	ft		
Travel Time	0.00	hr	0.00	hr	0.00	hr		
	TIME OF CO	ONCENTRA	TION					
Watershed or Subares T -	1.37	hr	0.59	hr	0.77	hr		
vvalersned or Subarea, 1 c =	82	min	35	min	46	min		





Basin	A,tot	A,imp	A,per	CN,avg	Тс	D/S
	ac	ас	ac	(pervious)	min	Node
А	4.18	3.08	1.10	79	5	Basin A
В	3.80	2.67	1.14	79	5	Basin B
С	102.7	0.00	102.7	73	82	Culv In
D	2.68	0.00	2.68	73	35	Culv In
Е	5.44	3.53	1.90	78	5	Culv In
F	9.39	0.00	9.39	73	46	Culv Out
G	23.94	15.56	8.38	73	15	MH-160

tot	TOTAL BASIN AREA
imp	IMPERVIOUS AREA
per	PERVIOUS AREA
l,avg	SPATIALLY-AVERAGED PERVIOUS CURVE NUMBER
;	TIME OF CONCENTRATION
S Node	DOWNSTREAM NODE PER XPSTORM MODEL

Downstream Analysis – XPSTORM Hydraulic Layout





XPSTORM RUNOFF DATA - DOWNSTREAM ANALYSIS - 25-YR STORM EVENT										
POST-DEVELOPED CONDITIONS - WOOD MS REMODEL										
	No	ode Informati	on			Runoff In	formation			
Node	Area	Impervious	Curve	Tc	Rainfall	Infiltration	Surface	Runoff		
Name	acre	%	Number	min.	in	in	in	cfs		
Basin A	3.08	100	98	5	4.00	2.04	1.96	3.39		
	1.100	0	79	5						
Basin B	2.67	100	98	5	4.00	2.04	1.96	3.02		
	1.14	0	79	5						
Culv In	102.7	0	73	82	4.00	0.98	3.02	15.69		
	2.68	0	73	35						
	5.44	65	78	5						
Culv Out	9.39	0	73	46	4.00	2.47	1.53	1.60		
MH-160	23.94	65	73	15	4.00	1.15	2.85	15.47		

XPSTORM RUNOFF DATA - DOWNSTREAM ANAYLSIS - 100-YR STORM EVENT																			
POST-DEVELOPED CONDITIONS - WOOD MS REMODEL																			
	N	ode Informati	on			Runoff In	formation												
Node	Area	Impervious	Curve	Tc	Rainfall	Infiltration	Surface	Runoff											
Name	acre	%	Number	min.	in	in	in	cfs											
Basin A	3.08	100	98	5	4.80	2.17	2.63	4.18											
	1.100	0	79	5															
Basin B	2.67	100	98	5	4.80	2.17	2.63	3.74											
	1.14	0	79	5															
Culv In	102.7	0	73	82	4.80	1.01	3.79	23.73											
	2.68	0	73	35															
	5.44	65	78	5															
Culv Out	9.39	0	73	46	4.80	2.68	2.12	2.46											
MH-160	23.94	65	73	15	4.80	1.20	3.61	19.76											
	XPSTORM CONVEYANCE DATA - DOWNSTREAM ANALYSIS - 25-YEAR STORM EVENT																		
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	THE RESERVE AT FERN HILL - POST-DEVELOPED CONDITIONS - WEST BASIN																		
	Location		Co	nduit Propert	ties			Conduit	Results				Conduit Profile						
	Stat	tion																	
Link	From	То	Diameter	Length	Slope	Design Capacity	Qmax/ Qdesign	Max Flow	Max Velocity	Max Flow Depth	y/d0	US Grnd Elev.	DS Grnd Elev.	US IE	DS IE	US Fb	DS Fb	US HGL	DS HGL
			ft	ft	%	cfs		cfs	ft/s	ft		ft	ft	ft	ft	ft	ft	ft	ft
Link63	Basin A	FCMH	1.25	70.00	0.3	3.54	0.68	2.40	2.10	1.20	0.96	173.00	173.50	169.50	165.29	2.44	3.01	170.56	170.49
Link61	Basin B	FCMH	1.25	120.00	0.3	3.54	0.85	3.01	2.88	1.20	0.96	173.25	173.50	169.65	165.29	2.56	3.01	170.69	170.49
Link74	Culv In	Culv Out	2.50	79.30	1.5	34.81	0.29	20.33	3.24	2.31	0.92	173.00	173.00	169.16	167.94	2.72	2.75	170.28	170.25
Link65	DUMMY	Culv In	1.50	62.00	0.1	2.67	1.76	4.70	3.72	1.15	0.76	173.50	173.00	165.29	169.16	3.06	2.72	170.44	170.28
Link75	Culv Out	MH-160	3.80	1130.00	0.3	79.07	0.27	20.96	0.92	2.79	0.74	173.00	168.95	167.94	164.10	2.75	2.06	170.25	166.89
Link76	MH-160	ST-155	2.25	60.00	1.2	24.33	1.32	32.05	7.94	2.79	1.24	168.95	169.64	164.10	163.39	2.06	3.90	166.89	165.74
Link77	ST-155	END	6.25	205.00	1.4	644.80	0.05	32.05	2.54	2.35	0.38	169.64	171.90	163.39	160.50	3.90	10.14	165.74	161.76

XPSTORM CONVEYANCE DATA - DOWNSTREAM ANALYSIS - 100-YEAR STORM EVENT THE RESERVE AT FERN HILL - POST-DEVELOPED CONDITIONS - WEST BASIN Location **Conduit Properties Conduit Results** Station Design Max Flow US Grnd DS Grnd Qmax/ Max Link Max Flow Diameter Length Slope y/d0 From То Capacity Qdesign Velocity Depth Elev. Elev. ft % cfs ft cfs ft/s ft ft ft FCMH Link63 Basin A 1.25 70.00 0.3 3.54 0.66 2.34 1.83 1.53 1.22 173.00 173.50 FCMH 120.00 1.22 173.25 173.50 Link61 Basin B 1.25 0.3 3.54 1.05 3.73 3.04 1.53 Link74 Culv In Culv Out 2.50 79.30 1.5 34.81 0.41 28.47 3.70 2.64 1.06 173.00 173.00 Link65 DUMMY Culv In 1.50 62.00 0.1 2.67 1.80 4.81 3.18 1.49 0.99 173.50 173.00 Link75 Culv Out MH-160 3.80 1130.00 0.3 79.07 0.38 29.95 0.94 3.75 0.99 173.00 168.95 Link76 MH-160 ST-155 2.25 60.00 1.2 24.33 1.68 40.78 10.02 3.75 1.67 168.95 169.64 Link77 ST-155 END 6.25 205.00 1.4 644.80 0.06 40.78 2.48 2.56 0.41 169.64 171.90

Conduit Profile

US IE

ft

169.50

169.65

169.16

165.29

167.94

164.10

163.39

DS IE	US Fb	DS Fb	US HGL	DS HGL
ft	ft	ft	ft	ft
165.29	2.10	2.68	170.90	170.82
165.29	2.15	2.68	171.10	170.82
167.94	2.32	2.42	170.68	170.58
169.16	2.72	2.32	170.78	170.68
164.10	2.42	1.10	170.58	167.85
163.39	1.10	3.69	167.85	165.95
160.50	3.69	10.02	165.95	161.88

AS-BUILT DOCUMENTS















C5. C6.3 SCALE: NONE



04 06 002 WOOD MIDDLE SCHOOL ADDITION

STORMWATER MANAGEMENT REPORT

City of Wilsonville Engineering Department

STORMWATER MANAGEMENT REPORT

for

Wood Middle School Additions & Remodel Project Wilsonville Road Wilsonville, Oregon







6650 SW Redwood Lane, Suite 360 Portland, Oregon 97224

June 15, 2004

WOOD MIDDLE SCHOOL PROJECT WILSONVILLE ROAD, WEST LINN, OR STORMWATER MANAGEMENT REPORT Page 2

TABLE OF CONTENTS

1. Project Overview Existing Site Information Proposed Development Agency Stormwater Criteria Proposed Stormwater Management

2. Stormwater Detention Summary Site Basin Areas Design Storm 24-Hour Rainfall Amounts Basin Curve Numbers (CN) Basin Runoff Concentration Times (Tc) Stormwater Discharge Peak Flows Detention Summary Orifice Control Structure

3. Water Quality Design

WOOD MIDDLE SCHOOL PROJECT WILSONVILLE ROAD, WEST LINN, OR STORMWATER MANAGEMENT REPORT Page 3

PROJECT OVERVIEW 1.

Existing Site Information

Wood Middle School is an existing facility that was originally developed in the 1970's. Several additions have been added over the years. This project will provide four building additions at different locations around the existing building. In addition, extensive interior remodeling is also included as well as site parking and drainage improvements.

Proposed Development

The proposed improvements to the Middle School include a number of additions and renovations to the school and site. Additional impervious areas are tabulated below:

- New classroom addition at the northeast corner of the existing building.
- B. New classroom addition at the northwest corner of the existing building.
- C. New locker room addition at the southeast corner of the existing building.
- D. New music room and stage addition on the west side of the building.
- E. New exterior plaza outside the stage addition on the west side of the building.
- F. New asphalt play area on the south end of the building.
- G. New expanded parking area to the west of the building.

Existing Site Drainage

The site currently drains to an existing wetland channel to the north. There are no existing water quality or quantity control facilities on the site. The City of Wilsonville has indicated that detention facilities appropriately sized for the total site impervious area (both existing and proposed) will be required as part of the development. The impervious areas are tabulated below:

Total Site Area	=	11.34 Acres
Existing Impervious Area		
Parking	=	1.89 Acres
Existing Roof	=	1.77 Acres
Outside Plaza	- 1 ± 1.	0.27 Acres
Loop Road	- E	0.27 Acres
Track	1 H	0.55 Acres
		4.75 Acres
Proposed New Impervious A	rea	
Classrooms	=	0.05 Acres
Commons/Music	=	0.38 Acres
Locker Rooms	=	0.04 Acres
Plaza (Additional)	=	0.11 Acres
Playground	=	0.19 Acres
Parking -	=	0.29 Acres
1		1.06 Acres

WOOD MIDDLE SCHOOL PROJECT WILSONVILLE ROAD, WEST LINN, OR STORMWATER MANAGEMENT REPORT

Page 4

Proposed Stormwater Management / Agency Stormwater Criteria

<u>Quantity Control</u>: The City of Wilsonville uses the Clean Water Services criteria. Onsite detention is required to provide quantity control for all impervious surface runoff. Detention will be provided to detain the 2-year storm, the 10-year storm, and the 25-year storm to pre-development levels. For this site, detention will be provided using a surface detention pond.

<u>Quality Control</u>: The City of Wilsonville uses the Clean Water Services criteria for quantity control. Onsite quality facilities shall be designed for a dry weather storm event totally 0.36 inches of precipitation falling in 4 hours with a 96 hour return interval. For this site, water quality will be provided using appropriately sized manufactured vender products like Stormceptor.

2. STORMWATER DETENTION SUMMARY

Basin	Impervious Area	Pervious Area	Total Acres
Pre-Development	0.00 acres	11.34 acres	11.34
Post-Development	5.83 acres	5.51 acres	11.34

Site Basin Area

Design 24-Hour Rainfall Amounts

Design Storm	24-Hour Rainfall	Source				
2-Year	2.50"	Based on Clean Water Services				
10-Year	3.45"	Stormwater Management Manua				
25-Year	3.90"	Appendix A				
		Hydrology & Hydraulics				

Basin Curve Numbers (CN)

Basin	Surface	CN	Description
Wood MS Site	New Impervious	98	AC Paving
	New Pervious	80	Lawn
	Existing Greenfield	82	Undeveloped/Greenfield

Concentration Times (Tc)

Basin	Pre/Post	Tc	Description
Wood MS Site	Pre-Dev	40 min	
ACCURATE AND A DESCRIPTION OF	Post-Dev	10 min	

WOOD MIDDLE SCHOOL PROJECT WILSONVILLE ROAD, WEST LINN, OR STORMWATER MANAGEMENT REPORT Page 5

Stormwater Discharge Flows

Design Storm	PreDev Peak Q	PostDev Peak Q	Reg. Det. Vol.
2 Year	1.43 cfs /	4.32 cfs 🦯	10,159 cf /
10 Year	2.85 cfs	6.70 cfs <	13,580 cf 🧹
25-Year	3.59 cfs /	7.87 cfs /	15,544 cf

Detention Summary

Basin	Req. Det. Vol.	Design Det. Vol
Wood MS Site	15,544 cf	Triangular Surface Detention Pond Average Area = (160' x 80') Working Depth = 2.5' Storage Volume = 16,000 cf

Orifice Control Structure

			li and			
Orifice Co	ontrol Struct	ture		Nê.		Production of
Basin	Orifice 1 Diameter	Orifice 1 Height	Orifice 2 Diameter	Orifice 2 Height /	Overflow Height	Jos and
Central	0.55' /	0.0' (= Pipe IE)	1.0' /	1.65%	(2.5)	3.0

Attached Calculations & Worksheets

Attached Calculations & Workshee	ts
Pre-Development Hydrographs Post-Development Hydrographs Routing & Orifice Calculations Charts & Tables Basin Diagrams	14

3. Water Quality Design

Provide Stormceptor for Existing Parking Lot Area Parking Lot Area = 82,500 sf = 1.89 Acres Rainfall = 0.36" Time Period = 4 hours

Water Quality Volume	= (82,500)(0.36) / 12	=	2,475 cf
Water Quality Flow	= 2,475 / 14,400	=	0.172 cfs = 77 gpm

.....

Summary

Use CSR Stormceptor Unit STC 900. Treatment Flow Capacity = 285 gpm. See attached data sheets.



Hydrographs for Wood MS Site

	Jate:	1404-02									
0	Given:	Project =		WOOD MS	5						
		Area =	11.34	acres							
		Pt =	2.5	inches	2-Year / 2	4 Hour St	orm				
		dt =	10	min.							
		Tc =	40	min. (Pre	-Developed	Site Cor	ditions)				
		PERVIOUS	SParcel	and the same	IMPERVIC	US Parc	el				
		Area =	11 34	acres	Area =	0	acres				
		CN =	82	00100	CN =	98	00100				
		s =	2 20		S =	0.20					
		0.26 -	0.44		0.26 -	0.20					
		0.25 -	0.44		0.23 -	0.04					
C	Compute:	Developed	Condition	s Runoff h	ydrograph						
		Column (3 Column (4 Column (5 Column (6) = SCS T) = Col. (3) = Accum) = [If P <=	ype IA Rain) x Pt = 10 julated Sum = 0.2S] = 0;	nfall Distribu year - 24 H of Col. (4) Note, use	ution lour Hyeto PERVIOL	ograph at th IS Area "S'	nis location " value.	i.		
		[If Column (7	P > 0.2S] = Col.(6)	= (Col.(5) - of Present	0.2S)^2/(0 Time Step	Col.(5) + 0 - Col.(6)	.8S); Using of Previous	g the PERV s Time Ste	VIOUS Are	ea "S" value	2.
		Column (8) = Same	method as	for Col.(6).	except us	e the IMP	ERVIOUS	Area "S" v	alue.	
		Column (9) = Col.(8)	of the pres	ent time st	ep - Col.(B) of the pr	evious tim	e step.	1.100 T	
		Column (1	(PEF) = ((PEF))	RVIOUS are	a / Total a	rea) x Col	.(7)) + ((IM	PERVIOU	S area / To	otal area) x	Col.(9))
		Column (1	1) = (60.5	x Col.(10) :	x Total Are	a) / 10 (dt	= 10 minu	tes)	the control of	100.000000	
		Routing	Constant,	w = dt / (21	c + dt) =		0.1111				
		Column (1)	2) = Col.(1	2) of Previ	ous Time S	tep + (w :	([Col.(11)	of Previou	s Time Ste	ep	
		+	Col.(11) c	f Present T	ime Step -	(2 x Col.(12) of Prev	vious Time	Step)])		
			274.2								
_						A	Imagain	Aron			
in.	-0.0		ada y		Pervious	Area	imperviou	IS Alea	1.565		17.36
(1)	(2)	(3)	(4)	(5)	Pervious (6)	(7)	(8)	(9)	(10)	(11)	(12)
(1) Time	(2) Time	(3) Rainfall	(4) Incre-	(5) Accumu-	(6) Accumu-	(7) Incre-	(8) Accumu-	(9) Incre-	(10) Total	(11) Instant	(12) design
(1) Time crement	(2) Time	(3) Rainfall distri-	(4) Incre- mental	(5) Accumu- lated	(6) Accumu- lated	(7) Incre- mental	(8) Accumu- lated	(9) Incre- mental	(10) Total Runoff	(11) Instant hydro-	(12) design hydro-
(1) Time crement	(2) Time	(3) Rainfall distri- bution	(4) Incre- mental Rainfall	(5) Accumu- lated Rainfall	(6) Accumu- lated Runoff	(7) Incre- mental Runoff	(8) Accumu- lated Runoff	(9) Incre- mental Runoff	(10) Total Runoff	(11) Instant hydro- graph	(12) design hydro- graph
(1) Time crement	(2) Time min.	(3) Rainfall distri- bution % of Pt	(4) Incre- mental Rainfall in.	(5) Accumu- lated Rainfall in.	Pervious (6) Accumu- lated Runoff in.	(7) Incre- mental Runoff in.	(8) Accumu- lated Runoff in.	(9) Incre- mental Runoff in.	(10) Total Runoff in.	(11) Instant hydro- graph cfs	(12) design hydro- graph cfs
(1) Time crement	(2) Time min.	(3) Rainfall distri- bution % of Pt	(4) Incre- mental Rainfall in.	(5) Accumu- lated Rainfall in.	Pervious (6) Accumu- lated Runoff in.	(7) Incre- mental Runoff in.	(8) Accumu- lated Runoff 'in.	(9) Incre- mental Runoff in.	(10) Total Runoff in.	(11) Instant hydro- graph cfs	(12) design hydro- graph cfs
(1) Time crement	(2) Time min.	(3) Rainfall distri- bution % of Pt 0.0040	(4) Incre- mental Rainfall in. 0.0100	(5) Accumu- lated Rainfall in. 0.0100	0.0000	(7) Incre- mental Runoff in.	(8) Accumu- lated Runoff 'in.	(9) Incre- mental Runoff in.	(10) Total Runoff in. 0.0000	(11) Instant hydro- graph cfs 0.0	(12) design hydro- graph cfs 0.000
(1) Time crement	(2) Time min. 10 200	(3) Rainfall distri- bution % of Pt 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0100 0.0100	(5) Accumu- lated Rainfall in. 0.0100 0.0200	Contemporation (6) Accumu- Iated Runoff in. 0.0000 0.0000	(7) Incre- mental Runoff in. 0.0000 0.0000	(8) Accumu- lated Runoff 'in. 0.0000 0.0000	(9) Incre- mental Runoff in. 0.0000 0.00000	(10) Total Runoff in. 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000
(1) Time crement 1 2 3	(2) Time min. 10 20 30	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0100 0.0100 0.0100	(5) Accumu- lated Rainfall in. 0.0100 0.0200 0.0300	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000	(7) Incre- mental Runoff in. 0.0000 0.0000 0.0000	(8) Accumu- lated Runoff in. 0.0000 0.0000 0.0000	(9) Incre- mental Runoff in. 0.0000 0.0000 0.0000	(10) Total Runoff in. 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000 0.000
(1) Time crement 1 2 3 4	(2) Time min. 10 20 30 40	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0100 0.0100 0.0100 0.0100	(5) Accumu- lated Rainfall in. 0.0100 0.0200 0.0300 0.0400	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000	(7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000	(8) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000	(9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000
(1) Time crement 1 2 3 4 5	(2) Time min. 10 20 30 40 50	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0100 0.0100 0.0100 0.0100	(5) Accumu- lated Rainfall in. 0.0100 0.0200 0.0300 0.0400 0.0500	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000	(7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000	(8) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000 0.000
(1) Time crement 1 2 3 4 5 6	(2) Time min. 10 20 30 40 50 60	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0100 0.0100 0.0100 0.0100 0.0100	(5) Accumu- lated Rainfall in. 0.0100 0.0200 0.0300 0.0400 0.0500 0.0600	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(8) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000 0.000 0.000
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(1) Time crement 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060	(4) Incre- mental Rainfall in. 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150	(5) Accumu- lated Rainfall in. 0.0100 0.0200 0.0300 0.0400 0.0500 0.0500 0.0600 0.0700 0.0800 0.0900 0.1000 0.1000 0.1125 0.1250 0.1375 0.1500 0.1625 0.1750 0.1900 0.2050 0.2200 0.2350 0.2500	Pervious (6) Accumu- lated Runoff in. 0.0000	(7) Incre- mental Runoff in. 0.0000	(8) Accumu- lated Runoff in. 0.0000 0.0003 0.0003 0.0003 0.0003 0.0003 0.0016 0.0031 0.0031 0.0032 0.0038 0.0052 0.0032 0.00532 0.00532 0.0055 0.00532000000000000000000000000000000000	(9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0004 0.0013 0.0020 0.0027 0.0032 0.0027 0.0032 0.0038 0.0053 0.0060 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102 0.0106 0.0109 0.0112	(10) Total Runoiff in. 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph <u>cfs</u> 0.0000 0.00000 0.00000 0.00000 0.000000 0.00000000
(1) Time crement 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060	(4) Incre- mental Rainfall in. 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150	(5) Accumu- lated Rainfall in. 0.0100 0.0200 0.0300 0.0400 0.0500 0.0400 0.0500 0.0600 0.0700 0.0800 0.0900 0.1025 0.1250 0.1250 0.1250 0.1250 0.1250 0.2200 0.2250 0.2250 0.2500	Pervious (6) Accumu- lated Runoff in. 0.0000	(7) Incre- mental Runoff in. 0.0000	(8) Accumu- lated Runoff in. 0.0000 0.00037 0.0053 0.0032 0.00381 0.00381 0.00532 0.0055 0.00552 0.005552 0.005555555555	(9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0002 0.0027 0.0032 0.0022 0.0038 0.0053 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102 0.0112 0.0115	(10) Total Runoff in. 0.00000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.000000 0.00000000
(1) Time crement 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060	(4) Incre- mental Rainfall in. 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0150 0.0150	(5) Accumu- lated Rainfall in. 0.0100 0.0200 0.0200 0.0300 0.0400 0.0500 0.0500 0.0400 0.0500 0.0600 0.0700 0.0800 0.0900 0.1025 0.1250 0.1250 0.1250 0.1250 0.1250 0.2200 0.2250 0.2250	Pervicus (6) Accumu- lated Runoff in. 0.0000	(7) Incre- mental Runoff in. 0.0000	(8) Accumu- lated Runoff in. 0.0000 0.00037 0.0053 0.0032 0.00381 0.0053 0.0055 0.0053 0.0055	(9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0002 0.0027 0.0032 0.0027 0.0032 0.0033 0.0060 0.0065 0.0070 0.0074 0.0078 0.0078 0.0098 0.0102 0.0112 0.0115 0.0137	(10) Total Runoff in. 0.00000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.000000 0.00000000
(1) Time crement 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0070	(4) Incre- mental Rainfall in. 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0150 0.0150 0.0175 0.0175	(5) Accumu- lated Rainfall in. 0.0100 0.0200 0.0300 0.0400 0.0500 0.0500 0.0500 0.0600 0.0700 0.0800 0.0900 0.1000 0.1125 0.1250 0.1375 0.1500 0.1625 0.1750 0.1625 0.1750 0.2200 0.2250 0.2250 0.2250 0.2855 0.3000	Pervicus (6) Accumu- lated Runoff in. 0.0000	(7) Incre- mental Runoff in. 0.0000	Impervice (8) Accumulated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00016 0.0037 0.0063 0.0246 0.0311 0.0455 0.0532 0.0630 0.0732 0.0838 0.0947 0.1059 0.1174 0.1310 0.1450	(9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0004 0.0013 0.0020 0.0027 0.0032 0.0038 0.0053 0.0065 0.0070 0.0074 0.0078 0.0078 0.0098 0.0102 0.0112 0.0115 0.0137 0.0140	(10) Total Runoif in. 0.00000 0.0000 0.00000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000 0.00000000
(1) Time crement 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0070 0.0070	(4) Incre- mental Rainfall in. 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0150 0.0175 0.0175	(5) Accumu- lated Rainfall in. 0.0100 0.0200 0.0300 0.0400 0.0500 0.0500 0.0600 0.0700 0.0800 0.0900 0.1000 0.1125 0.1250 0.1250 0.1375 0.1500 0.1625 0.1750 0.2200 0.2250 0.2250 0.2250 0.2250 0.2825 0.3000 0.3175	Pervicus (6) Accumu- lated Runoff in. 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	(7) Incre-mental Runoff 0.0000	Impervice (8) Accumulated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00016 0.0037 0.0063 0.0246 0.0381 0.0455 0.0532 0.0630 0.0732 0.0838 0.0947 0.1059 0.1174 0.1310 0.1450	(9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0004 0.0013 0.0020 0.0027 0.0032 0.0032 0.0038 0.0053 0.0065 0.0070 0.0075 0.0076 0.0078 0.0098 0.0102 0.0105 0.0112 0.0115 0.0137 0.0140 0.0142	(10) Total Runoif in. 0.00000 0.00000 0.00000 0.00000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000000
(1) Time Increment 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0070 0.0070 0.0070	(4) Incre- mental Rainfall in. 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0155 0.0175 0.0175 0.0175 0.0175	(5) Accumu- lated Rainfall in. 0.0100 0.0200 0.0300 0.0400 0.0500 0.0500 0.0500 0.0600 0.0700 0.0800 0.0900 0.1000 0.1125 0.1250 0.1250 0.1250 0.1500 0.1625 0.1750 0.2200 0.2250 0.2350 0.2350 0.2350 0.2350 0.2350 0.2350 0.2350 0.2350 0.2350 0.2350 0.2350	Pervicus (6) Accumu- lated Runoff in. 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	(7) Incre-mental Runoff 0.0000	Impervice (8) Accumulated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00016 0.0037 0.0063 0.0133 0.0186 0.0246 0.0381 0.0455 0.0532 0.0630 0.0732 0.0838 0.0947 0.1059 0.1174 0.1310 0.1450 0.1592 0.1737	(9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0004 0.0013 0.0020 0.0027 0.0032 0.0032 0.0038 0.0053 0.0065 0.0065 0.0065 0.0065 0.0070 0.0070 0.0074 0.0078 0.0098 0.0102 0.0106 0.0109 0.0112 0.0115 0.0137 0.0140 0.0142 0.0145	(10) Total Runoif in. 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000000

(1) Time crement	(2) Time	(3) Rainfall distri- bution	(4) Incre- mental Rainfall	(5) Accumu- lated Rainfall	Pervious (6) Accumu- lated Runoff	Area (7) Incre- mental Runoff	Imperviou (8) Accumu- lated Runoff	us Area (9) Incre- mental Runoff	(10) Total Runoff	(11) Instant hydro- graph	(12) design hydro- graph
1	min.	- Caraco	in.	in.	ìn.	in.	in.	in.	in,	cfs	cfs
00	200	0.0070	0.0176	0 2700	0.0000	0.0000	0 2022	0.0149	0.0000	0.0	0.000
28	280	0.0070	0.0175	0.3700	0.0000	0.0000	0.2032	0.0140	0.0000	0.0	0.000
29	290	0.0082	0.0205	0.3903	0.0000	0.0000	0.2200	0.0170	0.0000	0.0	0.000
30	300	0.0082	0.0205	0.4110	0.0000	0.0000	0.2380	0.0176	0.0000	0.0	0.000
31	310	0.0082	0.0205	0.4315	0.0000	0.0000	0.2500	0.0180	0.0000	0.0	0.000
32	320	0.0082	0.0205	0.4520	0.0001	0.0001	0.2748	0.0182	0.0001	0.0	0.001
33	330	0.0082	0.0205	0.4725	0.0005	0.0004	0.2931	0.0183	0.0004	0.0	0.004
34	340	0.0082	0.0205	0.4930	0.0013	0.0008	0.3116	0.0185	8000.0	0.1	0.013
35	350	0.0095	0.0238	0.5168	0.0027	0.0014	0.3331	0.0215	0.0014	0.1	0.026
36	360	0.0095	0.0238	0.5405	0.0045	0.0018	0.3548	0.0217	0.0018	0.1	0.045
37	370	0.0095	0.0238	0.5643	0.0068	0.0023	0.3766	0.0218	0.0023	0.2	0.066
38	380	0.0095	0.0238	0.5880	0.0095	0.0027	0.3985	0.0219	0.0027	0.2	0.089
39	390	0.0095	0.0238	0.6118	0.0126	0.0031	0.4206	0.0221	0.0031	0.2	0.114
40	400	0.0095	0.0238	0.6355	0.0161	0.0035	0.4427	0.0222	0.0035	0.2	0.140
41	410	0.0134	0.0335	0.6690	0.0218	0.0057	0.4741	0.0314	0.0057	0.4	0.179
42	420	0.0134	0.0335	0.7025	0.0282	0.0064	0.5057	0.0316	0.0064	0.4	0.231
43	430	0.0134	0.0335	0.7360	0.0354	0.0072	0.5374	0.0317	0.0072	0.5	0.283
44	440	0.0180	0.0450	0.7810	0.0461	0.0107	0.5802	0.0428	0.0107	0.7	0.357
45	450	0.0180	0.0450	0.8260	0.0580	0.0119	0.6232	0.0430	0.0119	0.8	0.450
46	460	0.0340	0.0850	0.9110	0.0835	0.0255	0.7049	0.0817	0.0255	1.8	0.635
47	470	0.0540	0.1350	1.0460	0.1315	0.0480	0.8355	0.1307	0.0480	3.3	1.054
48	480	0.0270	0.0675	1.1135	0.1585	0.0271	0.9012	0.0657	0.0271	1.9	1.392
49	490	0.0180	0.0450	1.1585	0.1776	0.0191	0.9451	0.0439	0.0191	1.3	0.434
50	500	0.0134	0.0335	1.1920	0.1923	0.0147	.0.9778	0.0327	0.0147	1.0	1.373
51	510	0.0134	0.0335	1.2255	0.2075	0.0151	1.0106	0.0328	0.0151	1.0	1.295
52	520	0.0134	0.0335	1.2590	0.2230	0.0155	1.0434	0.0328	0.0155	1.1	1.241
53	530	0.0088	0.0220	1.2810	0.2334	0.0104	1.0649	0.0216	0.0104	0.7	1.163
54	540	0.0088	0.0220	1.3030	0.2440	0.0106	1.0865	0.0216	0.0106	0.7	1.065
55	550	0.0088	0.0220	1.3250	0.2548	0.0108	1.1081	0.0216	0.0108	0.7	0.991
56	560	0.0088	0.0220	1.3470	0.2657	0.0109	1.1297	0.0216	0.0109	0.7	0.936
57	570	0.0088	0.0220	1.3690	0.2767	0.0111	1,1513	0.0216	0.0111	0.8	0.896
58	580	0.0088	0.0220	1.3910	0.2880	0.0112	1.1729	0.0216	0.0112	0.8	0.866
59	590	0.0088	0.0220	1.4130	0.2993	0.0114	1.1945	0.0216	0.0114	0.8	0.846
60	600	0.0088	0.0220	1.4350	0.3109	0.0115	1.2162	0.0216	0.0115	0.8	0.833
61	610	0.0088	0.0220	1.4570	0.3225	0.0117	1.2378	0.0216	0.0117	0.8	0.824
62	620	0.0088	0.0220	1.4790	0.3343	0.0118	1.2595	0.0217	0.0118	0.8	0.820
63	630	0.0088	0.0220	1.5010	0.3463	0.0119	1.2811	0.0217	0.0119	0.8	0.819
64	640	0.0088	0.0220	1.5230	0.3583	0.0121	1.3028	0.0217	0.0121	0.8	0.820
65	650	0.0072	0.0180	1.5410	0.3683	0.0100	1,3205	0.0177	0.0100	0.7	0.806
66	660	0.0072	0.0180	1.5590	0.3784	0.0101	1.3383	0.0177	0.0101	0.7	0.779
67	670	0.0072	0.0180	1.5770	0.3885	0.0102	1.3560	0.0177	0.0102	0.7	0.760
68	680	0.0072	0.0180	1.5950	0.3988	0.0102	1.3738	0.0178	0.0102	0.7	0.747
69	690	0.0072	0.0180	1.6130	0.4091	0.0103	1.3915	0.0178	0.0103	0.7	0.738
70	700	0.0072	0.0180	1.6310	0.4195	0.0104	1.4093	0.0178	0.0104	0.7	0.732
71	710	0.0072	0.0180	1.6490	0.4300	0.0105	1.4271	0.0178	0.0105	0.7	0.728
72	720	0.0072	0.0180	1.6670	0.4405	0.0106	1.4449	0.0178	0.0106	0.7	0.727
73	730	0.0072	0.0180	1.6850	0.4512	0.0106	1.4626	0.0178	0.0106	0.7	0.727
74	740	0.0072	0.0180	1.7030	0.4619	0.0107	1.4804	0.0178	0.0107	0.7	0.728
75	750	0.0072	0.0180	1.7210	0.4727	0.0108	1.4982	0.0178	0.0108	0.7	0.730
76	760	0.0072	0.0180	1.7390	0.4835	0.0109	1.5160	0.0178	0.0109	0.7	0.733
77	770	0.0057	0.0143	1.7533	0.4922	0.0087	1.5301	0.0141	0.0087	0.6	0.719
78	780	0.0057	0.0143	1.7675	0.5009	0.0087	1.5442	0.0141	0.0087	0.6	0.691
79	790	0.0057	0.0143	1.7818	0.5096	0.0087	1.5583	0.0141	0.0087	0.6	0.671
80	800	0.0057	0.0143	1.7960	0.5184	0.0088	1.5724	0.0141	0.0088	0.6	0.655
81	810	0.0057	0.0143	1.8103	0.5272	0.0088	1.5865	0.0141	0.0088	0.6	0.644

111	(2)	(3)	(4)	(5)	(6)	(7)	(8)	IS Area	(10)	(11)	(12)
Time Increment	Time	Rainfall distri- bution	Incre- mental Rainfall	Accumu- lated Rainfall	Accumu- lated Runoff	Incre- mental Runoff	Accumu- lated Runoff	Incre- mental Runoff	Total Runoff	Instant hydro- graph	design hydro- graph
	min.		in.	in.	in.	in.	in.	in,	in.	cfs	cfs
82	820	0.0057	0.0143	1.8245	0.5361	0.0089	1.6006	0.0141	0.0089	0.6	0.636
83	830	0.0057	0.0143	1.8388	0.5450	0.0089	1.6147	0.0141	0.0089	0.6	0.630
84	840	0.0057	0.0143	1.8530	0.5540	0.0090	1.6288	0.0141	0.0090	0.6	0.626
85	850	0.0057	0.0143	1.8673	0.5630	0.0090	1.6429	0.0141	0.0090	0.6	0.624
86	860	0.0057	0.0143	1.8815	0.5720	0.0090	1.6570	0.0141	0.0090	0.6	0.623
87	870	0.0057	0.0143	1.8958	0.5811	0.0091	1.6711	0.0141	0.0091	0.6	0.623
88	880	0.0057	0.0143	1.9100	0.5902	0.0091	1.6852	0.0141	0.0091	0.6	0.623
89	890	0.0050	0.0125	1.9225	0.5982	0.0080	1.6976	0.0124	0.0080	0.6	0.615
90	900	0.0050	0.0125	1.9350	0.6063	0.0081	1.7100	0.0124	0.0081	0.6	0.601
91	910	0.0050	0.0125	1.9475	0.6144	0.0081	1.7223	0.0124	0.0081	0.6	0.591
92	920	0.0050	0.0125	1.9600	0,6225	0.0081	1.7347	0.0124	0.0081	0.6	0.583
93	930	0.0050	0.0125	1.9725	0.6307	0.0082	1.7471	0.0124	0.0082	0.6	0.578
94	940	0.0050	0.0125	1.9850	0.6389	0.0082	1.7595	0.0124	0.0082	0.6	0.574
95	950	0.0050	0.0125	1.9975	0.6471	0.0082	1.7719	0.0124	0.0082	0.6	0.571
96	960	0.0050	0.0125	2.0100	0.6553	0.0082	1.7843	0.0124	0.0082	0.6	0.570
97	970	0.0050	0.0125	2.0225	0.6636	0.0083	1.7967	0.0124	0.0083	0.6	0.569
98	980	0.0050	0.0125	2.0350	0.6719	0.0083	1.8090	0.0124	0.0083	0.6	0.569
99	990	0.0050	0.0125	2.0475	0.6802	0.0083	1.8214	0.0124	0.0083	0.6	0.569
100	1000	0.0050	0.0125	2.0600	0.6885	0.0084	1.8338	0.0124	0.0084	0.6	0.570
101	1010	0.0040	0.0100	2.0700	0.6952	0.0067	1.8438	0.0099	0.0067	0.5	0.558
102	1020	0.0040	0.0100	2.0800	0.7020	0.0067	1.8537	0.0099	0.0067	0.5	0.536
103	1030	0.0040	0.0100	2.0900	0.7087	0.0067	1.8030	0.0099	0.0067	0.5	0.520
104	1040	0.0040	0.0100	2.1000	0.7154	0.0068	1.8/35	0.0099	0.0068	0.5	0.507
105	1050	0.0040	0.0100	2.1100	0.7222	0.0068	1.8834	0.0099	0.0068	0.5	0.497
106	1060	0.0040	0.0100	2.1200	0.7290	0.0068	1.8933	0.0099	0.0068	0.5	0.490
107	1070	0.0040	0.0100	2.1300	0.7330	0.0000	1.9033	0.0099	0.0000	0.5	0.400
108	1080	0.0040	0.0100	2.1400	0.7420	0.0000	1.9102	0.0099	0.0068	0.5	0.401
109	1100	0.0040	0.0100	2.1500	0.7495	0.0000	1.9231	0.0099	0.0068	0.5	0.476
111	1110	0.0040	0.0100	2.1000	0.7503	0.0000	1 9430	0.0033	0.0000	0.5	0.475
112	1120	0.0040	0.0100	2 1800	0.7002	0.0005	1 9529	0.00000	0.0005	0.5	0.474
112	1130	0.0040	0.0100	2 1900	0.7769	0.0069	1 9628	0.0099	0.0069	0.5	0 474
114	1140	0.0040	0.0100	2 2000	0.7839	0.0069	1 9727	0.0099	0.0069	0.5	0 474
115	1150	0.0040	0.0100	2 2100	0.7908	0.0069	1 9827	0.0099	0.0069	0.5	0.474
116	1160	0.0040	0.0100	2 2200	0.7977	0.0069	1,9926	0.0099	0.0069	0.5	0.474
117	1170	0.0040	0.0100	2 2300	0 8047	0.0070	2.0025	0.0099	0.0070	0.5	0.475
118	1180	0.0040	0.0100	2 2400	0.8117	0.0070	2.0124	0.0099	0.0070	0.5	0.476
119	1190	0.0040	0.0100	2.2500	0.8187	0.0070	2.0224	0.0099	0.0070	0.5	0.476
120	1200	0.0040	0.0100	2.2600	0.8257	0.0070	2.0323	0.0099	0.0070	0.5	0.477
121	1210	0.0040	0.0100	2.2700	0.8327	0.0070	2.0422	0.0099	0.0070	0.5	0.478
122	1220	0.0040	0.0100	2.2800	0.8397	0.0070	2.0521	0.0099	0.0070	0.5	0.479
123	1230	0.0040	0.0100	2.2900	0.8468	0.0070	2.0621	0.0099	0.0070	0.5	0.480
124	1240	0.0040	0.0100	2.3000	0.8538	0.0071	2.0720	0.0099	0.0071	0.5	0.481
125	1250	0.0040	0.0100	2.3100	0.8609	0.0071	2.0819	0.0099	0.0071	0.5	0.482
126	1260	0.0040	0.0100	2.3200	0.8680	0.0071	2.0919	0.0099	0.0071	0.5	0.483
127	1270	0.0040	0.0100	2.3300	0.8751	0.0071	2.1018	0.0099	0.0071	0.5	0.484
128	1280	0.0040	0.0100	2.3400	0.8822	0.0071	2.1117	0.0099	0.0071	0.5	0.485
129	1290	0.0040	0.0100	2.3500	0.8894	0.0071	2.1217	0.0099	0.0071	0.5	0.486
130	1300	0.0040	0.0100	2.3600	0.8965	0.0071	2,1316	0.0099	0.0071	0.5	0.487
131	1310	0.0040	0.0100	2.3700	0.9037	0.0072	2.1415	0.0099	0.0072	0.5	0.488
132	1320	0.0040	0.0100	2.3800	0.9109	0.0072	2.1515	0.0099	0.0072	0.5	0.489
133	1330	0.0040	0.0100	2.3900	0.9180	0.0072	2.1614	0.0099	0.0072	0.5	0.489
134	1340	0.0040	0.0100	2.4000	0.9252	0.0072	2.1714	0.0099	0.0072	0.5	0.490

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				Pervious	Area	Imperviou	is Area			
(2) Time	(3) Rainfall distri-	(4) Incre- mental Raisfall	(5) Accumu- lated Rainfall	(6) Accumu- lated Bupoff	(7) Incre- mental Runoff	(8) Accumu- lated	(9) Incre- mental Bunoff	(10) Total Runoff	(11) Instant hydro-	(12) design hydro-
min.	oution	in.	in.	in.	in.	in.	in.	in.	cfs	cfs
1350	0.0040	0.0100	2 4 1 0 0	0.9325	0.0072	2,1813	0.0099	0.0072	0.5	0.491
1360	0.0040	0.0100	2,4200	0.9397	0.0072	2,1912	0.0099	0.0072	0.5	0.492
1370	0.0040	0.0100	2.4300	0.9469	0.0072	2.2012	0.0099	0.0072	0.5	0.493
1380	0.0040	0.0100	2.4400	0.9542	0.0073	2.2111	0.0099	0.0073	0.5	0.494
1390	0.0040	0.0100	2.4500	0.9615	0.0073	2.2210	0.0099	0.0073	0.5	0.495
1400	0.0040	0.0100	2.4600	0.9687	0.0073	2.2310	0.0099	0.0073	0.5	0.496
1410	0.0040	0.0100	2.4700	0.9760	0.0073	2.2409	0.0099	0.0073	0.5	0.497
1420	0.0040	0.0100	2.4800	0.9834	0.0073	2.2509	0.0099	0.0073	0.5	0.498
1430	0.0040	0.0100	2.4900	0.9907	0.0073	2.2608	0.0099	0.0073	0.5	0.499
1440	0.0040	0.0100	2.5000	0.9980	0.0073	2.2707	0.0099	0.0073	0.5	0.500
							Total Vo	lume of R	unoff =	39882.111
						(cu.ft.)	(Found t multiply convers SUM(Q in cubic V = SUI = (cu.ft/s)	by summin ing by 600 ion require) in cfs to 1 feet as fo $M(Q) \times dt$ x (10 min	g this colur 600 is the ed to conve total volum llows: .) x (60 s/m	sorna mn and ert e
	(2) Time 1350 1360 1370 1380 1400 1410 1420 1430 1440	(2) (3) Time Rainfall distri- bution min. 1350 0.0040 1360 0.0040 1370 0.0040 1380 0.0040 1390 0.0040 1400 0.0040 1410 0.0040 1430 0.0040 1440 0.0040	(2) (3) (4) Time Rainfall distri- bution Incre- mental Rainfall in. 1350 0.0040 0.0100 1360 0.0040 0.0100 1370 0.0040 0.0100 1380 0.0040 0.0100 1390 0.0040 0.0100 1400 0.0040 0.0100 1410 0.0040 0.0100 1420 0.0040 0.0100 1430 0.0040 0.0100 1440 0.0040 0.0100	(2) Time (3) Rainfall distri- bution (4) Incre- mental Rainfall in. (5) Accumu- lated Rainfall in. 1350 0.0040 0.0100 2.4100 1360 0.0040 0.0100 2.4200 1370 0.0040 0.0100 2.4200 1380 0.0040 0.0100 2.4200 1380 0.0040 0.0100 2.4200 1380 0.0040 0.0100 2.4200 1380 0.0040 0.0100 2.4200 1400 0.0040 0.0100 2.4200 1410 0.0040 0.0100 2.4200 1420 0.0040 0.0100 2.4500 1430 0.0040 0.0100 2.4900 1440 0.0040 0.0100 2.5000	(2) (3) (4) (5) (6) Time Rainfall distri- bution Incre- mental Accumu- lated Accumu- lated Accumu- lated 1350 0.0040 0.0100 2.4100 0.9325 1360 0.0040 0.0100 2.4200 0.9397 1370 0.0040 0.0100 2.4200 0.9397 1380 0.0040 0.0100 2.4200 0.9397 1380 0.0040 0.0100 2.4200 0.9397 1380 0.0040 0.0100 2.4200 0.9397 1380 0.0040 0.0100 2.4200 0.9397 1400 0.0040 0.0100 2.4200 0.9542 1390 0.0040 0.0100 2.4500 0.9687 1410 0.0040 0.0100 2.4800 0.9834 1430 0.0040 0.0100 2.4900 0.9907 1440 0.0040 0.0100 2.5000 0.9980	(2) (3) (4) (5) (6) (7) Time Rainfall distri- bution Incre- mental Rainfall Accumu- lated Rainfall Accumu- lated Runoff Incre- mental Runoff 1350 0.0040 0.0100 2.4100 0.9325 0.0072 1360 0.0040 0.0100 2.4200 0.9397 0.0072 1370 0.0040 0.0100 2.4200 0.9397 0.0072 1380 0.0040 0.0100 2.4400 0.9542 0.0073 1390 0.0040 0.0100 2.4500 0.9615 0.0073 1400 0.0040 0.0100 2.4500 0.9687 0.0073 1410 0.0040 0.0100 2.4800 0.9834 0.0073 1420 0.0040 0.0100 2.4800 0.9834 0.0073 1430 0.0040 0.0100 2.4900 0.9980 0.0073 1440 0.0040 0.0100 2.5000 0.9980 0.0073	(2) (3) (4) (5) (6) (7) (8) Time Rainfall distri- bution Incre- mental Rainfall Accumu- lated Rainfall Accumu- lated Runoff Incre- mental Runoff Accumu- mental Runoff Incre- mental Runoff Accumu- lated Runoff Incre- mental Runoff Accumu- lated Runoff 1350 0.0040 0.0100 2.4100 0.9325 0.0072 2.1813 1360 0.0040 0.0100 2.4200 0.9397 0.0072 2.1912 1370 0.0040 0.0100 2.4400 0.9542 0.0073 2.2111 1390 0.0040 0.0100 2.4500 0.9615 0.0073 2.2310 1400 0.0040 0.0100 2.4600 0.9687 0.0073 2.2409 1420 0.0040 0.0100 2.4800 0.9834 0.0073 2.2509 1430 0.0040 0.0100 2.4800 0.9980 0.0073 2.2608 1440 0.0040 0.0100 2.5000 0.9980 0.0073	(2) (3) (4) (5) (6) (7) (8) (9) Time Rainfall distri- bution Incre- mental Accumu- lated Incre- mental Accumu- lated Incre- mental Accumu- mental Incre- mental Accumu- lated Incre- mental Accumu- mental Incre- mental Incr	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	(2) (3) (4) (5) (6) (7) (8) (9) (10) (11) Time Rainfall Incre- bution Accumu- mental Racumu- lated Incre- mental Accumu- lated Incre- mental Total Instant 1350 0.0040 0.0100 2.4100 0.9325 0.0072 2.1813 0.0099 0.0072 0.5 1350 0.0040 0.0100 2.4100 0.9325 0.0072 2.1813 0.0099 0.0072 0.5 1350 0.0040 0.0100 2.4400 0.9325 0.0072 2.1912 0.0099 0.0072 0.5 1380 0.0040 0.0100 2.4400 0.9542 0.0073 2.2111 0.0099 0.0073 0.5 1400 0.0040 0.0100 2.4400 0.9645 0.0073 2.2310 0.0099 0.0073 0.5 1400 0.0040 0.0100 2.4600 0.9834 0.0073 2.2509 0.0099 0.0073 0.5

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	STORMY	VATER CA	LCULATI	ON MATRI	K - SANTA	BARBAR	RA HYDRO	GRAPGH	METHOD		
1 1 1	Date:	Nov-03									
	Given:	Project =		WOOD MS	S						
1.1.1		Area =	11.34	acres							
		Pt =	2.5	inches	2-Year / 2	4 Hour St	orm				
		dt =	10	min.							
		Tc =	10	min. (Pos	t-Develope	ed Site Co	inditions)				
		PERVIOU	S Parcel		IMPERVIO	OUS Parc	el				
		Area =	5.51	acres	Area =	5.83	acres				
		CN =	80		CN =	98					
		S =	2.50		S =	0.20					
		0.2S =	0.50		0.2S =	0.04					
	Compute	Developed	Condition	s Runoff h	vdrooraph						
					, and graphic						
		Column (3	= SCST	ype IA Rair	Ifall Distrib	ution	araab at th	nic location			
		Column (4) = COL(3)) X PL = 10	year - 24 F		igraph at u	iis location	6		
		Column (5) = fif D	- 0 251 - 0	Note une	PEDVICI	IS Area "C	" unlun			
		Columnito	P S O 261	- (Col (5)	note, use		SALES S	value.		n "C" volue	
		Column /7) = Col (6)	- (COL(D) -	Time Stor	COL(S) + 0	of Previous	Time Sie	NOUS AR	a o value	tr.
		Column /9) = Same	method as	for Col (6)	evcent u	the MDI	ERVIOUS	Area "S"	alua	
		Column (9	= Col /8	of the ores	and time st	except us	8) of the or	avious tim	A ston	alue.	
		Column (1	() = (() = () = ()	NIOUS are	a / Total a	real v Col	(7)) + ((1M))	PERVIOU	S area / T	v (core leto	Col (Q))
		Column (1	(1) = (60.5)	v Col (10)	Total Ara	a)/10/dt	- 10 minu	PERVIOU	S alea / I	olar area) x	Col.(9))
		Column (1	(00.5 Constant	x Col.(10)	k Total Are	a)/ 10 (dt	- 10 111110	(es)			
		Routing Column (1	Constant,	w = 017 (2)	c + di =	ton thus	0.3333	of Denviou	Time Ct.		
		Column (1.	Col (11)	(Drospet T	imo Stop	(2 × Col (12) of Prov	inus Timo	Stop)I)	=p	
			00.(11)0	Fiesenti	ine Step -	(2 × COI.(12) 01 Flev	nous rime	Stepili		
1. 10.00		0.0		- Y	Pervious	Area	Imperviou	is Area	10.00	A	-
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)
Time	Time	Rainfall	Incre-	Accumu-	Accumu-	Incre-	Accumu-	Incre-	Total	Instant	design
Increment		distri-	mental Raiofall	lated	lated	mental	lated	mental	Runoff	hydro-	hydro-
		bution	Rainfall	Rainfall	Runoff	Runoff	Runoff	Runoff		graph	graph
	min.	% of Pt	in.	in.	in.	in.	în.	in.	in.	cfs	cfs
1	10	0.0040	0.0100	0.0100	0.0000	0.0000	0,0000	0.0000	0.0000	0.0	0.000
2	20	0.0040	0.0100	0.0200	0.0000	0.0000	0.0000	0.0000	0.0000	0.0	0.000
3	30	0.0040	0.0100	0.0200	0.0000	0.0000	0.0000	0.0000	0.0000	0.0	0.000
4	40	0.0040	0.0100	0.0300	0.0000	0.0000	0.0000	0.0000	0.0000	0.0	0.000
4	50	0.0040	0.0100	0.0400	0.0000	0.0000	0.0000	0.0000	0.0000	0.0	0.000
5	60	0.0040	0.0100	0.0500	0.0000	0.0000	0.0004	0.0004	0.0002	0.0	0.005
0	70	0.0040	0.0100	0.0000	0.0000	0.0000	0.0010	0.0013	0.0000	0.0	0.021
(10	0.0040	0.0100	0.0700	0.0000	0.0000	0.0037	0.0020	0.0010	0.1	0.045
8	80	0.0040	0.0100	0.0800	0.0000	0.0000	0.0003	0.0027	0.0014	0.1	0.070
9	90	0.0040	0.0100	0.0900	0.0000	0.0000	0.0096	0.0032	0.0017	0.1	0.093
10	100	0.0040	0.0100	0.1000	0.0000	0.0000	0.0133	0.0038	0.0019	0.1	0.113
11	110	0.0050	0.0125	0.1125	0.0000	0.0000	0.0186	0.0053	0.0027	0.2	0.144
10	400	0.0000	0.0405	0 1000	0.0000	0.0000	0.0040	0.0000	0.000+	0.0	
12	120	0.0050	0.0125	0.1250	0.0000	0.0000	0.0246	0.0060	0.0031	0.2	0.181
12 13	120	0.0050	0.0125	0.1250	0.0000	0.0000	0.0246	0.0060	0.0031	0.2	0.181
12 13 14	120 130 140	0.0050 0.0050 0.0050	0.0125 0.0125 0.0125	0.1250 0.1375 0.1500	0.0000 0.0000 0.0000	0.0000 0.0000 0.0000	0.0246 0.0311 0.0381	0.0060 0.0065 0.0070	0.0031 0.0033 0.0036	0.2 0.2 0.2	0.181 0.207 0.227
12 13 14 15	120 130 140 150	0.0050 0.0050 0.0050 0.0050	0.0125 0.0125 0.0125 0.0125	0.1250 0.1375 0.1500 0.1625	0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455	0.0060 0.0065 0.0070 0.0074	0.0031 0.0033 0.0036 0.0038	0.2 0.2 0.2 0.3	0.181 0.207 0.227 0.245
12 13 14 15 16	120 130 140 150 160	0.0050 0.0050 0.0050 0.0050 0.0050	0.0125 0.0125 0.0125 0.0125 0.0125 0.0125	0.1250 0.1375 0.1500 0.1625 0.1750	0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532	0.0060 0.0065 0.0070 0.0074 0.0078	0.0031 0.0033 0.0036 0.0038 0.0040	0.2 0.2 0.3 0.3	0.181 0.207 0.227 0.245 0.260
12 13 14 15 16 17	120 130 140 150 160 170	0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060	0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0150	0.1250 0.1375 0.1500 0.1625 0.1750 0.1900	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532 0.0630	0.0060 0.0065 0.0070 0.0074 0.0078 0.0098	0.0031 0.0033 0.0036 0.0038 0.0040 0.0050	0.2 0.2 0.3 0.3 0.3	0.181 0.207 0.227 0.245 0.260 0.293
12 13 14 15 16 17 18	120 130 140 150 160 170 180	0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060	0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150	0.1250 0.1375 0.1500 0.1625 0.1750 0.1900 0.2050	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532 0.0630 0.0732	0.0060 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102	0.0031 0.0033 0.0036 0.0038 0.0040 0.0050 0.0052	0.2 0.2 0.3 0.3 0.3 0.3 0.4	0.181 0.207 0.227 0.245 0.260 0.293 0.332
12 13 14 15 16 17 18 19	120 130 140 150 160 170 180 190	0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060	0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150	0.1250 0.1375 0.1500 0.1625 0.1750 0.1900 0.2050 0.2200	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532 0.0630 0.0732 0.0838	0.0060 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102 0.0106	0.0031 0.0033 0.0036 0.0038 0.0040 0.0050 0.0052 0.0054	0.2 0.2 0.3 0.3 0.3 0.4 0.4	0.181 0.207 0.227 0.245 0.260 0.293 0.332 0.355
12 13 14 15 16 17 18 19 20	120 130 140 150 160 170 180 190 200	0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060	0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0150	0.1250 0.1375 0.1500 0.1625 0.1750 0.1900 0.2050 0.2200 0.2350	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532 0.0630 0.0732 0.0838 0.0947	0.0060 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102 0.0106 0.0109	0.0031 0.0033 0.0036 0.0038 0.0040 0.0050 0.0052 0.0054 0.0056	0.2 0.2 0.3 0.3 0.3 0.4 0.4 0.4	0.181 0.207 0.227 0.245 0.260 0.293 0.332 0.355 0.371
12 13 14 15 16 17 18 19 20 21	120 130 140 150 160 170 180 190 200 210	0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060	0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0150 0.0150	0.1250 0.1375 0.1500 0.1625 0.1750 0.1900 0.2050 0.2200 0.2350 0.2500	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532 0.0630 0.0732 0.0838 0.0947 0.1059	0.0060 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102 0.0106 0.0109 0.0112	0.0031 0.0033 0.0036 0.0038 0.0040 0.0050 0.0052 0.0054 0.0056 0.0058	0.2 0.2 0.3 0.3 0.3 0.4 0.4 0.4 0.4	0.181 0.207 0.227 0.245 0.260 0.293 0.332 0.355 0.371 0.384
12 13 14 15 16 17 18 19 20 21 22	120 130 140 150 160 170 180 190 200 210 220	0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060	0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0150 0.0150	0.1250 0.1375 0.1500 0.1625 0.1750 0.1900 0.2050 0.2200 0.2350 0.2500 0.2650	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532 0.0630 0.0732 0.0838 0.0947 0.1059 0.1174	0.0060 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102 0.0106 0.0109 0.0112 0.0115	0.0031 0.0033 0.0036 0.0038 0.0040 0.0050 0.0052 0.0054 0.0056 0.0058 0.0059	0.2 0.2 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4	0.181 0.207 0.225 0.260 0.293 0.332 0.355 0.371 0.384 0.394
12 13 14 15 16 17 18 19 20 21 22 23	120 130 140 150 160 170 180 190 200 210 220 230	0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060	0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0150 0.0150 0.0175	0.1250 0.1375 0.1500 0.1625 0.1750 0.1900 0.2050 0.2200 0.2350 0.2500 0.2650 0.2825	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532 0.0630 0.0732 0.0838 0.0947 0.1059 0.1174 0.1310	0.0060 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102 0.0106 0.0109 0.0112 0.0115 0.0137	0.0031 0.0033 0.0036 0.0038 0.0040 0.0050 0.0052 0.0054 0.0056 0.0058 0.0059 0.0070	0.2 0.2 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.5	0.181 0.207 0.227 0.245 0.260 0.293 0.332 0.355 0.371 0.384 0.394 0.427
12 13 14 15 16 17 18 19 20 21 22 23 24	120 130 140 150 160 170 180 190 200 210 220 230 230 240	0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0070	0.0125 0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0150 0.0150 0.0175 0.0175	0.1250 0.1375 0.1500 0.1625 0.1750 0.2050 0.2050 0.2200 0.2350 0.2500 0.2650 0.2825 0.3000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532 0.0630 0.0732 0.0838 0.0947 0.1059 0.1174 0.1310 0.1450	0.0060 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102 0.0106 0.0109 0.0112 0.0115 0.0137 0.0140	0.0031 0.0033 0.0036 0.0038 0.0040 0.0050 0.0052 0.0054 0.0056 0.0058 0.0059 0.0070 0.0072	0.2 0.2 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.5 0.5	0.181 0.207 0.227 0.245 0.260 0.293 0.332 0.355 0.371 0.384 0.394 0.427 0.468
12 13 14 15 16 17 18 19 20 21 22 23 24 25	120 130 140 150 160 170 180 190 200 210 220 230 240 250	0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0070 0.0070	0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0150 0.0150 0.0175 0.0175 0.0175	0.1250 0.1375 0.1500 0.1625 0.1750 0.2050 0.2200 0.2350 0.2500 0.2650 0.2825 0.3000 0.3175	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532 0.0630 0.0732 0.0838 0.0947 0.1059 0.1174 0.1310 0.1450 0.1592	0.0060 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102 0.0106 0.0109 0.0112 0.0115 0.0137 0.0140 0.0142	0.0031 0.0033 0.0036 0.0038 0.0040 0.0050 0.0052 0.0054 0.0056 0.0058 0.0059 0.0070 0.0072 0.0073	0.2 0.2 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.5 0.5 0.5	0.181 0.207 0.227 0.245 0.260 0.293 0.332 0.355 0.371 0.384 0.394 0.427 0.468 0.487
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	120 130 140 150 160 170 180 190 200 210 220 230 240 250 260	0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0070 0.0070 0.0070	0.0125 0.0125 0.0125 0.0125 0.0150 0.0150 0.0150 0.0150 0.0150 0.0175 0.0175 0.0175 0.0175	0.1250 0.1375 0.1500 0.1625 0.1750 0.2050 0.2200 0.2350 0.2500 0.2650 0.2825 0.3000 0.3175 0.3350	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0246 0.0311 0.0381 0.0455 0.0532 0.0630 0.0732 0.0838 0.0947 0.1059 0.1174 0.1310 0.1450 0.1592 0.1737	0.0060 0.0065 0.0070 0.0074 0.0078 0.0098 0.0102 0.0106 0.0109 0.0112 0.0115 0.0137 0.0140 0.0142 0.0145	0.0031 0.0033 0.0036 0.0038 0.0040 0.0050 0.0052 0.0054 0.0056 0.0058 0.0059 0.0070 0.0072 0.0073 0.0074	0.2 0.2 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.5 0.5 0.5 0.5	0.181 0.207 0.227 0.245 0.260 0.293 0.332 0.355 0.371 0.384 0.394 0.427 0.468 0.487 0.500

(1) Time ncrement	(2) Time	(3) Rainfall distri- bution	(4) Incre- mental Rainfall	(5) Accumu- lated Rainfall	(6) Accumu- lated Runoff	(7) Incre- mental Runoff	(8) Accumu- lated Runoff	(9) Incre- mental Runoff	(10) Total Runoff	(11) Instant hydro- graph	(12) design hydro- graph	
	mm.		<u></u>	10.		10.		40.	111	CIS	CIS	
28	280	0.0070	0.0175	0.3700	0.0000	0.0000	0.2032	0.0148	0.0076	. 0.5	0.517	
29	290	0.0082	0.0205	0.3905	0.0000	0.0000	0.2208	0.0176	0.0091	0.6	0.554	
30	300	0.0082	0.0205	0.4110	0.0000	0.0000	0.2386	0.0178	0.0092	0.6	0.601	1.4
31	310	0.0082	0.0205	0.4315	0.0000	0.0000	0.2566	0.0180	0.0093	0.6	0.621	
32	320	0.0082	0.0205	0.4520	0.0000	0.0000	0.2748	0.0182	0.0093	0.6	0.632	
33	330	0.0082	0.0205	0.4725	0.0000	0.0000	0.2931	0.0183	0.0094	0.6	0.640	
34	340	0.0082	0.0205	0.4930	0.0000	0.0000	0.3116	0.0185	0.0095	0.7	0.646	
35	350	0.0095	0.0238	0.5168	0.0001	0.0001	0.3331	0.0215	0.0111	0.8	0.687	
36	360	0.0095	0.0238	0.5405	0.0006	0.0005	0.3548	0.0217	0.0114	0.8	0.744	1
37	370	0.0095	0.0238	0.5643	0.0016	0.0010	0.3766	0.0218	0.0117	0.8	0.776	
38	380	0.0095	0.0238	0.5880	0.0030	0.0014	0.3985	0.0219	0.0120	0.8	0.799	
39	390	0.0095	0.0238	0.6118	0.0048	0.0018	0.4206	0.0221	0.0122	0.8	0.819	
40	400	0.0095	0.0238	0.6355	0.0070	0.0022	0.4427	0.0222	0.0125	0.9	0.837	
41	410	0.0134	0.0335	0.6690	0.0107	0.0037	0.4741	0.0314	0.0180	1.2	0.974	
42	420	0.0134	0.0335	0.7025	0.0152	0.0045	0.5057	0.0316	0.0184	1.3	1.156	
43	430	0.0134	0.0335	0.7360	0.0204	0.0052	0.5374	0.0317	0.0188	1.3	1.237	
44	440	0.0180	0.0450	0.7810	0.0284	0.0080	0.5802	0.0428	0.0259	1.8	1.435	
45	450	0.0180	0.0450	0.8260	0.0376	0.0092	0.6232	0.0430	0.0266	1.8	1.679	
46	460	0.0340	0.0850	0.9110	0.0580	0.0204	0.7049	0.0817	0.0519	3.6	2.355	
47	470	0.0540	0.1350	1.0460	0.0979	0.0398	0.8355	0.1307	0.0865	5.9	3.95+	∇
48	480	0.0270	0.0675	1.1135	0.1209	0.0230	0.9012	0.0657	0.0449	3.1	@:324	Sept-
49	490	0.0180	0.0450	1.1585	0.1373	0.0164	0.9451	0.0439	0.0305	2.1	3.168	VE DEN
50	500	0.0134	0.0335	1.1920	0.1500	0.0127	.0.9778	0.0327	0.0230	1.6	2.280	100, 0
51	510	0.0134	0.0335	1.2255	0.1632	0.0132	1.0106	0.0328	0.0232	1.6	1.818	0:4.00
52	520	0.0134	0.0335	1.2590	0.1768	0.0136	1.0434	0.0328	0.0235	1.6	1.674	CC
53	530	0.0088	0.0220	1.2810	0.1859	0.0091	1.0649	0.0216	0.0155	1.1	1.449	DESTRIC
54	540	0.0088	0.0220	1.3030	0.1952	0.0093	1.0865	0.0216	0.0156	1.1	1.195	Cm 14
55	550	0.0088	0.0220	1.3250	0.2047	0.0095	1.1081	0.0216	0.0157	1.1	1.114	Teril
56	560	0.0088	0.0220	1.3470	0.2143	0.0096	1.1297	0.0216	0.0158	3.1	1.092	Ur.
57	570	0.0088	0.0220	1.3690	0.2241	0.0098	1.1513	0.0216	0.0159	1.1	1.000	/
58	580	0.0088	0.0220	1.3910	0.2341	0.0100	1.1729	0.0216	0.0160	1.1	1.090	
59	590	0.0088	0.0220	1.4130	0.2442	0.0101	1.1945	0.0210	0.0160	1.1	1.095	
60	600	0.0088	0.0220	1.4350	0.2545	0.0103	1.2102	0.0210	0.0167	1.1	1.100	1.0
61	610	0.0088	0.0220	1,4570	0.2649	0.0104	1.2370	0.0210	0.0163	1.1	1.100	
02	620	0.0000	0.0220	1.4790	0.2755	0.0100	1 2011	0.0217	0.0163	1.1	1 116	
03	630	0.0088	0.0220	1,5010	0.2002	0.0107	1 2029	0.0217	0.0164	1.1	1 121	
04	040	0.0088	0.0220	1.5230	0.2971	0.0109	1 2205	0.0217	0.0135	0.0	1.057	
00	000	0.0072	0.0180	1.5410	0.3000	0.0090	1 2292	0.0177	0.0135	0.9	0.970	
00	670	0.0072	0.0100	1.5590	0.3131	0.0091	1 3560	0.0177	0.0136	0.0	0.9/0	
60	670	0.0072	0.0100	1 5050	0.3243	0.0092	1 3739	0.0178	0.0136	0.0	0 937	
60	600	0.0072	0.0100	1,5950	0.3333	0.0093	1 3015	0.0178	0.0137	0.9	0.936	
70	700	0.0072	0.0180	1 6310	0 3523	0.0093	1 4093	0.0178	0.0137	0.9	0.938	
70	710	0.0072	0.0180	1 6400	0.3523	0.0094	1 4000	0.0178	0.0138	0.9	0.941	
72	720	0.0072	0.0180	1 6670	0.3714	0.0095	1 4440	0.0178	0.0138	0.9	0.944	
72	720	0.0072	0.0180	1.6850	0.3811	0 0097	1 4626	0.0178	0.0138	0.9	0 947	
74	740	0.0072	0.0180	1 7030	0.3001	0.0000	1 4804	0.0178	0.0139	10	0.950	
75	740	0.0072	0.0180	1 7210	0.4007	0.0098	1 4982	0.0178	0.0139	1.0	0.952	
76	760	0.0072	0.0190	1 7300	0.4106	0.0000	1.5160	0.0178	0.0140	10	0.955	
70	770	0.0072	0.0143	1 7533	0.4195	0.0039	1 5301	0.0141	0.0111	0.8	0.801	1.0
70	790	0.0057	0.0143	1 7675	0.4764	0.0080	1 5442	0.0141	0.0111	0.8	0.805	
70	700	0.0057	0.0143	1 7919	0.4344	0.0080	1 5583	0.0141	0.0111	0.8	0.777	
80	800	0.0057	0.0143	1 7060	0 4425	0.0080	1 5724	0.0141	0.0112	0.8	0.769	
81	810	0.0057	0.0143	1 8103	0.4506	0.0081	1,5865	0.0141	0.0112	0.8	0.767	

1		1.00			Pervious	Area	Imperviou	is Area			
(1) Time Increment	(2) Time	(3) Rainfall distri- bution	(4) Incre- mental Rainfall	(5) Accumu- lated Rainfall	(6) Accumu- lated Runoff	(7) Incre- mental Runoff	(8) Accumu- lated Runoff	(9) Incre- mental Runoff	(10) Total Runoff	(11) Instant hydro- graph	(12) design hydro- graph
	min.		in	in.	in.	in.	in.	in.	in.	cfs	cfs
82	820	0.0057	0.0143	1 8245	0.4587	0.0081	1 6006	0.0141	0.0112	0.8	0.768
83	830	0.0057	0.0143	1 8388	0.4669	0.0082	1.6147	0.0141	0.0112	0.0	0.760
84	840	0.0057	0.0143	1 8530	0.4005	0.0002	1 6288	0.0141	0.0112	0.8	0.705
85	850	0.0057	0.0143	1 8673	0 4834	0.0083	1 6429	0.0141	0.0113	0.8	0.772
86	860	0.0057	0.0143	1 8815	0.4034	0.0003	1.6570	0.0141	0.0113	0.0	0.773
97	870	0.0057	0.0143	1 8058	0.5001	0.0000	1 6711	0.0141	0.0113	0.0	0.775
88	880	0.0057	0.0143	1 9100	0.5085	0.0084	1.6852	0.0141	0.0113	0.8	0.776
80	800	0.0050	0.0125	1 9225	0.5005	0.0004	1 6976	0.0124	0.0100	0.0	0.746
09	000	0.0050	0.0125	1.9220	0.5133	0.0074	1 7100	0.0124	0.0100	0.7	0.740
90	010	0.0050	0.0125	1.9330	0.5209	0.0074	1 7222	0.0124	0.0100	0.7	0.703
91	910	0.0050	0.0125	1.9475	0.5308	0.0075	1.7223	0.0124	0.0100	0.7	0.092
92	920	0.0050	0.0125	1.9000	0.5363	0.0075	1.7.347	0.0124	0.0100	0.7	0.000
93	930	0.0050	0.0125	1.9720	0.5458	0.0075	1.7471	0.0124	0.0100	0.7	0.000
94	940	0.0050	0.0125	1.9850	0.5534	0.0076	1.7595	0.0124	0.0100	0.7	0.088
95	950	0.0050	0.0125	1.9975	0.5610	0.0076	1.7719	0.0124	0.0101	0.7	0.689
96	960	0.0050	0.0125	2.0100	0.5686	0.0076	1.7843	0.0124	0.0101	0.7	0.690
97	970	0.0050	0.0125	2.0225	0.5763	0.0077	1.7967	0.0124	0.0101	0.7	0.691
98	980	0.0050	0.0125	2.0350	0.5839	0.0077	1.8090	0.0124	0.0101	0.7	0.692
99	990	0.0050	0.0125	2.0475	0.5917	0.0077	1.8214	0.0124	0.0101	0.7	0.693
100	1000	0.0050	0.0125	2.0600	0.5994	0.0077	1.8338	0.0124	0.0101	0.7	0.694
101	1010	0.0040	0.0100	2.0700	0.6056	0.0062	1.8438	0.0099	0.0081	0.6	0.649
102	1020	0.0040	0.0100	2.0800	0.6119	0.0062	1.8537	0.0099	0.0081	0.6	0.588
103	1030	0.0040	0.0100	2.0900	0.6181	0.0063	1.8636	0.0099	0.0081	0.6	0.568
104	1040	0.0040	0.0100	2.1000	0.6244	0.0063	.1.8735	0.0099	0.0081	0.6	0.562
105	1050	0.0040	0.0100	2.1100	0.6307	0.0063	1.8834	0.0099	0.0082	0.6	0.560
106	1060	0.0040	0.0100	2.1200	0.6370	0.0063	1.8933	0.0099	0.0082	0.6	0.560
107	1070	0.0040	0.0100	2.1300	0.6433	0.0063	1.9033	0.0099	0.0082	0.6	0.560
108	1080	0.0040	0.0100	2.1400	0.6497	0.0063	1.9132	0.0099	0.0082	0.6	0.561
109	1090	0.0040	0.0100	2.1500	0.6560	0.0064	1.9231	0.0099	0.0082	0.6	0.561
110	1100	0.0040	0.0100	2.1600	0.6624	0.0064	1.9330	0.0099	0.0082	0.6	0.562
111	1110	0.0040	0.0100	2.1700	0.6688	0.0064	1.9430	0.0099	0.0082	0.6	0.563
112	1120	0.0040	0.0100	2,1800	0.6752	0.0064	1.9529	0.0099	0.0082	0.6	0.563
113	1130	0.0040	0.0100	2,1900	0.6816	0.0064	1.9628	0.0099	0.0082	0.6	0.564
114	1140	0.0040	0.0100	2,2000	0.6881	0.0064	1.9727	0.0099	0.0082	0.6	0.564
115	1150	0.0040	0.0100	2,2100	0.6946	0.0065	1,9827	0.0099	0.0082	0.6	0.565
116	1160	0.0040	0.0100	2,2200	0.7010	0.0065	1,9926	0.0099	0.0083	0.6	0.566
117	1170	0.0040	0.0100	2 2300	0.7075	0.0065	2 0025	0.0099	0.0083	0.6	0.566
118	1180	0.0040	0.0100	2 2400	0.7141	0.0065	2.0124	0.0099	0.0083	0.6	0.567
119	1190	0.0040	0.0100	2 2500	0.7206	0.0065	2 0224	0.0099	0.0083	0.6	0.567
120	1200	0.0040	0.0100	2 2600	0.7271	0.0065	2 0323	0.0099	0.0083	0.6	0.568
121	1210	0.0040	0.0100	2 2700	0 7337	0.0066	2 0422	0.0099	0.0083	0.6	0.568
122	1220	0.0040	0.0100	2 2800	0.7403	0.0066	2 0521	0.0000	0.0083	0.6	0.569
123	1220	0.0040	0.0100	2 2900	0 7469	0.0066	2 0621	0.0000	0.0083	0.6	0.570
124	1240	0.0040	0.0100	2 3000	0.7535	0.0066	2 0720	0.0000	0.0083	0.6	0.570
124	1250	0.0040	0.0100	2 3100	0.7601	0.0066	2 0810	0.0000	0.0083	0.6	0.571
120	1250	0.0040	0.0100	2.3100	0.7669	0.0000	2,0019	0.0099	0.0003	0.0	0.571
120	1200	0.0040	0.0100	2.3200	0.7000	0.0000	2 1019	0.0099	0.0003	0.0	0.571
12/	1270	0.0040	0.0100	2.000	0.7704	0.0007	2.1010	0.0099	0.0003	0.0	0.572
128	1280	0.0040	0.0100	2.3400	0.7801	0.0007	2.111/	0.0099	0.0003	0.0	0.572
129	1290	0.0040	0.0100	2.3500	0.7668	0.0067	2.121/	0.0099	0.0084	0.0	0.573
130	1300	0.0040	0.0100	2.3600	0.7935	0.0067	2.1310	0.0099	0.0084	0.0	0.5/3
131	1310	0.0040	0.0100	2.3700	0.8002	0.0067	2.1415	0.0099	0.0084	0.6	0.574
132	1320	0.0040	0.0100	2.3800	0.8069	0.0067	2.1515	0.0099	0.0084	0.6	0.574
133	1330	0.0040	0.0100	2.3900	0.8137	0.0067	2.1614	0.0099	0.0084	0.6	0.575
134	1340	0.0040	0.0100	2.4000	0.8205	0.0068	2.1714	0.0099	0.0084	0.6	0.575

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					Pervious	Area	Imperviou	is Area			
(1) Time Increment	(2) Time	(3) Rainfall distri-	(4) Incre- mental	(5) Accumu- lated	(6) Accumu- lated	(7) Incre- mental	(8) Accumu- lated	(9) Incre- mental	(10) Total Runoff	(11) Instant hydro-	(12) design hydro-
	min.	bution	Rainfall in.	Rainfall in.	Runoff in.	Runoff in.	Runoff in.	Runoff in.	in.	graph cfs	graph cfs
-1						The State State		Barrier Weisergereiten			-
135	1350	0.0040	0.0100	2.4100	0.8272	0.0068	2.1813	0.0099	0.0084	0.6	0.576
136	1360	0.0040	0.0100	2.4200	0.8340	0.0068	2.1912	0.0099	0.0084	0.6	0.576
137	1370	0.0040	0.0100	2.4300	0.8408	0.0068	2.2012	0.0099	0.0084	0.6	0.577
138	1380	0.0040	0.0100	2.4400	0.8477	0.0068	2.2111	0.0099	0.0084	0.6	0.577
139	1390	0.0040	0.0100	2.4500	0.8545	0.0068	2.2210	0.0099	0.0084	0.6	0.578
140	1400	0.0040	0.0100	2.4600	0.8613	0.0069	2.2310	0.0099	0.0084	0.6	0.578
141	1410	0.0040	0.0100	2.4700	0.8682	0.0069	2.2409	0.0099	0.0084	0.6	0.579
142	1420	0.0040	0.0100	2.4800	0.8751	0.0069	2.2509	0.0099	0.0085	0.6	0.579
143	1430	0.0040	0.0100	2.4900	0.8820	0.0069	2.2608	0.0099	0.0085	0.6	0.580
144	1440	0.0040	0.0100	2.5000	0.8889	0.0069	2.2707	0.0099	0.0085	0.6	0.580
		.*:		243				Total Vo	lume of R	unoff =	65486.006 cu. ft
						×	(cu.ft.)	(Found b multiply convers SUM(Q in cubic V = SUM = (cu.ft/s)	by summin ing by 600 ion require) in cfs to t feet as fo V(Q) x dt x (10 min	ig this colui . 600 is the ed to conve- total volume llows: .) x (60 s/m	mn and ert e
							8				

G	Siven: Aver Ave	age Pond Le rage Pond V	Project = W ength (ft) =	OOD MS - 2-1 120.000	YEAR		System:	Pond 120'	long x 50'	wide	
	Aver Ave	rage Pond Li rage Pond V	ength (ft) =	120.000			System:	Pond 120'	long x 50'	wide	
	Ave	rage Pond		E0 000			-)	ond neo	iong x so	wide	
		Orifica Dia	motor (ft) =	0.550							
		Office Dia	neter (it) -	0.550							
	-	Orifice Area		0.238 SF							
	8	Avg Pond Ar Column (3) = Column (4) =	ea = = Col A:L * 600 = Starting Pon	6000.000 SF = Incrementa d Depth = Prev	I CFS into I vious Rema	Pond ining Pon	id Depth = C	ol (11)			
	1	Column (6) =	= 2 * g * Startin	ng h							
		Column (7) =	= Square Root	of 2gh			-				
	1.53	Column (8) =	= Incremental	Vol out = Col (7)*0.60*0	Drifice Are	ea* 600				
	1.2	Column $(9) =$	= Delta Vol = I	Pond Vol = Pr	I In - Increm	iental Vol	out = Col(3)) - Gol (8)			
		Column (10)	= Pond Deoth	at End of Inte	evious Rein	J) / Pond	Area				
	1.1	Column (12)	= Pond CFS	Discharge = C	01(8) / 600	0/11 0/10	/ liou				
(1)	121	(3)	(4)		(6)	(7)	(8)	(9)	(10)	(11)	(12)
Time	Time	Increm.	Starting		(0)	1.1	Increm.	Delta	Remain	Remain	CFS
ncrem.		Vol into	Pond				Vol out	Vol	Total	Pond	Discharge
		Pond	Depth				Pond		Vol	Depth	10000
	min.	cf	ft.				cf	cf	in.	ft	
- 1	10	0.00	0.000		0.000	0.000	0.000	0.00	0.0	0.000	0.0
2	20	0.00	0.000		0.000	0.000	0.000	0.00	0.0	0.000	0.0
3	30	0.00	0.000		0:000	0.000	0.000	0.00	0.0	0.000	0.0
4	40	0.00	0.000		0.000	0.000	0.000	0.00	0.0	0.000	0.0
5	50	2.79	0.000		0.000	0.000	0.000	2.79	2.8	0.000	0.0
5	60	12.56	0.000		0.030	0.173	14.800	-2.24	0.5	0.000	0.0
1	70	27.15	0.000		0.006	0.077	0.000	20.00	21.1	0.004	0.0
8	80	41.95	0.004		0.227	0.470	40.740	12.70	22.3	0.004	0.
10	100	55.00	0.004		0.240	0.490	52 212	14.66	50.7	0.000	0.
11	110	96.60	0.008		0.507	0.022	63 106	23.50	74.3	0.000	0.
12	120	108 47	0.008	÷	0.708	0.750	76 383	32.00	106.4	0.012	0.
13	120	123.95	0.012		1 142	1.069	91 398	32.56	138.9	0.023	0.
14	140	136 34	0.013		1 491	1.221	104 450	31.89	170.8	0.028	0.
15	150	146.84	0.028		1 834	1 354	115 817	31.02	201.9	0.034	0.
16	160	155.99	0.034		2.167	1.472	125.893	30.09	231.9	0.039	0.
17	170	175.78	0.039		2.490	1.578	134.952	40.83	272.8	0.045	0.
18	180	199.47	0.045		2.928	1.711	146.348	53.12	325.9	0.054	0.:
19	190	213.02	0.054		3.498	1.870	159.964	53.05	378.9	0.063	0.:
20	200	222.54	0.063		4.067	2.017	172.494	50.04	429.0	0.071	0.
21	210	230.16	0.071		4.604	2.146	183.531	46.63	475.6	0.079	0.3
22	220	236.67	0.079		5.105	2.259	193.248	43.42	519.0	0.087	0.
23	230	256.32	0.087		5.571	2.360	201.877	54.44	573.5	0.096	0.
24	240	280.51	0.096		6.155	2.481	212.201	68.31	641.8	0.107	0.
25	250	292.42	0.107		6.889	2.625	224.484	67.94	709.7	0.118	0.
25	260	299.82	0.118		7.618	2.760	236.066	63.76	773.5	0.129	0.
26	AND DESCRIPTION OF	2015 27	0.120		8 302	2 881	146 447	58 92	8324	0139	0 /

(1) îme crem.	(2) Time min.	(3) Increm. Vol into Pond cf	(4) Starting Pond Depth ft.	(6)	(7)	(8) Increm. Vol out Pond cf	(9) Delta Vol cf	(10) Remain Total Vol in.	(11) Remain Pond Depth ft	(12) CFS Discharge	
20	200	200.00	0.130	9.025	2 090	255 657	54.22	006.0	0 149	0.43	
20	200	332.30	0.139	9.518	3.085	263.869	68 43	955.2	0.140	0.43	
30	300	360.66	0.159	10 252	3 202	273 861	86.80	1042.0	0.174	0.46	
31	310	372.87	0.174	11 184	3 344	286 033	86.84	1128.8	0 188	0.48	
32	320	379.42	0 188	12 116	3 481	297 714	81.71	1210.5	0.202	0.50	
33	330	383 84	0.202	12 993	3 605	308 301	75.54	1286.1	0.214	0.51	
34	340	387 34	0.214	13 804	3 715	317 775	69.57	1355.6	0.226	0.53	
35	350	411 94	0.226	14 551	3 815	326 256	85.68	1441.3	0.240	0.54	
36	360	446.48	0.240	15 470	3 933	336 408	110.07	1551.4	0.259	0.56	
37	370	465.69	0.259	16 652	4 081	349 018	116.67	1668.1	0.278	0.58	1.0
29	380	470.56	0.278	17 904	4 231	361 903	117.65	1785.7	0.298	0.60	
30	300	475.30	0.208	19 167	4 378	374 449	116.88	1902.6	0.317	0.62	
40	400	502.09	0.317	20 421	4 519	386 509	115.59	2018.2	0.336	0.64	
40	400	584 61	0.336	21 662	4 654	398 076	186 54	2204 7	0.367	0.66	
41	420	693.76	0.367	23 664	4 865	416.066	277 69	2482.4	0.414	0.69	
43	430	741 97	0.414	26 645	5.162	441 492	300.47	2782 9	0.464	0.74	
44	440	861.01	0.464	29.870	5.465	467.448	393 56	3176.4	0.529	0.78	
45	450	1007 17	0.529	34 094	5 839	499 409	507.76	3684.2	0.614	0.83	
46	460	1412 71	0.614	39.544	6,288	537,846	874.87	4559.1	0.760	0.90	
40	470	2370 61	0.760	48 934	6 995	598 307	1772.30	6331.4	1.055	1.00	
48	480	2594 41	1.055	67,957	8.244	705.075	1889.33	8220.7	1.370	1.18	
49	490	1900 52	1.370	88,236	9.393	803.416	1097.11	9317.8	1.553	1.34	
50	500	1368 17	1.553	100.011	10.001	855.348	512.82	9830.6	. 1.638	1.43	
51	510	1090.63	1.638	105.516	10.272	878.571	212.06	10042.7	Nº 1.674	1.46	1
52	520	1004 29	1.674	107.792	10.382	887,996	116.29	10159.0	1.693	20 1.48	1 va
53	530	869.64	1.693	109.040	10.442	893,123	-23:48	10135.5	1.689	1.49	1pe-
54	540	717.10	1.689	108,788	10,430	892.090	-174.99	9960.5	1.660	1.49	(10
55	550	668.70	1.660	106.910	10.340	884.356	-215.66	9744.9	1.624	1.47	1,43
56	560	654.96	1.624	104.595	10.227	874,730	-219.77	9525.1	1.588	1.46	1.5
57	570	652.72	1.588	102,236	10.111	864.810	-212.09	9313.0	1.552	1.44	(5)
58	580	654.26	1,552	99.959	9.998	855.127	-200.86	9112.1	1.519	1.43	-
59	590	657.02	1.519	97.804	9.890	845.855	-188.83	8923.3	1.487	1.41	/
60	600	660.14	1.487	95.777	9.787	837.045	-176.90	8746.4	1.458	1.40	1.1
61	610	663.33	1.458	93.878	9.689	828.706	-165.37	8581.0	1.430	1.38	
62	620	666.51	1.430	92.103	9.597	820.835	-154.33	8426.7	1.404	1.37	
63	630	669.63	1.404	90.447	9.510	813.420	-143.79	8282.9	1.380	1.36	
64	640	672.69	1.380	88.903	9.429	806.450	-133.76	8149.1	1.358	1.34	
65	650	634.49	1.358	87.467	9.352	799.912	-165.42	7983.7	1.331	1.33	
66	660	582.19	1.331	85.692	9.257	791.752	-209.57	7774.2	1.296	1.32	
67	670	566.03	1.296	83.443	9.135	781.291	-215.26	7558.9	1.260	1.30	
68	680	561.91	1.260	81.132	9.007	770.399	-208.49	7350.4	1.225	1.28	h
69	690	561.78	1.225	78.894	8.882	759.700	-197.92	7152.5	1.192	1.27	1.1
70	700	562.96	1,192	76.770	8.762	749.402	-186.44	6966.0	1.161	1.25	
71	710	564.55	1.161	74.769	8.647	739.570	-175.02	6791.0	1.132	1.23	
72	720	566.27	1.132	72.890	8.538	730.221	-163.95	6627.1	1.105	1.22	
73	730	568.01	1.105	71.131	8.434	721.352	-153.34	6473.7	1.079	1.20	
74	740	569.74	1.079	69.485	8.336	712.958	-143.22	6330.5	1.055	1.19	
75	750	571.44	1.055	67.948	8.243	705.027	-133.58	6196.9	1.033	1.18	
76	760	573.13	1.033	66.514	8.156	697.549	-124.42	6072.5	1.012	1.16	-
77	770	534.71	1.012	65.178	8.073	690.511	-155.80	5916.7	0.986	1.15	
78	780	482.71	0.986	63.506	7.969	681.595	-198.88	5717.8	0.953	1.14	
79	790	466.05	0.953	61.371	7.834	670.042	-203.99	5513.8	0.919	1.12	
80	800	461.16	0.919	59.182	7.693	657.981	-196.82	5317.0	0.886	1.10	
81	810	460.18	0.886	57.069	7.554	646.130	-185.95	5131.1	0.855	1.08	

(1) Time Increm.	(2) Time	(3) Increm. Vol into Pond	(4) Starting Pond Depth	(0)	(7)	(8) Increm. Vol out Pond	(9) Delta Vol	(10) Remain Total Vol	(11) Remain Pond Depth	(12) CFS Discharge
	THEL									12 H 1000
82	820	460.50	0.000	57.069	7.554	646.130	-185.63	4945.4	0.824	1.0
83	830	461.25	0.824	53.081	7.286	623.144	-161.90	4783.5	0.797	1.0
84	840	462.13	0.797	51.343	7.165	612.860	-150.73	4632.8	0.772	1.0
85	850	463.05	0.772	49.726	7.052	603.127	-140.08	4492.7	0.749	1.0
86	860	463.97	0.749	48.222	6.944	593.938	-129.97	4362.8	0.727	0.9
87	870	464.89	0.727	46.827	6.843	585.284	-120.40	4242.4	0.707	0.9
88	880	465.80	0.707	45.535	6.748	577.152	-111.35	4131.0	0.689	0.9
89	890	447.54	0.689	44.340	6.659	569.527	-121.99	4009.0	0.668	0.9
90	900	422.82	0.668	43.030	6.560	561.055	-138.24	3870.8	0.645	0.9
91	910	415.03	0.645	41.546	6.446	551.297	-136.27	3734.5	0.622	0.9
92	920	412.88	0.622	40.084	6.331	541.506	-128.63	3605.9	0.601	0.9
93	930	412.60	0.601	38.703	6.221	532.099	-119.50	3486.4	0.581	0.8
94	940	412.94	0.581	37.421	6.117	523.208	-110.26	3376.1	0.563	0.8
95	950	413.49	0.563	36.237	6.020	514.868	-101.38	32/4.8	0.546	0.8
96	960	414.10	0.546	35.149	5.929	507.079	-92.98	3181.8	0.530	0.8
97	970	414.73	0.530	34.151	5.844	499.828	-85.10	3096.7	0.516	0.8
98	980	415.36	0.516	33.238	5.705	493.099	-11.14	3018.9	0.503	0.8
99	990	415.98	0.503	32.403	5.092	400.070	-70.09	2940.0	0.491	0.0
100	1000	416.60	0.491	31.642	5.625	481.120	-04.32	2003.0	0.461	0.0
101	1010	389.35	0.481	30.950	5.303	473.820	-00.40	2/9/.1	0.400	0.7
102	1020	352.72	0.466	30.022	5.479	400.037	-110.92	2001.1	0.447	0.7
103	1030	340.77	0.447	20.110	5.304	400.020	-110.00	2003.1	0.427	0.7
104	1040	337.04	0.427	27.010	5.120	440.000	102.60	2431.3	0.409	0.7
105	1050	336.05	0.409	20.313	5.130	430.730	-102.09	2340.0	0.391	0.7
100	1000	335.97	0.391	20.211	4 020	429.449	-93.40	2170 7	0.362	0.7
107	1070	330.19	0.370	24.207	4.920	420.017	-04.02	2004 4	0.340	0.6
100	1000	330.52	0.302	22.299	4.021	405 523	-68.65	2025.7	0.338	0.6
110	1100	337.23	0.345	21 743	4 663	308 821	-61.59	1964 2	0.327	0.6
111	1110	337 59	0.327	21 082	4 592	392 711	-55.12	1909.0	0.318	0.6
112	1120	337 95	0.318	20 490	4 527	387 162	-49.21	1859.8	0.310	0.6
113	1130	338 31	0.310	19 962	4 468	382,139	-43.83	1816.0	0.303	0.6
114	1140	338.67	0.303	19 492	4.415	377.610	-38.94	1777.1	0.296	0.6
115	1150	339.02	0.296	19.074	4.367	373.539	-34.52	1742.5	0.290	0.6
116	1160	339 37	0.290	18,703	4.325	369.893	-30.52	1712.0	0.285	0.6
117	1170	339.72	0.285	18.376	4.287	366.640	-26.92	1685.1	0.281	0.6
118	1180	340.07	0.281	18.087	4.253	363.746	-23.68	1661.4	0.277	0.6
119	1190	340.41	0.277	17.832	4.223	361.181	-20.77	1640.6	0.273	0.6
120	1200	340.75	0.273	17.610	4.196	358.916	-18.17	1622.5	0.270	0.6
121	1210	341.09	0.270	17.415	4.173	356.923	-15.84	1606.6	0.268	0.5
122	1220	341.42	0.268	17.245	4.153	355.177	-13.75	1592.9	0.265	0.5
123	1230	341.76	0.265	17.097	4.135	353.653	-11.90	1581.0	0.263	0.5
124	1240	342.09	0.263	16.969	4.119	352.330	-10.24	1570.7	0.262	0.5
125	1250	342.42	0.262	16.859	4.106	351.187	-8.77	1562.0	0.260	0.5
126	1260	342.74	0.260	16.765	4.095	350.205	-7.46	1554.5	0.259	0.5
127	1270	343.07	0.259	16.685	4.085	349.368	-6.30	1548.2	0.258	0.5
128	1280	343.39	0.258	16.617	4.076	348.659	-5.27	1542.9	0.257	0.5
129	1290	343.71	0.257	16.561	4.070	348.065	-4.36	1538.6	0.256	0.5
130	1300	344.02	0.256	16.514	4.064	347.573	-3.55	1535.0	0.256	0.5
131	1310	344.34	0.256	16.476	4.059	347.172	-2.83	1532.2	0.255	0.5
132	1320	344.65	0.255	16.446	4.055	346.851	-2,20	1530.0	0.255	0.5
133	1330	344.96	0.255	16.422	4.052	346.602	-1.64	1528.4	0.255	0.5
134	1340	345.27	0.255	16.404	4.050	346.417	-1.15	1527.2	0.255	0.5

(1) Time Increm.	(2) Time min.	(3) Increm. Vol into Pond cf	(4) Starting Pond Depth ft.	(6)	(7)	(8) Increm. Vol out Pond cf	(9) Delta Vol	(10) Remain Total Vol in.	(11) Remain Pond Depth ft	(12) CFS Discharge
135	1350	345.58	0.255	16.392	4.049	346.287	-0.71	1526.5	0.254	0.58
136	1360	345.88	0.254	16.384	4.048	346.206	-0.33	1526.2	0.254	0.58
137	1370	346.18	0.254	16.381	4.047	346.169	0.01	1526.2	0.254	0.58
138	1380	346.48	0.254	16.381	4.047	346.171	0.31	1526.5	0.254	0.58
139	1390	346.78	0.254	16.384	4.048	346.206	0.57	1527.1	0.255	0.58
140	1400	347.08	0.255	16.391	4.049	346.271	0.80	1527.9	0.255	0.58
141	1410	347.37	0.255	16.399	4.050	346.362	1.01	1528.9	0.255	0.58
142	1420	347.66	0.255	16.410	4.051	346.477	1.18	1530.1	0.255	0.58
143	1430	347.95	0.255	16.423	4.053	346.611	1.34	1531.4	0.255	0.58
144	1440	348.24	0.255	16.437	4.054	346.762	1.48	1532.9	0.255	0.58
		65486.01								
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163		1			- QAILIA		AHIDROG	SKAFGH	METHOD		
	Date:	Jun-04		WOODW							
	Given:	Project =	44.94	WOOD M:	5						
		Area =	11.04	acres	10 Verst		· · · · · ·				
		Pt =	3.45	inches	IU-rear/	24 Hour S	storm				
		ar =	10	min.							
		10 =	40	min. (Pre	-Developed	Site Con	ditions)				
		PERVIOUS	SParcel		IMPERVIC	JUS Parc	ef				
		Area =	11.34	acres	Area =	0	acres				
		CN =	82		CN =	98					
		S =	2.20		S =	0.20					
		0.25 =	0.44		0.25 =	0.04					
	Compute	Developed	Condition	s Runoff hy	drograph						
		Column (3 Column (4 Column (5 Column (6 [lf Column (7 Column (8 Column (9) Column (1) Column (1) Routing (1) Column (1) +) = SCS T) = Col. (3) = Accum) = [If P <= P > 0.2S]) = Col.(6)) = Same) = Col.(8) 0) = ((PEF 1) = (60.5 Constant, 2) = Col.(11) o	ype IA Rain) x Pt = 10 ulated Sum = 0.2S] = 0; = (Col.(5) - of Present method as of the pres XVIOUS are x Col.(10) y w = dt / (2T 2) of Previa f Present T	fall Distribu- year - 24 H of Col. (4) Note, use 0.2S)^2/(C Time Step for Col.(6), ent time step for Col.(6), ent time step c Total are c + dt) = bus Time Step - Pervious	ution our Hyeto PERVIOU col.(5) + 0. - Col.(6) (except us ep - Col.(6) rea) x Col. a) / 10 (dt tep + (w x (2 x Col.(1) Area	graph at th S Area "S" 8S); Using of Previous e the IMPE 3) of the pre (7)) + ((IMF = 10 minut 0.1111 [Col.(11) c 12) of Previou	is location. value. the PERV Time Step RVIOUS A evious time PERVIOUS es) of Previous ous Time	IOUS Area Area "S" va step. S area / To Time Step Step)])	a "S" value. alue. tal area) x (o	Col.(9))
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)
Time	Time	Rainfall	Incre-	Accumu-	Accumu-	Incre-	Accumu-	Incre-	Total	Instant	design
Increment		distri-	mental	lated	lated	mental	lated	mental	Runoff	hvdro-	hydro-
		bution	Rainfall	Rainfall	Runoff	Runoff	Runoff	Runoff	Creston -	graph	graph
	min.	% of Pt	in.	in.	in.	in.	in.	in.	in.	cfs	cfs
	10	0.0040	0.0138	0.0128	0.0000	0,000	0.0000	0 0000	0.0000	0.0	0.000
1	10	0.0040	0.0138	0.0138	0.0000	0.0000	0.0000	0.0000	0.0000	0.0	0.000
1 2 2	10 20	0.0040	0.0138	0.0138	0.0000	0.0000	0.0000	0.0000	0.0000	0.0	0.000
1 2 3	10 20 30	0.0040 0.0040 0.0040	0.0138 0.0138 0.0138	0.0138 0.0276 0.0414	0.0000 0.0000 0.0000	0.0000	0.0000 0.0000 0.0000	0.0000 0.0000 0.0000	0.0000 0.0000 0.0000	0.0 0.0 0.0	0.000 0.000 0.000
1 2 3 4	10 20 30 40	0.0040 0.0040 0.0040 0.0040	0.0138 0.0138 0.0138 0.0138	0.0138 0.0276 0.0414 0.0552	0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0009	0.0000 0.0000 0.0000 0.0009	0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000
1 2 3 4 5	10 20 30 40 50	0.0040 0.0040 0.0040 0.0040 0.0040	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138	0.0138 0.0276 0.0414 0.0552 0.0690	0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0009 0.0034	0.0000 0.0000 0.0000 0.0009 0.0025	0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6	10 20 30 40 50 60	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0009 0.0034 0.0072	0.0000 0.0000 0.0000 0.0009 0.0025 0.0037	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7	10 20 30 40 50 60 70	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8	10 20 30 40 50 60 70 80	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9	10 20 30 40 50 60 70 80 90	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10	10 20 30 40 50 60 70 80 90 100	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11	10 20 30 40 50 60 70 80 90 100	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12	10 20 30 40 50 60 70 80 90 100 110 120	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13	10 20 30 40 50 60 70 80 90 100 110 120 130	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14	10 20 30 40 50 60 70 80 90 100 110 120 130	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0118	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	10 20 30 40 50 60 70 80 90 100 110 120 130 140	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173 0.0173	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0118 0.0122	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0133 0.0173 0.0173 0.0173 0.0173 0.0173	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0995	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0118 0.0122 0.0127	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0133 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0995 0.1152	0.0000 0.0009 0.0025 0.0037 0.0048 0.0055 0.0055 0.0072 0.0098 0.0105 0.0112 0.0118 0.0122 0.0127 0.0157	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622 0.2829	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0995 0.1152 0.1314	0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0112 0.0112 0.0127 0.0157 0.0157 0.0162	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2243 0.2245 0.2622 0.2829 0.3036	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0995 0.1152 0.1314 0.1479	0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0112 0.0112 0.0112 0.0122 0.0127 0.0162 0.0166	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0207 0.0207	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622 0.2829 0.3036 0.3243	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0995 0.1152 0.1314 0.1479 0.1648	0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0112 0.0112 0.0122 0.0127 0.0157 0.0162 0.0166 0.0169	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0207 0.0207 0.0207	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622 0.2829 0.3036 0.3243 0.3243	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0746 0.0868 0.0995 0.1152 0.1314 0.1479 0.1648 0.1820	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0118 0.0122 0.0127 0.0157 0.0162 0.0166 0.0169 0.0172	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 8 9 20 20	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0207 0.0207 0.0207	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622 0.2829 0.3036 0.3243 0.3450 0.3657	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0746 0.08695 0.1152 0.1314 0.1479 0.1648 0.1820 0.01995	0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0118 0.0122 0.0127 0.0157 0.0162 0.0166 0.0166 0.0169 0.0172 0.0175	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 7 8 9 20 21 22 23	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0207 0.0207 0.0207 0.0207	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622 0.2829 0.3036 0.3243 0.3450 0.3657 0.3899	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0995 0.1152 0.1314 0.1479 0.1648 0.1820 0.1995	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0118 0.0122 0.0127 0.0157 0.0162 0.0166 0.0169 0.0172 0.0175 0.027	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 9 20 21 22 3 4	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0207 0.0207 0.0207 0.0207 0.0207	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622 0.2829 0.3036 0.3243 0.3450 0.3657 0.3899	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0995 0.1152 0.1314 0.1479 0.1648 0.1820 0.1995 0.2203 0.2412	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0118 0.0122 0.0127 0.0157 0.0162 0.0166 0.0169 0.0172 0.0175 0.0207	0.0000 0.0000	$\begin{array}{c} 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0$	0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 9 20 21 22 3 24 25	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060 0.0070 0.0070	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0207 0.0207 0.0207 0.0207 0.0207 0.0207 0.0242 0.0242	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622 0.2829 0.3036 0.3243 0.3450 0.3657 0.3899 0.4140	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0995 0.1152 0.1314 0.1479 0.1648 0.1820 0.1995 0.2203 0.2203	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0118 0.0122 0.0127 0.0157 0.0162 0.0166 0.0169 0.0172 0.0175 0.0207 0.0210	0.0000 0.0000	$\begin{array}{c} 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0$	0.000 0.000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 9 20 21 22 3 24 25 22	10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250	0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0070 0.0070	0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0207 0.0207 0.0207 0.0207 0.0207 0.0207 0.0207 0.0207	0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622 0.2829 0.3036 0.3243 0.3450 0.3657 0.3899 0.4140 0.4382	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000 0.0009 0.0034 0.0072 0.0120 0.0177 0.0242 0.0313 0.0411 0.0516 0.0628 0.0746 0.0868 0.0746 0.0868 0.0995 0.1152 0.1314 0.1479 0.1648 0.1820 0.1995 0.2203 0.2413 0.2625	0.0000 0.0000 0.0009 0.0025 0.0037 0.0048 0.0057 0.0065 0.0072 0.0098 0.0105 0.0112 0.0118 0.0122 0.0118 0.0122 0.0127 0.0157 0.0162 0.0166 0.0169 0.0172 0.0175 0.0207 0.0210 0.0213	0.0000 0.0000	$\begin{array}{c} 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0$	0.000 0.000

(1) Time ncrement	(2) Time min,	(3) Rainfall distri- bution	(4) Incre- mental Rainfall in.	(5) Accumu- lated Rainfall in.	(6) Accumu- lated Runoff in.	(7) Incre- mental Runoff in.	(8) Accumu- lated Runoff in.	(9) Incre- mental Runoff in.	(10) Total Runoff in.	(11) Instant hydro- graph cfs	(12) design hydro- graph cfs
			10.0212	C. Partice							
28	280	0.0070	0.0242	0.5106	0.0023	0.0013	0.3275	0.0219	0.0013	0.1	0.022
29	290	0.0082	0.0283	0.5389	0.0043	0.0021	0.3533	0.0258	0.0021	0.1	0.043
30	300	0.0082	0.0283	0.5672	0.0071	0.0027	0.3793	0.0260	0.0027	0.2	0.070
31	310	0.0082	0.0283	0.5955	0.0104	0.0033	0.4055	0.0262	0.0033	0.2	0.101
32	320	0.0082	0.0283	0.6238	0.0143	0.0039	0.4318	0.0263	0.0039	0.3	0.134
33	330	0.0082	0.0283	0.6521	0.0188	0.0045	0.4582	0.0265	0.0045	0.3	0.168
34	340	0.0082	0.0283	0.6803	0.0239	0.0051	0.4848	0.0266	0.0051	0.3	0.204
35	350	0.0095	0.0328	0.7131	0.0304	0.0065	0.5157	0.0309	0.0065	0.4	0.247
36	360	0.0095	0.0328	0.7459	0.0376	0.0072	0.5468	0.0311	0.0072	0.5	0.297
37	370	0.0095	0.0328	0.7787	0.0455	0.0079	0.5780	0.0312	0.0079	0.5	0.346
38	380	0.0095	0.0328	0.8114	0.0540	0.0085	0.6093	0.0313	0.0085	0.6	0.394
39	390	0.0095	0.0328	0.8442	0.0631	0.0091	0.6407	0.0314	0.0091	0.6	0.441
40	400	0.0095	0.0328	0.8770	0.0728	0.0097	0.6721	0.0315	0.0097	0.7	0.486
41	410	0.0134	0.0462	0.9232	0.0875	0.0147	0.7167	0.0445	0.0147	1.0	0.564
42	420	0.0134	0.0462	0.9695	0.1032	0.0157	0.7613	0.0447	0.0157	1.1	0.670
12	430	0.0134	0.0462	1 0157	0 1200	0.0167	0 8061	0.0448	0.0167	11	0.769
40	440	0.0180	0.0621	1 0778	0.1440	0.0240	0.8664	0.0603	0.0240	16	0 909
44	440	0.0100	0.0624	1 1200	0.1606	0.0240	0.0004	0.0605	0.0256	1.0	1 085
45	450	0.0160	0.1173	1 2572	0.1090	0.0200	1 0416	0.1147	0.0525	3.6	1 440
40	400	0.0340	0.1173	1.2012	0.2221	0.0020	1.0410	0.1920	0.0020	5.0	3.321
41	470	0.0540	0.1863	1.4435	0.3153	0.0932	1.2243	0.1029	0.0932	0.4	2.231
48	480	0.0270	0.0932	1.5366	0.3659	0.0505	1.3102	0.0917	0.0000	3.5	2.054
49	490	0.0180	0.0621	1.5987	0.4009	0.0350	1.3/75	0.0612	0.0350	2.4	(2.854
50	500	0.0134	0.0462	1.6450	0.4276	0.0267	. 1.4231	0.0456	0.0267	1.8	2:090
51	510	0.0134	0.0462	1.6912	0.4548	0.0272	1.4688	0.0457	0.0272	1.9	2.503
52	520	0.0134	0.0462	1.7374	0.4826	0.0277	1.5144	0.0457	0.0277	1.9	2.366
53	530	0.0088	0.0304	1.7678	0.5010	0.0185	1.5445	0.0300	0.0185	1.3	2.193
54	540	0.0088	0.0304	1.7981	0.5197	0.0187	1.5745	0.0300	0.0187	1.3	1.989
55	550	0.0088	0.0304	1.8285	0.5386	0.0189	1.6045	0.0300	0.0189	1.3	1.833
56	560	0.0088	0.0304	1.8589	0.5577	0.0191	1.6346	0.0300	0.0191	1.3	1.715
57	570	0.0088	0.0304	1.8892	0.5769	0.0193	1.6646	0.0301	0.0193	1.3	1.626
58	580	0.0088	0.0304	1.9196	0.5964	0.0194	1.6947	0.0301	0.0194	1.3	1.560
59	590	0.0088	0.0304	1.9499	0.6160	0.0196	1.7248	0.0301	0.0196	1.3	1.511
60	600	0.0088	0.0304	1,9803	0.6358	0.0198	1.7548	0.0301	0.0198	1.4	1.476
61	610	0.0088	0.0304	2.0107	0.6557	0.0200	1.7849	0.0301	0.0200	1.4	1,451
62	620	0.0088	0.0304	2.0410	0.6759	0.0201	1.8150	0.0301	0.0201	1.4	1,434
63	630	0.0088	0.0304	2.0714	0.6962	0.0203	1.8451	0.0301	0.0203	1.4	1,424
64	640	0.0088	0.0304	2 1017	0.7166	0.0205	1.8752	0.0301	0.0205	1.4	1,418
65	650	0.0072	0.0248	2 1266	0.7335	0.0168	1.8999	0.0240	0.0168	12	1.387
66	660	0.0072	0.0248	2 1514	0 7504	0.0170	1 9245	0.0246	0.0170	12	1 337
67	670	0.0072	0.0248	2 1763	0 7675	0.0171	1 9492	0.0246	0.0171	12	1 299
69	680	0.0072	0.0249	2 2011	0 7846	0.0171	1 9738	0.0247	0.0171	12	1 271
60	600	0.0072	0.0240	2 2250	0.8010	0.0172	1 0085	0.0247	0.0172	12	1 251
70	700	0.0072	0.0240	2.2209	0.8100	0.0172	2 0221	0.0247	0.0172	12	1 226
70	700	0.0072	0.0248	2.2008	0.0192	0.0173	2.0231	0.0247	0.0174	1.2	1 207
/1	710	0.0072	0.0248	2.2/50	0.0300	0.0174	2.04/8	0.0247	0.0174	1.2	1.227
12	720	0.0072	0.0248	2.3005	0.8542	0.0175	2.0725	0.0247	0.0175	1.2	1.220
73	730	0.0072	0.0248	2.3253	0.8/18	0.0176	2.09/1	0.0247	0.0176	1.2	1.21/
74	740	0.0072	0.0248	2.3501	0.8895	0.0177	2.1218	0.0247	0.0177	1.2	1,216
75	750	0.0072	0.0248	2.3750	0.9073	0.0178	2.1465	0.0247	0.0178	1.2	1.216
76	760	0.0072	0.0248	2.3998	0.9251	0.0179	2.1712	0.0247	0.0179	1.2	1.218
77	770	0.0057	0.0197	2.4195	0.9393	0.0142	2.1907	0.0195	0.0142	1.0	1.192
78	780	0.0057	0.0197	2.4392	0.9536	0.0143	2.2103	0.0195	0.0143	1.0	1.144
79	790	0.0057	0.0197	2.4588	0.9679	0.0143	2.2298	0.0195	0.0143	1.0	1.107
80	800	0.0057	0.0197	2.4785	0.9822	0.0144	2.2493	0.0195	0.0144	1.0	1.080
81	810	0.0057	0.0197	2.4981	0.9966	0.0144	2.2689	0.0195	0.0144	1.0	1.059

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	1000		11.		Pervious	Area	Imperviou	is Area	14.14	L /CAN	
(1) Time ncrement	(2) Time	(3) Rainfall distri-	(4) Incre- mental	(5) Accumu- lated	(6) Accumu- lated	(7) Incre- mental	(8) Accumu- lated	(9) Incre- mental	(10) Total Runoff	(11) Instant hydro-	(12) design hydro-
	-	bution	Rainfall	Rainfall	Runoff	Runoff	Runoff	Runoff	4.4	graph	graph
	min.		in.	in.	in.	Jn.	in,	in.	In.	CIS	CIS
82	820	0.0057	0.0197	2.5178	1.0111	0.0145	2.2884	0.0196	0.0145	1.0	1.044
83	830	0.0057	0.0197	2.5375	1.0256	0.0145	2.3080	0.0196	0.0145	1.0	1.032
84	840	0.0057	0.0197	2.5571	1.0401	0.0145	2.3276	0.0196	0.0145	1.0	1.024
85	850	0.0057	0.0197	2.5768	1.0547	0.0146	2.3471	0.0196	0.0146	1.0	1.019
86	860	0.0057	0.0197	2.5965	1.0694	0.0146	2.3667	0.0196	0.0146	1.0	1.015
87	870	0.0057	0.0197	2.6161	1.0841	0.0147	2.3862	0.0196	0.0147	1.0	1.013
88	880	0.0057	0.0197	2.6358	1.0988	0.0147	2.4058	0.0196	0.0147	1.0	1.012
89	890	0.0050	0.0173	2.6531	1.1118	0.0130	2.4229	0.0172	0.0130	0.9	0.998
90	900	0.0050	0.0173	2.6703	1.1248	0.0130	2.4401	0.0172	0.0130	0.9	0.974
91	910	0.0050	0.0173	2.6876	1.1378	0.0130	2.4573	0.0172	0.0130	0.9	0.956
92	920	0.0050	0.0173	2.7048	1.1508	0.0131	2.4744	0.0172	0.0131	0.9	0.943
93	930	0.0050	0.0173	2.7221	1.1639	0.0131	2.4916	0.0172	0.0131	0.9	0.932
94	940	0.0050	0.0173	2.7393	1.1770	0.0131	2.5088	0.0172	0.0131	0.9	0.925
95	950	0.0050	0.0173	2.7566	1.1902	0.0132	2.5259	0.0172	0.0132	0.9	0.920
96	960	0.0050	0.0173	2.7738	1.2034	0.0132	2.5431	0.0172	0.0132	0.9	0.916
97	970	0.0050	0.0173	2.7911	1.2166	0.0132	2.5602	0.0172	0.0132	0.9	0.914
98	980	0.0050	0.0173	2.8083	1.2298	0.0132	2.5774	0.0172	0.0132	0.9	0.912
99	990	0.0050	0.0173	2.8256	1.2431	0.0133	2.5946	0.0172	0.0133	0.9	0.912
100	1000	0.0050	0.0173	2.8428	1.2564	0.0133	2.6118	0.0172	0.0133	0.9	0.912
101	1010	0.0040	0.0138	2.8566	1.2671	0.0107	2.6255	0.0137	0.0107	0.7	0.892
102	1020	0.0040	0.0138	2.8704	1.2778	0.0107	2.6392	0.0137	0.0107	0.7	0.856
103	1030	0.0040	0.0138	2.8842	1.2885	0.0107	2.6530	0.0137	0.0107	0.7	0.829
104	1040	0.0040	0.0138	2.8980	1.2992	0.0107	2.6667	0.0137	0.0107	0.7	0.808
105	1050	0.0040	0.0138	2.9118	1.3099	0.0107	2.6804	0.0137	0.0107	0,7	0.792
106	1060	0.0040	0.0138	2.9256	1.3207	0.0108	2.6942	0.0137	0.0108	0.7	0.780
107	1070	0.0040	0.0138	2.9394	1.3315	0.0108	2.7079	0.0137	0.0108	0.7	0.771
108	1080	0.0040	0.0138	2.9532	1.3423	0.0108	2.7217	0.0137	0.0108	0.7	0.764
109	1090	0.0040	0.0138	2.9670	1.3531	0.0108	2.7354	0.0137	0.0108	0.7	0.759
110	1100	0.0040	0.0138	2.9808	1.3639	0.0108	2.7491	0.0137	0.0108	0.7	0.755
111	1110	0.0040	0.0138	2.9946	1.3747	0.0108	2.7629	0.0137	0.0108	0.7	0.753
112	1120	0.0040	0.0138	3.0084	1.3856	0.0109	2.7766	0.0137	0.0109	0.7	0.751
113	1130	0.0040	0.0138	3.0222	1.3965	0.0109	2.7904	0.0137	0.0109	0.7	0.750
114	1140	0.0040	0.0138	3.0360	1.4074	0.0109	2.8041	0.0137	0.0109	0.7	0.749
115	1150	0.0040	0.0138	3.0498	1.4183	0.0109	2.8179	0.0137	0.0109	0.7	0.749
116	1160	0.0040	0.0138	3.0636	1.4292	0.0109	2.8316	0.0137	0.0109	0.7	0.749
117	1170	0.0040	0.0138	3.0774	1.4402	0.0109	2.8454	0.0137	0.0109	0.8	0.749
118	1180	0.0040	0.0138	3.0912	1.4511	0.0110	2.8591	0.0137	0.0110	0.8	0.750
119	1190	0.0040	0.0138	3.1050	1.4621	0.0110	2.8728	0.0137	0.0110	0.8	0.750
120	1200	0.0040	0.0138	3.1188	1.4731	0.0110	2.8866	0.0137	0.0110	0.8	0.751
121	1210	0.0040	0.0138	3.1326	1.4841	0.0110	2.9003	0.0137	0.0110	0.8	0.752
122	1220	0.0040	0.0138	3.1464	1.4951	0.0110	2.9141	0.0137	0.0110	0.8	0.753
123	1230	0.0040	0.0138	3.1602	1.5062	0.0110	2.9278	0.0137	0.0110	0.8	0.754
124	1240	0.0040	0.0138	3.1740	1.5172	0.0111	2.9416	0.0137	0.0111	0.8	0.755
125	1250	0.0040	0.0138	3.1878	1.5283	0.0111	2.9553	0.0137	0.0111	0.8	0.756
126	1260	0.0040	0.0138	3.2016	1.5394	0.0111	2.9691	0.0137	0.0111	0.8	0.757
127	1270	0.0040	0.0138	3.2154	1.5505	0.0111	2.9828	0.0137	0.0111	0.8	0.758
128	1280	0.0040	0.0138	3.2292	1.5616	0.0111	2.9966	0.0137	0.0111	0.8	0.759
129	1290	0.0040	0.0138	3.2430	1.5727	0.0111	3.0103	0.0138	0.0111	0.8	0.760
130	1300	0.0040	0.0138	3.2568	1.5839	0.0111	3.0241	0.0138	0.0111	0.8	0.761
131	1310	0.0040	0.0138	3.2706	1.5950	0.0112	3.0378	0.0138	0.0112	0.8	0.762
132	1320	0.0040	0.0138	3.2844	1.6062	0.0112	3.0516	0.0138	0.0112	0.8	0.763
133	1330	0.0040	0.0138	3.2982	1.6174	0.0112	3.0653	0.0138	0.0112	0.8	0.764
134	1340	0.0040	0.0138	3.3120	1.6286	0.0112	3.0791	0.0138	0.0112	0.8	0.765

					Pervious	Area	Imperviou	is Area	1.1100		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)
Time	Time	Rainfall	Incre-	Accumu-	Accumu-	Incre-	Accumu-	Incre-	Total	Instant	design
Increment		distri-	mental	lated	lated	mental	lated	mental	Runoff	hydro-	hydro-
		bution	Rainfall	Rainfall	Runoff	Runoff	Runoff	Runoff		graph	graph
	min.		in.	in.	in.	in.	in.	in.	in.	cfs	cfs
135	1350	0.0040	0.0138	3.3258	1.6398	0.0112	3.0928	0.0138	0.0112	0.8	0.766
136	1360	0.0040	0.0138	3.3396	1.6511	0.0112	3.1066	0.0138	0.0112	0.8	0.767
137	1370	0.0040	0.0138	3.3534	1.6623	0.0112	3.1203	0.0138	0.0112	0.8	0.768
138	1380	0.0040	0.0138	3.3672	1.6736	0.0113	3.1341	0.0138	0.0113	0.8	0.769
139	1390	0.0040	0.0138	3.3810	1.6848	0.0113	3.1479	0.0138	0.0113	0.8	0.770
140	1400	0.0040	0.0138	3.3948	1.6961	0.0113	3.1616	0.0138	0.0113	0.8	0.771
141	1410	0.0040	0.0138	3.4086	1.7074	0.0113	3.1754	0.0138	0.0113	0.8	0.772
142	1420	0.0040	0.0138	3.4224	1.7187	0.0113	3.1891	0.0138	0.0113	0.8	0.772
143	1430	0.0040	0.0138	3.4362	1.7301	0.0113	3.2029	0.0138	0.0113	0.8	0.773
144	1440	0.0040	0.0138	3.4500	1.7414	0.0113	3.2166	0.0138	0.0113	0.8	0.774
								Total Vo	lume of Ru	unoff =	69824.489
											cu. ft.
								(Found to multiply convers SUM(Q) in cubic V = SUM	by summin ng by 600 ion require) in cfs to t feet as fol M(Q) x dt	g this colur . 600 is the ed to conve otal volume lows:	nn and rt
<u>.</u>							(cu.ft.)	= (cu.ft/s)	x (10 min.) x (60 s/m	in.)
							3 4 .5				

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Given: Project = 11.34 acres Area = 11.34 acres Pt = 3.45 inches 10-Year / 24 Hour Storm dt = 10 init. (Post-Developed Site Conditions) PERVIOUS Parcel IMPERVIOUS Parcel IMPERVIOUS Parcel Area = 5.51 acres Area = 5.53 acres CN = 98 S = 2.50 S = 0.20 0.25 = 0.04 Compute: Developed Conditions Rundfl hydrograph Column (3) = SCS Type IA Rainfall Distribution Column (3) = CoL (3) × P1 = 10 year. 24 Hour Myetograph at this location. Column (5) = CoL (3) × P1 = 0 year. 24 Hour Myetograph at this location. Column (5) = CoL (3) × P1 = 0 year. 24 Hour Myetograph at this location. Column (5) = CoL (3) = 0 Note, use PERVIOUS Area "5" value. (If P > 0.28) = (CoL (5) · 0.28)*2/(CoL (5) · 0.88); Using the PERVIOUS Area "5" value. Column (6) = Same method as for CoL (6), except use the IMPERVIOUS Area "5" value. Column (1) = (CPERVIOUS area / Total area) x CoL (7)) * ((IMPERVIOUS Area 7" value. Column (1) = (60 x CoL (10) x Trait Area) / 10 (41 = 10 minutes) Column (1) = (CA (2) of the present Time Step + 0x (2(Ca) (11) of Previous Time Step) Column (1) = CoL (8) CO (10) x Trait Area) / 10 (41 = 10 minutes) Column (1) = (CA (2) of the previous Time Step) Column (1) = CO (2) CO (10) x Trait Area) / 10 (41 = 10 minutes) Routing Constant, w = dt /	1	Date:	Nov-03	1.1.1	Section.		-	1.1.1.1				
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	(Given:	Project =		WOOD MS	S						
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			Area =	11.34	acres							
$ \begin{array}{cccc} dt & = & 10 \min. \\ Tc & = & 10 \min. (Post-Developed Site Conditions). \\ PERVIOUS Parcel IMPERVIOUS Parcel Area = 5.51 acres Area = 5.53 acres CN = 80 \\ S & = & 2.50 \ S = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.50 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.20 \ 0.25 & = & 0.20 \\ 0.25 & = & 0.20 \ 0.25 \ $			Pt =	3.45	inches	10-Year/	24 Hour S	Storm				
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$			dt =	10	min.							
PERVIOUS Parcel IMPERVIOUS Parcel Area = 5.51 acres Area = 5.83 acres CN = 80 CN = 98 S = 2.50 S = 0.20 0.25 = 0.50 0.25 = 0.04 Column (3) = SCS Type IA Rainfail Distribution Column (4) = Col. (3) x Pt = 10 year - 24 Hour Hyetograph at this location. Column (5) = Accumulated Sum of Col. (4) Column (6) = IIF P <= 0.28] = 0; Note, use PERVIOUS Area "S" value. Column (6) = IIF P <= 0.28] = (0; (6), except use the IMPERVIOUS Area "S" value. Column (7) = Col.(6) of Present Time Step - Col.(6) of Previous Time Step Column (8) = Same method as for Col.(6), except use the IMPERVIOUS area / Total area) x Col.(9)) Column (10) = ((PERVIOUS area / Total area) x Col.(7) + ((IMHERVIOUS area / Total area) x Col.(9)) Column (10) = ((PERVIOUS area / Total area) x Col.(7) + ((IMHERVIOUS area / Total area) x Col.(9)) Column (10) = ((PERVIOUS area / Total area) x Col.(10) of Previous Time Step + Col.(11) of Present Time Step - (2 x Col.(12) of Previous Time Step) + Col.(11) of Present Time Step - (2 x Col.(12) of Previous Time Step) + Col.(11) of Present Time Step - (2 x Col.(12) of Previous Time Step) + Col.(11) of Present Time Step - (2 x Col.(12) of Previous Time Step) + Col.(11) of Present Time Step - (2 x Col.(12) of Previous Time Step) + Col.(11) of Rainfail Runoff Runoff Runoff Runoff Runoff Runoff graph graph (1) (2) (3) (4) (5) (6) (7) (8) (9) (11) (12) Time Rainfail Innet ale Innet and Runof			Tc =	10	min. (Pos	st-Develope	ed Site Co	onditions)				
Area = 5.51 acres CN = 80 CN = 98 S = 2.50 S = 0.20 0.25 = 0.50 0.25 = 0.04 Compute: Developed Conditions Runoff hydrograph Column (3) = SCS Type IA Rainfall Distribution Column (6) = Col. (3) × PT = 10 year - 24 Hour Hyetograph at this location. Column (6) = Col. (3) × PT = 10 year - 24 Hour Hyetograph at this location. Column (6) = Col. (3) × PT = 10 year - 24 Hour Hyetograph at this location. Column (7) = Col. (6) P Present Time Step - Col. (6) of Previous Time Step Column (8) = Same method as for Col. (4) Column (7) = Col. (7) Present Time Step - Col. (6) of Previous Time Step Column (9) = Col. (8) Present Time Step - Col. (6) of Previous Time Step Column (10) = ((PERVIOUS area / Total area) × Col. (7) + ((IMPERVIOUS area / Total area) × Col. (9)) Column (12) = Col. (12) of Previous Time Step + (w x (Col. (11) of Previous Time Step) + Col. (11) of Present Time Step - (2 x Col. (12) of Previous Time Step) Time Rainfall Incer Total areal x Col. (7) (8) (9) (9) (10) (11) (12) Time Rainfall Incer Roundf Runoff Runoff Runoff Graph graph Incerment Math Nath Runoff Runoff Runoff Runoff Graph graph			PERVIOU	S Parcel		IMPERVIO	OUS Parc	el				
$ \begin{array}{cccc} {\sf CN} &= & 80 & {\sf CN} &= & 98 \\ {\sf S} &= & 2.50 & {\sf S} &= & 0.20 \\ {\sf 0.2S} &= & 0.50 & {\sf 0.2S} &= & 0.04 \\ \\ \hline \\ {\sf Compute: Developed Conditions Runoff hydrograph \\ {\sf Column} (3) = SCS Type IA Rainfall Distribution \\ {\sf Column} (4) = Col. (3) \times PI = 10 year - 24 Hour Hyetograph at this location. \\ {\sf Column} (5) = Accumutated Sum of Col. (4) \\ {\sf Column} (6) = [IP <= 0.2S] = (0.16) & {\sf 0.2S} \ {\sf value}. \\ {\sf Column} (5) = Accumutated Sum of Col. (4) \\ {\sf Column} (6) = [IP <= 0.2S] = (Col. (5) - 0.2S) \ {\sf value}. \\ {\sf Column} (7) = Col. (6) of Present Time Step - Col. (6) of Previous Time Step \\ {\sf Column} (9) = Col. (8) of the present time step - Col. (8) of the previous time step \\ {\sf Column} (9) = Col. (8) of the present time step - Col. (8) of the previous time step \\ {\sf Column} (10) = ((PERVIOUS area / Total area) \times Col. (7)) + ((IMPERVIOUS area / Total area) \times Col. (9)) \\ {\sf Column} (10) = (0.16) \ {\sf (0)} \ {\sf (10)} \ {\sf (11)} = (0.5 \cdot Col. (10) \times Total Area) / 10 \ {\sf (10)} \ {\sf (10)} \ {\sf (12)} \ {\sf (21)} \ {\sf (0)} \ {\sf (10)} \ {\sf (12)} \ {\sf (11)} \ {\sf (21)} \ {\sf (0)} \ {\sf (11)} \ {\sf (21)} \ {\sf (0)} \ {\sf (11)} \ {\sf (12)} \ {\sf (12)} \ {\sf (11)} \ {\sf (11)} \ {\sf (12)} \ {\sf (11)} \ {\sf (12)} \ {\sf (11)} \ {\sf (11)} \ {\sf (12)} \ {\sf (11)} \ {\sf (11)} \ {\sf (12)} \ {\sf (11)} \ {\sf (12)} \ {\sf (11)} \ {\sf (11)} \ {\sf (12)} \ {\sf (11)} \ {\sf (11)} \ {\sf (12)} \ {\sf (11)} \ {\sf (11)} \ {\sf (12)} \ {\sf (11)$			Area =	5.51	acres	Area =	5.83	acres				
S = 2.50 S = 0.20 0.25 = 0.50 0.25 = 0.04 Column (3) = SCS Type IA Rainfall Distrbution Column (5) = Accumulated Sum of Col. (4) Column (6) = Col. (3) × PT = 10 year - 24 Hour Hyetograph at this location. Column (5) = Accumulated Sum of Col. (4) Column (6) = I(P < - 0.25) = 0; Note use PERVIOUS Area "S" value. [f(P > 0.25) = 0; Olot use PERVIOUS Area "S" value. Column (7) = Col.(6) of Present Time Step - Col.(6) of Previous Time Step Column (8) = Same method as for Col. (6), except use the IMPERVIOUS area 7 trail area) × Col.(9) Column (10) = ((PERVIOUS area 1 Total area) × Col.(7) + ((IMPERVIOUS area 7 Total area) × Col.(9)) Column (10) = ((PERVIOUS area 1 Total area) × Col.(7) + ((IMPERVIOUS Time Step Column (10) = ((PERVIOUS area 1 Total area) × Col.(2) of Previous Time Step + Col.(11) of Present Time Step · (2 × Col.(12) of Previous Time Step) (1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (12) (1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (12) (1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (12) (11)			CN =	80		CN =	98					
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$ \begin{array}{c} Column (3) = SCS Type IA Rainfall Distribution \\ \mbox{Column (4) = Col. (3) \times Pt = 10 year - 24 Hour Hyetograph at this location. \\ \mbox{Column (5) = Accumulated Sum of Col. (4) \\ \mbox{Column (6) = [IF P < 0.2S] = 0; Note, use PERVIOUS Area "5" value. \\ \mbox{Column (7) = Col. (6) of Present Time Step - Col. (6) of Previous Time Step Col. (5) + 0.2S); Using the PERVIOUS Area "5" value. \\ \mbox{Column (7) = Col. (6) of the present Time Step - Col. (6) of Previous Time Step - Col. (6) of the present Time Step - Col. (6) of Previous Time Step - Col. (6) of the present Time Step - Col. (6) of the present Time Step - Col. (6) of Previous Time Step - Col. (6) of the present Time Step - Col. (7) of (10) = (10) Column (10) = ((12) Col. (7) of Area) / 10 (11) = 100. So Col. (7) + ((IMPERVIOUS area / Total area) \times Col. (9)) Column (11) = (60. So Col. (10) \times Total Area) / 10 (11) = 100. So Column (12) = Col. (12) of Previous Time Step + (w \times [Col. (11) of Previous Time Step + + Col. (11) of Present Time Step - (2 \times Col. (12) of Previous Time Step)) + + Col. (11) of Present Time Step - (2 \times Col. (12) of Previous Time Step)) + + Col. (11) of Present Time Step - (2 \times Col. (12) of Previous Time Step) + + Col. (11) of Previous Time Step) + + Col. (11) of Previous Time Step - (2 \times Col. (12) of Previous Time Step)) + + Col. (11) of Previous Time Step - (2 \times Col. (12) of Previous Time Step)) + + Col. (11) of Previous Time Step - (2 \times Col. (12) of Previous Time Step) + + Col. (11) of Previous Time Step) + + Col. (11) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12) of Previous Time Step - (2 \times Col. (12)$	(Compute:	Developed	Condition	s Runoff h	ydrograph						
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$ \begin{array}{c} \mbox{Column (5) = Accumulated Sum of Col. (4) \\ \mbox{Column (6) = [If $P < 0.2S] = 0; Note, use PERVIOUS Area "S" value. \\ \mbox{[If $P > 0.2S] = (Col.(5) - 0.2S)^{2/2}(Col.(5) + 0.8S); Using the PERVIOUS Area "S" value. \\ Column (7) = Col.(6) of Present Time Step - Col.(6) of Previous Time Step - Column (8) = Same method as for Col.(6), except use the IMPERVIOUS Area "S" value. \\ \mbox{Column (8) = Same method as for Col.(6), except use the IMPERVIOUS Area "S" value. \\ \mbox{Column (10) = ((PERVIOUS area / Total area) x Col.(7)) + ((IMPERVIOUS area / Total area) x Col.(9)) \\ \mbox{Column (11) = (60.5 x Col.(10) x Total Area) / 10 (dt = 10 minutes) \\ \mbox{Routing Constant, w = dt/(2Tc + dt) = 0.3333 \\ \mbox{Column (12) = Col.(12) of Previous Time Step + (w x [Col.(11) of Previous Time Step) \\ + Col.(11) of Present Time Step + (x x Col.(12) of Previous Time Step) \\ + Col.(11) of Present Time Step + (x x Col.(12) of Previous Time Step)] \\ \hline \mbox{Time Rainfall Incre- Accumu- Accumu- Incre- Accumu- Incre- Total Instant design mental lated mental lated mental kunoff Runoff graph graph min. % of Pt in. in. in. in. in. in. in. in. in. in.$			Column (4) = Col. (3	$) \times Pt = 10$	vear - 24 H	lour Hyeto	ograph at th	his location	1.		
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bution min. Rainfall % of Pt Rainfall in. Runoff in. Runoff in. <t< th=""><th>(1) Time</th><th>(2) Time</th><th>(3) Rainfall</th><th>(4)</th><th>(5) Accumu-</th><th>Pervious (6) Accumu-</th><th>(2 x Col.(Area (7) Incre-</th><th>12) of Prev Imperviou (8) Accumu-</th><th>vious Time Is Area (9) Incre-</th><th>(10) (10)</th><th>(11) Instant</th><th>(12) design</th></t<>	(1) Time	(2) Time	(3) Rainfall	(4)	(5) Accumu-	Pervious (6) Accumu-	(2 x Col.(Area (7) Incre-	12) of Prev Imperviou (8) Accumu-	vious Time Is Area (9) Incre-	(10) (10)	(11) Instant	(12) design
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	(1) Time Increment	(2) Time	(3) Rainfall distri- bution	(4) Incre- mental Rainfall	(5) Accumu- lated Rainfall	Pervious (6) Accumu- lated Runoff	(2 x Col.(Area (7) Incre- mental Runoff	12) of Prev Imperviou (8) Accumu- lated Runoff	vious Time us Area (9) Incre- mental Runoff	(10) Total Runoff	(11) Instant hydro- graph	(12) design hydro- graph
1 10 0.0040 0.0138 0.0138 0.0000 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0013 0.0138 0.0138 0.0000 0.0000 0.00177 0.0019 0.1 0.0 0.0013 0.1124 0.0006 0.00177 0.0029 0.2 0.7 9 90 0.0040 0.0138 0.1242 0.0000 0.00177 0.0037 0.3 0.2 0.7 11 110 0.	(1) Time Increment	(2) Time min.	(3) Rainfall distri- bution % of Pt	(4) Incre- mental Rainfall in.	(5) Accumu- lated Rainfall in.	Pervious (6) Accumu- lated Runoff in.	(2 x Col.(Area (7) Incre- mental Runoff in.	Imperviou (8) Accumu- lated Runoff in.	vious Time us Area (9) Incre- mental Runoff in.	(10) Total Runoff in.	(11) Instant hydro- graph cfs	(12) design hydro- graph cfs
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9 90 0.0040 0.0138 0.1242 0.0000 0.0242 0.0065 0.0033 0.2 0. 10 100 0.0040 0.0138 0.1380 0.0000 0.0000 0.0313 0.0072 0.0037 0.3 0.3 11 110 0.0050 0.0173 0.1553 0.0000 0.0000 0.0411 0.0098 0.0050 0.3 0.3 12 120 0.0050 0.0173 0.1725 0.0000 0.0000 0.0516 0.0105 0.0054 0.4 0.3 13 130 0.0050 0.0173 0.1898 0.0000 0.00628 0.0112 0.0058 0.4 0.3 14 140 0.0050 0.0173 0.2243 0.0000 0.0068 0.0122 0.0063 0.4 0.3 15 150 0.0050 0.0173 0.2415 0.0000 0.0995 0.0127 0.0065 0.4 0.4 16 160 0.0050 <t< td=""><td>(1) Time Increment 1 2 3 4 5 6 7</td><td>(2) Time min. 10 20 30 40 50 60 70</td><td>+ (3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040</td><td>(4) Incre- mental Rainfall in. 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138</td><td>(5) Accumu- lated Rainfall in. 0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966</td><td>ime Step - Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000</td><td>(2 x Col.(Area (7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000</td><td>Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0009 0.0034 0.0072 0.0120</td><td>vious Time Is Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0009 0.0025 0.0037 0.0048</td><td>(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0005 0.0013 0.0019 0.0025</td><td>(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.1 0.1 0.2</td><td>(12) design hydro- graph cfs 0.000 0.000 0.000 0.001 0.004 0.011 0.044 0.088 0.130</td></t<>	(1) Time Increment 1 2 3 4 5 6 7	(2) Time min. 10 20 30 40 50 60 70	+ (3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138	(5) Accumu- lated Rainfall in. 0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966	ime Step - Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(2 x Col.(Area (7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0009 0.0034 0.0072 0.0120	vious Time Is Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0009 0.0025 0.0037 0.0048	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0005 0.0013 0.0019 0.0025	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.1 0.1 0.2	(12) design hydro- graph cfs 0.000 0.000 0.000 0.001 0.004 0.011 0.044 0.088 0.130
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20 200 0.0060 0.0207 0.3243 0.0000 0.1648 0.0169 0.0087 0.6 0.5 21 210 0.0060 0.0207 0.3450 0.0000 0.1820 0.0172 0.0089 0.6 0.5 22 220 0.0060 0.0207 0.3657 0.0000 0.1995 0.0175 0.0090 0.6 0.6	(1) Time Increment 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180	+ (3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.00500000000	(4) Incre- mental Rainfall in. 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0133 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173	(5) Accumu- lated Rainfall in. 0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2215 0.2829	ime Step - Pervious (6) Accumulated Runoff in. 0.0000 0.00	(2 x Col.(Area (7) Incre- mental Runoff in. 0,0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0012 0.0051 0.0012 0.00510000000000	vious Time vious Time Is Area (9) Incre- mental Runoff in. 0.0000 0.0005 0.0005 0.0012 0.0012 0.0012 0.0012 0.0012 0.0012 0.0012 0.0012 0.0012 0.0012 0.0012 0.0012 0.0015 0.0112 0.0115 0.0112 0.0157 0.0	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0005 0.0013 0.0019 0.0025 0.0029 0.0033 0.0019 0.0025 0.0029 0.0033 0.0050 0.0054 0.0050 0.0054 0.0055 0.0063 0.0065 0.0081 0.0083	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.1 0.1 0.1 0.2 0.2 0.2 0.2 0.2 0.2 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.6 0.6	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000 0.000 0.001 0.004 0.004 0.030 0.130 0.130 0.130 0.130 0.130 0.130 0.227 0.275 0.330 0.365 0.392 0.413 0.430 0.430 0.430
21 210 0.0060 0.0207 0.3450 0.0000 0.1820 0.0172 0.0089 0.6 0.5 22 220 0.0060 0.0207 0.3657 0.0000 0.1995 0.0175 0.0090 0.6 0.6	(1) Time Increment 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	(2) Time min. 10 20 30 40 50 60 70 80 90 100 100 110 120 130 140 150 160 170 180 190	+ (3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.	(4) Incre- mental Rainfall in. 0.0138 0.0173 0.0173 0.0173 0.0173 0.0277 0.0277 0.0277	(5) Accumu- lated Rainfall in. 0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.11042 0.1242 0.1380 0.1553 0.1725 0.1725 0.1898 0.2070 0.2243 0.2071 0.2243 0.2415 0.2622 0.2829 0.3036	ime Step - Pervious (6) Accumulated Runoff in. 0.0000 0.00	(2 x Col.(Area (7) Incre- mental Runoff in. 0,0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0012 0.0011 0.00516 0.00688 0.0746 0.00868 0.0746 0.00868 0.0746 0.00868 0.0746 0.01152 0.01152 0.01152 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01110 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01120 0.01110 0.01100 0.011100 0.011100 0.011100 0.011100 0.011100000000	vious Time vious Time (9) Incre- mental Runoff in. 0.0000 0.0005 0.0007 0.0005 0.0012 0.0012 0.0112 0.0112 0.0112 0.0157 0.01	Step))) (10) Total Runoff in. 0.0000 0.0000 0.0000 0.0005 0.0013 0.0019 0.0025 0.0029 0.0033 0.0019 0.0025 0.0029 0.0033 0.0050 0.0054 0.0058 0.0060 0.0063 0.0063 0.0063 0.0081 0.0083 0.0085	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.1 0.1 0.1	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000 0.000 0.001 0.044 0.088 0.130 0.130 0.167 0.199 0.227 0.275 0.330 0.365 0.392 0.413 0.430 0.430 0.430 0.430
22 220 0.0060 0.0207 0.3657 0.0000 0.0000 0.1995 0.0175 0.0090 0.6 0.6	(1) Time Increment 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200	+ (3) Rainfall distri- bution % of Pt 0.0040 0.0050 0.	(4) Incre- mental Rainfall in. 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0133 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0207 0.0207	(5) Accumu- lated Rainfall in. 0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622 0.2829 0.3036 0.3243	ime Step - Pervious (6) Accumulated Runoff in. 0.0000 0.00	(2 x Col.(Area (7) Incre- mental Runoff in. 0.00000 0.0000 0.000000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00141 0.00516 0.00868 0.0095 0.01152	vious Time vious Time (9) Incre- mental Runoff in. 0.0000 0.0005 0.0005 0.0012 0.0012 0.0112 0.0112 0.0112 0.0112 0.0157 0.0157 0.0157 0.0112 0.0112 0.0157 0.0162 0.0157 0.0166 0.0169 0.0169	Step))) (10) Total Runoff in. 0.0000 0.0000 0.0000 0.0005 0.0013 0.0019 0.0025 0.0029 0.0033 0.0019 0.0025 0.0029 0.0033 0.0055 0.0054 0.0058 0.0060 0.0063 0.0065 0.0081 0.0083 0.0085 0.0087	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.1 0.1 0.2 0.2 0.2 0.2 0.2 0.2 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.6 0.6 0.6 0.6	(12) design hydro- graph cfs 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000
NAME AND	(1) Time Increment 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	(2) Time min. 10 20 30 40 50 60 70 80 90 100 100 110 120 130 140 150 160 170 180 190 200 210	+ (3) Rainfall distri- bution % of Pt 0.0040 0.0050 0.	(4) Incre- mental Rainfall in. 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0138 0.0133 0.0173 0.0173 0.0173 0.0173 0.0173 0.0173 0.0207 0.0207 0.0207	(5) Accumu- lated Rainfall in. 0.0138 0.0276 0.0414 0.0552 0.0690 0.0828 0.0966 0.1104 0.1242 0.1380 0.1553 0.1725 0.1898 0.2070 0.2243 0.2415 0.2622 0.2829 0.3036 0.3243 0.3450	ime Step - Pervious (6) Accumu- lated Runoff in. 0.00000 0.00000 0.00000	(2 x Col.(Area (7) Incre- mental Runoff in. 0.00000 0.0000 0.000000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0012 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00120 0.00141 0.00516 0.00868 0.0095 0.1152 0.01152	vious Time vious Time Is Area (9) Incre- mental Runoff in. 0.0000 0.0005 0.0005 0.0015 0.0010 0.0005 0.0012 0.0012 0.0012 0.0112 0.0112 0.0112 0.0112 0.0157 0.0122 0.0157 0.0112 0.0112 0.0157 0.0157 0.0157 0.0112 0.0157 0.0162 0.0169 0.0157 0.0169 0.0157 0.0169 0.0157 0.0169 0.0172 0.0157 0.0169 0.0172 0.0157 0.0	Step))) (10) Total Runoff in. 0.0000 0.0000 0.0000 0.0005 0.0013 0.0019 0.0025 0.0029 0.0033 0.0019 0.0025 0.0029 0.0033 0.0055 0.0054 0.0058 0.0060 0.0063 0.0065 0.0081 0.0083 0.0085 0.0087 0.0089	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.1 0.1 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.6 0.6 0.6 0.6 0.6	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000 0.000 0.001 0.004 0.008 0.130 0.130 0.130 0.130 0.130 0.167 0.227 0.275 0.330 0.365 0.392 0.430 0.430 0.430 0.430 0.430 0.430 0.430 0.430 0.430 0.430

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					Penvinus	Area	Impenvio	is Area				
(1) Time Increment	(2) Time	(3) Rainfall distri- bution	(4) Incre- mental Rainfall	(5) Accumu- lated Rainfall	(6) Accumu- lated Runoff	(7) Incre- mental Runoff	(8) Accumu- lated Runoff	(9) Incre- mental Runoff	(10) Total Runoff	(11) Instant hydro- graph	(12) design hydro- graph	
	min.		in.	In.	In.	<u>.</u>	in.	<u> </u>	ın.	CIS	CIS	
28	280	0.0070	0.0242	0.5106	0.0000	0,0000	0 3275	0.0219	0.0113	0.8	0 764	
20	200	0.0082	0.0292	0.5389	0.0006	0.0006	0.3533	0.0258	0.0135	0.0	0.822	
30	300	0.0082	0.0283	0.5672	0.0018	0.0012	0 3793	0.0260	0.0139	1.0	0.902	
31	310	0.0082	0.0283	0 5955	0.0035	0.0018	0 4055	0.0262	0.0143	1.0	0.946	
32	320	0.0082	0.0283	0.6238	0.0058	0.0023	0.4318	0.0263	0.0147	1.0	0.978	
33	330	0.0082	0.0283	0.6521	0.0087	0.0029	0 4582	0.0265	0.0150	1.0	1 004	
34	340	0.0082	0.0283	0.6803	0.0121	0.0034	0 4848	0.0266	0.0153	1.1	1 028	
35	350	0.0002	0.0200	0.7131	0.0167	0.0046	0.5157	0.0309	0.0181	1.2	1.108	
36	360	0.0095	0.0328	0.7459	0.0220	0.0053	0.5468	0.0311	0.0185	1.3	1.208	
30	300	0.0095	0.0328	0 7787	0.0220	0.0050	0.5780	0.0312	0.0189	13	1 259	
20	200	0.0095	0.0328	0.8114	0.02/5	0.0005	0.6093	0.0313	0.0193	13	1 293	
20	200	0.0095	0.0328	0.8442	0.0417	0.0000	0.6407	0.0314	0.0196	13	1 320	
39	390	0.0095	0.0320	0.0442	0.0417	0.0072	0.6721	0.0315	0.0100	1.4	1 345	
40	400	0.0095	0.0320	0.0770	0.0454	0.00110	0.7167	0.0315	0.0133	20	1 560	
41	410	0.0134	0.0462	0.9232	0.0013	0.0119	0.7612	0.0445	0.0207	2.0	1.000	
42	420	0.0134	0.0462	1.0167	0.0742	0.0129	0.7013	0.0447	0.0293	2.0	1.044	2.5
43	430	0.0134	0.0462	1.015/	0.0002	0.0140	0.8001	0.0448	0.0290	2.0	2 272	
44	440	0.0180	0.0021	1.0778	0.1085	0.0203	0.0004	0.0605	0.0409	2.0	2.212	
45	450	0.0180	0.0021	1.1399	0,1304	0.0219	1.0416	0.0000	0.0410	2.9	3.602	
40	460	0.0340	0.11/3	1.2372	0.1/00	0.0430	1.0410	0.1147	0.0011	0.0	6 153	-
47	470	0.0540	0.1803	1.4435	0.2565	0.0020	1.2240	0.1029	0.1341	9.2	0.1.15	Onale
48	480	0.0270	0.0932	1.5366	0.3038	0.0453	1.3102	0.0917	0.0092	4.7	0.700	Upeak
49	490	0.0180	0.0621	1.5987	0.3355	0.0310	1.3//5	0.0612	0.0400	3.2	4.007	10-1
50	500	0.0134	0.0462	1.6450	0.3597	0.0242	1.4231	0.0450	0.0352	2.4	3.505	1.10
51	510	0.0134	0.0462	1.0912	0.3644	0.0240	1.4000	0.0457	0.0355	2.4	2.700	Post
52	520	0.0134	0.0462	1.7374	0,4097	0.0253	1.5144	0.0457	0.0330	2.0	2.009	THEN
53	530	0.0088	0.0304	1.7678	0.4266	0.0169	1.5445	0.0300	0.0230	1.0	2.211	
54	540	0.0088	0.0304	1.7981	0.4437	0.0171	1.5/45	0.0300	0.0237	1.0	1.021	125
55	550	0.0088	0.0304	1.8285	0.4610	0.0173	1.6045	0.0300	0.0239	1.0	1.095	0.1
56	560	0.0088	0.0304	1.8589	0.4785	0.01/5	1.6346	0.0300	0.0240	1.0	1.659	10.
57	570	0.0088	0.0304	1.8892	0.4962	0.0177	1.6646	0.0301	0.0241	1.7	1.001	1.1.1.1.1
58	580	0.0088	0.0304	1.9196	0.5141	0.0179	1.6947	0.0301	0.0242	1.7	1.000	1.00
59	590	0.0088	0.0304	1.9499	0.5322	0.0181	1.7248	0.0301	0.0243	1.7	1.008	1
60	600	0.0088	0.0304	1.9803	0.5505	0.0183	1.7548	0.0301	0.0244	1.7	1.004	
61	610	0.0088	0.0304	2.0107	0.5690	0.0185	1.7849	0.0301	0.0244	1.7	1.6/1	
62	620	0.0088	0.0304	2.0410	0.5877	0.0187	1.8150	0.0301	0.0245	1./	1.6//	
63	630	0.0088	0.0304	2.0714	0.6065	0.0188	1.8451	0.0301	0.0246	1./	1.683	
64	640	0.0088	0.0304	2.1017	0.6255	0.0190	1.8752	0.0301	0.0247	1.7	1.689	
65	650	0.0072	0.0248	2.1266	0.6412	0.0157	1.8999	0.0246	0.0203	1.4	1.592	
66	660	0.0072	0.0248	2.1514	0.6569	0.0158	1.9245	0.0246	0.0203	1.4	1.460	A
67	670	0.0072	0.0248	2.1763	0.6728	0.0159	1.9492	0.0246	0.0204	1.4	1.418	
68	680	0.0072	0.0248	2.2011	0.6888	0.0160	1.9738	0.0247	0.0204	1.4	1.406	
69	690	0.0072	0.0248	2.2259	0.7049	0.0161	1.9985	0.0247	0.0205	1.4	1.405	
70	700	0.0072	0.0248	2.2508	0.7211	0.0162	2.0231	0.0247	0.0205	1.4	1.407	
71	710	0.0072	0.0248	2.2756	0.7374	0.0163	2.0478	0.0247	0.0206	1.4	1.410	
72	720	0.0072	0.0248	2.3005	0.7538	0.0164	2.0725	0.0247	0.0206	1.4	1.413	
73	730	0.0072	0.0248	2.3253	0.7703	0.0165	2.0971	0.0247	0.0207	1.4	1.417	
74	740	0.0072	0.0248	2.3501	0.7869	0.0166	2.1218	0.0247	0.0207	1.4	1.420	
75	750	0.0072	0.0248	2.3750	0.8036	0.0167	2.1465	0.0247	0.0208	1.4	1.423	
76	760	0.0072	0.0248	2.3998	0.8203	0.0168	2.1712	0.0247	0.0208	1.4	1.427	
77	770	0.0057	0.0197	2.4195	0.8337	0.0133	2.1907	0.0195	0.0165	1.1	1.330	
78	780	0.0057	0.0197	2.4392	0.8471	0.0134	2.2103	0.0195	0.0166	1.1	1.200	
79	790	0.0057	0.0197	2.4588	0.8605	0.0135	2.2298	0.0195	0.0166	1.1	1.158	
80	800	0.0057	0.0197	2.4785	0.8740	0.0135	2.2493	0.0195	0.0166	1.1	1.145	
81	810	0.0057	0.0197	2.4981	0.8876	0.0136	2,2689	0.0195	0.0166	1.1	1.142	

	1.40	- Call			Pervious	Area	Imperviou	is Area	Judu		
(1) Time ncrement	(2) Time	(3) Rainfall distri- bution	(4) Incre- mental Rainfall	(5) Accumu- lated Rainfall	(6) Accumu- lated Runoff	(7) Incre- mental Runoff	(8) Accumu- lated Runoff	(9) Incre- mental Runoff	(10) Total Runoff	(11) Instant hydro- graph	(12) design hydro- graph
	min,		in,	In.	10.	in.	in,	in,	10.	CIS	CIS
82	820	0.0057	0.0197	2.5178	0.9012	0.0136	2.2884	0.0196	0.0167	1.1	1.142
83	830	0.0057	0.0197	2.5375	0.9149	0.0137	2.3080	0.0196	0.0167	1.1	1.144
84	840	0.0057	0.0197	2.5571	0.9286	0.0137	2.3276	0.0196	0.0167	1.1	1.14
85	850	0.0057	0.0197	2.5768	0.9424	0.0138	2.3471	0.0196	0.0167	1.1	1.14
86	860	0.0057	0.0197	2.5965	0.9562	0.0138	2.3667	0.0196	0.0168	1.2	1.149
87	870	0.0057	0.0197	2.6161	0.9701	0.0139	2.3862	0.0196	0.0168	1.2	1.15
88	880	0.0057	0.0197	2.6358	0.9840	0.0139	2.4058	0.0196	0.0168	1.2	1.15
89	890	0.0050	0.0173	2.6531	0.9963	0.0123	2.4229	0.0172	0.0148	1.0	1.10
90	900	0.0050	0.0173	2.6703	1.0085	0.0123	2.4401	0.0172	0.0148	1.0	1.04
91	910	0.0050	0.0173	2.6876	1.0209	0.0123	2.4573	0.0172	0.0148	1.0	1.025
92	920	0.0050	0.0173	2.7048	1.0332	0.0124	2.4744	0.0172	0.0148	1.0	1.020
93	930	0.0050	0.0173	2.7221	1.0456	0.0124	2.4916	0.0172	0.0148	1.0	1.019
94	940	0.0050	0.0173	2.7393	1.0581	0.0124	2.5088	0.0172	0.0149	1.0	1.019
95	950	0.0050	0.0173	2.7566	1.0705	0.0125	2.5259	0.0172	0.0149	1.0	1.020
96	960	0.0050	0.0173	2.7738	1.0830	0.0125	2.5431	0.0172	0.0149	1.0	1.02
97	970	0.0050	0.0173	2.7911	1.0956	0.0125	2.5602	0.0172	0.0149	1.0	1.02
98	980	0.0050	0.0173	2.8083	1.1081	0.0126	2.5774	0.0172	0.0149	1.0	1.023
99	990	0.0050	0.0173	2.8256	1.1207	0.0126	2.5946	0.0172	0.0150	1.0	1.02
100	1000	0.0050	0.0173	2.8428	1.1334	0.0126	2.6118	0.0172	0.0150	1.0	1.02
101	1010	0.0040	0.0138	2.8566	1.1435	0.0101	2.6255	0.0137	0.0120	0.8	0.95
102	1020	0.0040	0.0138	2.8704	1.1537	0.0102	2.6392	0.0137	0.0120	0.8	0.86
103	1030	0.0040	0.0138	2.8842	1.1638	0.0102	2.6530	0.0137	0.0120	0.8	0.83
104	1040	0.0040	0.0138	2.8980	1.1740	0.0102	.2.6667	0.0137	0.0120	0.8	0.82
105	1050	0.0040	0.0138	2,9118	1.1842	0.0102	2.6804	0.0137	0.0120	0.8	0.82
106	1060	0.0040	0.0138	2.9256	1.1945	0.0102	2.6942	0.0137	0.0120	0.8	0.82
107	1070	0.0040	0.0138	2.9394	1.2047	0.0103	2.7079	0.0137	0.0120	0.8	0.820
108	1080	0.0040	0.0138	2.9532	1.2150	0.0103	2.7217	0.0137	0.0121	0.8	0.82
109	1090	0.0040	0.0138	2.9670	1.2253	0.0103	2.7354	0.0137	0.0121	0.8	0.82
110	1100	0.0040	0.0138	2.9808	1.2356	0.0103	2.7491	0.0137	0.0121	0.8	0.82
111	1110	0.0040	0.0138	2.9946	1.2460	0.0103	2.7629	0.0137	0.0121	0.8	0.82
112	1120	0.0040	0.0138	3.0084	1.2563	0.0104	2.7766	0.0137	0.0121	0.8	0.829
113	1130	0.0040	0.0138	3.0222	1.2667	0.0104	2.7904	0.0137	0.0121	0.8	0.830
114	1140	0.0040	0.0138	3.0360	1.2771	0.0104	2.8041	0.0137	0.0121	0.8	0.830
115	1150	0.0040	0.0138	3.0498	1.2875	0.0104	2.8179	0.0137	0.0121	0.8	0.83
116	1160	0.0040	0.0138	3.0636	1.2979	0.0104	2.8316	0.0137	0.0121	0.8	0.83
117	1170	0.0040	0.0138	3.0774	1.3083	0.0104	2.8454	0.0137	0.0121	0.8	0.83
118	1180	0.0040	0.0138	3.0912	1.3188	0.0105	2.8591	0.0137	0.0122	0.8	0.833
119	1190	0.0040	0.0138	3.1050	1.3293	0.0105	2.8728	0.0137	0.0122	0.8	0.83
120	1200	0.0040	0.0138	3.1188	1.3398	0.0105	2.8866	0.0137	0.0122	0.8.	0.83
121	1210	0.0040	0.0138	3.1326	1.3503	0.0105	2.9003	0.0137	0.0122	0.8	0.83
122	1220	0.0040	0.0138	3.1464	1.3608	0.0105	2.9141	0.0137	0.0122	0.8	0.83
123	1230	0.0040	0.0138	3.1602	1.3714	0.0106	2.9278	0.0137	0.0122	0.8	0.83
124	1240	0.0040	0.0138	3.1740	1.3820	0.0106	2.9416	0.0137	0.0122	0.8	0.83
125	1250	0.0040	0.0138	3.1878	1.3925	0.0106	2.9553	0.0137	0.0122	0.8	0.83
126	1260	0.0040	0.0138	3.2016	1.4032	0.0106	2.9691	0.0137	0.0122	0.8	0.83
127	1270	0.0040	0.0138	3.2154	1.4138	0.0106	2.9828	0.0137	0.0122	0.8	0.83
128	1280	0.0040	0.0138	3.2292	1.4244	0.0106	2.9966	0.0137	0.0122	0.8	0.83
129	1290	0.0040	0.0138	3.2430	1.4351	0.0107	3.0103	0.0138	0.0122	0.8	0.84
130	1300	0.0040	0.0138	3.2568	1.4457	0.0107	3.0241	0.0138	0.0123	0.8	0.84
131	1310	0.0040	0.0138	3.2706	1.4564	0.0107	3.0378	0.0138	0.0123	0.8	0.84
132	1320	0.0040	0.0138	3.2844	1.4671	0.0107	3.0516	0.0138	0.0123	0.8	0.84
133	1330	0.0040	0.0138	3.2982	1.4778	0.0107	3.0653	0.0138	0.0123	0.8	0.84
134	1340	0.0040	0.0138	3.3120	1.4886	0.0107	3.0791	0.0138	0.0123	0.8	0.84

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					Pervious	Area	Imperviou	is Area		4.5	
(1) Time	(2) Time	(3) Rainfall	(4) Incre-	(5) Accumu-	(6) Accumu-	(7) Incre-	(8) Accumu-	(9) Incre-	(10) Total	(11) Instant	(12) design
Increment		distri-	Deinfall	Deinfell	Ducoff	Dunoff	lated	nental	RUNOT	nyaro-	nyaro-
	mia	Dution	Raintali	Rainiali	Runon	Runon	Runon	Runon	in	graph	graph
	11001.	Second Second Second	111.		u					CIS	LIS
135	1350	0.0040	0.0138	3.3258	1.4993	0.0108	3.0928	0.0138	0.0123	0.8	0.843
136	1360	0.0040	0.0138	3.3396	1.5101	0.0108	3.1066	0.0138	0.0123	0.8	0.843
137	1370	0.0040	0.0138	3.3534	1.5209	0.0108	3.1203	0.0138	0.0123	0.8	0.844
138	1380	0.0040	0.0138	3.3672	1.5317	0.0108	3.1341	0.0138	0.0123	0.8	0.845
139	1390	0.0040	0.0138	3.3810	1.5425	0.0108	3.1479	0.0138	0.0123	0.8	0.845
140	1400	0.0040	0.0138	3.3948	1.5533	0.0108	3.1616	0.0138	0.0123	0.8	0.846
141	1410	0.0040	0.0138	3.4086	1.5642	0.0108	3.1754	0.0138	0.0123	0.8	0.846
142	1420	0.0040	0.0138	3.4224	1.5750	0.0109	3.1891	0.0138	0.0123	0.8	0.847
143	1430	0.0040	0.0138	3.4362	1.5859	0.0109	3.2029	0.0138	0.0124	0.8	0.847
144	1440	0.0040	0.0138	3.4500	1.5968	0.0109	3.2166	0.0138	0.0124	0.8	0.848
								Total Vo	lume of R	unoff =	99502.298 cu. ft.
							(cu.ft.)	(Found to multiply convers SUM(Q in cubic V = SUN = (cu.ft/s)	by summin ing by 600 ion require) in cfs to 1 feet as fo M(Q) x dt x (10 min	ng this colu b. 600 is the ed to conve total volum llows: .) x (60 s/m	mn and ent e nin.)
							X				

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	Date:	37945.00	P	OND ROUTING						
1	Given:		Project = W	OOD MS - 10-YEAR						
	Aver	age Pond L	ength (ft) =	120.000		System:	Pond 120' I	ong x 50'	wide	
	Ave	rage Pond	Width (ft) =	50.000						
	C	Drifice 1 Dia	meter (ft) =	0.550						
	c	Drifice 2 Dia	meter (ft) =	1.000						
		Height to	Orifice 2 =	1.650						
				2000 A 200						
		Orifice 2 Are	a	0.785 SF						
		Orifice 1 Are	a =	0.238 SF						
		Avg Pond Al	Col At \$ 600	= Incremental CES into P	bnd					
		Column (4) =	= Starting Pon	d Deoth = Previous Remain	ing Pond	Depth = Cr	51 (11)			
		Column (5) =	= = 2 * a * Startir	na h	ing rond	Dopin - Ot	5(())			
		Column (7) =	= g otorin	of 2ob						
		Column (8) =	= Incremental	Vol out = Col (7) * 0.60 * O	ifice Area	* 600				
		Column (9) =	= Delta Vol = li	ncremental Vol in - Increme	ental Vol o	ut = Col (3)	- Col (8)			
		Column (10)	= Remaining	Pond Vol = Previous Rema	ining Vol	+ Col (9)				
		Column (11)	= Pond Denth	at End of Interval = Col (.)	/ Pond A	rea				
		Column (12)	= Pond CFS	Discharge = $Col(8) / 600$						
			aller.	Ver		1.1	224			- 000
(1)	(2)	(3)	(4)	(6)	(7)	(8)	(6a)			(9)
(1) Time	(2) Time	(3) Increm.	(4) Starting	(6)	(7)	(8) (Increm.	(6a)			(9) Delta
(1) Time Icrem.	(2) Time	(3) Increm. Vol into	(4) Starting Pond	(6)	(7)	(8) Increm. Vol 1 out	(6a)			(9) Delta Vol
(1) Time Increm.	(2) Time	(3) Increm. Vol into Pond	(4) Starting Pond Depth	(6)	(7)	(8) Increm. Vol 1 out Pond	(6a)			(9) Delta Vol
(1) Time Icrem.	(2) Time min.	(3) Increm. Vol into Pond cf	(4) Starting Pond Depth ft.	(6)	(7)	(8) Increm. Vol 1 out Pond cf	(6a)			(9) Delta Vol
(1) Fime Increm.	(2) Time <u>min.</u> 10	(3) Increm. Vol into Pond cf 0.00	(4) Starting Pond Depth ft. 0.000	(6)	(7)	(8) Increm. Vol 1 out Pond cf 0,000	(6a) -106.26	0.000	0.000	(9) Delta Vol cf
(1) Fime Iccrem.	(2) Time min. 10 20	(3) Increm. Vol into Pond cf 0.00 0.00	(4) Starting Pond Depth ft. 0.000 0.000	(6) 0.000 0.000	(7) 0.000 0.000	(8) Increm. Vol 1 out Pond cf 0,000 0,000	(6a) -106.26 -106.26	0.000	0.000	(9) Delta Vol cf 0.00
(1) Fime crem. 1 2 3	(2) Time min. 10 20 30	(3) Increm. Vol into Pond cf 0.00 0.00 0.01	(4) Starting Pond Depth ft. 0.000 0.000 0.000	(6) 0.000 0.000 0.000	(7) 0.000 0.000 0.000	(8) Increm. Vol 1 out Pond cf 0,000 0,000 0,000	(6a) -106.26 -106.26 -106.26	0.000 0.000 0.000	0.000 0.000 0.000	.(9) Delta Vol cf 0.00 0.00
(1) Fime crem. 1 2 3 4	(2) Time min. 10 20 30 40	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68	(4) Starting Pond Depth ft. 0.000 0.000 0.000 0.000	(6) 0.000 0.000 0.000 0.000	(7) 0.000 0.000 0.000 0.011	(8) Increm. Vol 1 out Pond cf 0,000 0,000 0,000 0,000 0,960	-106.26 -106.26 -106.26 -106.26	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	.(9) Delta Vol cf 0.00 0.01 5.72
(1) ime crem. 1 2 3 4 5	(2) Time min. 10 20 30 40 50	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68 26.34	(4) Starting Pond Depth ft. 0.000 0.000 0.000 0.000 0.000	(6) 0.000 0.000 0.000 0.000 0.000 0.000	(7) 0.000 0.000 0.000 0.011 0.248	(8) Increm. Vol 1 out Pond cf 0,000 0,000 0,000 0,000 0,960 21,222	-106.26 -106.26 -106.26 -106.26 -106.20	0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12
(1) Time crem. 1 2 3 4 5 6	(2) Time min. 10 20 30 40 50 60	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68 26.34 52.63	(4) Starting Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.002	(6) 0.000 0.000 0.000 0.000 0.062 0.117	(7) 0.000 0.000 0.001 0.248 0.341	(8) Increm. Vol 1 out Pond cf 0,000 0.000 0.000 0.960 21,222 29,195	-106.26 -106.26 -106.26 -106.26 -106.20 -106.14	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44
(1) Time crem. 1 2 3 4 5 6 7	(2) Time min. 10 20 30 40 50 60 70	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68 26.34 52.63 77.89	(4) Starting Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.002 0.006	(6) 0.000 0.000 0.000 0.000 0.000 0.062 0.117 0.368	(7) 0.000 0.000 0.001 0.248 0.341 0.607	(8) Increm. Vol 1 out Pond cf 0,000 0.000 0.000 0.000 0.960 21,222 29,195 51,890	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00
(1) Time crem. 1 2 3 4 5 6 7 8	(2) Time min. 10 20 30 40 50 60 70 80	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68 26.34 52.63 77.89 100.24	(4) Starting Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.002 0.006 0.010	(6) 0.000 0.000 0.000 0.062 0.117 0.368 0.647	(7) 0.000 0.000 0.001 0.248 0.341 0.607 0.804	(8) Increm. Vol 1 out Pond cf 0,000 0.000 0.000 0.960 21,222 29,195 51,890 68,806	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.42
(1) Time crem. 1 2 3 4 5 6 7 8 9	(2) Time min. 10 20 30 40 50 60 70 80 90	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56	(4) Starting Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.002 0.006 0.010 0.015	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985	(7) 0.000 0.000 0.000 0.011 0.248 0.341 0.607 0.804 0.992	(8) Increm. Vol 1 out Pond cf 0,000 0.000 0.000 0.960 21,222 29,195 51,890 68,806 84,868	(6a) -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69
(1) Time crem. 1 2 3 4 5 6 7 8 9 10	(2) Time min. 10 20 30 40 50 60 70 80 90 100	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20	(4) Starting Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.002 0.006 0.010 0.015 0.021	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357	(7) 0.000 0.000 0.001 0.248 0.341 0.607 0.804 0.992 1.165	(8) Increm. Vol 1 out Pond cf 0,000 0.000 0.000 0.960 21,222 29,195 51,890 68,806 84,868 99,632	(6a) -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.54
(1) Time crem. 1 2 3 4 5 6 7 8 9 10 11	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80	(4) Starting Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.002 0.006 0.010 0.010 0.021 0.027	(6) 0.000 0.000 0.000 0.000 0.000 0.002 0.117 0.368 0.647 0.985 1.357 1.749	(7) 0.000 0.000 0.001 0.248 0.341 0.607 0.804 0.992 1.165 1.323	(8) Increm. Vol 1 out Pond cf 0,000 0.000 0.000 0.960 21,222 29,195 51,890 68,806 84,868 99,632 113,126	(6a) -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.65 36.56 51.67
(1) fime crem. 1 2 3 4 5 6 7 8 9 10 11 12	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10	(4) Starting Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.002 0.006 0.010 0.010 0.021 0.027 0.036	(6) 0.000 0.000 0.000 0.000 0.000 0.002 0.117 0.368 0.647 0.985 1.357 1.749 2.304	(7) 0.000 0.000 0.001 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518	(8) Increm. Vol 1 out Pond cf 0.000 0.000 0.000 0.960 21.222 29.195 51.890 68.806 84.868 99.632 113.126 129.827	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27
(1) fime crem. 1 2 3 4 5 6 7 8 9 10 11 12 13	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26	(4) Starting Pond Depth ft. 0.000 0.001 0.002 0.005 0.010 0.021 0.027 0.036 0.047 0.04	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037	(7) 0.000 0.000 0.001 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743	(8) Increm. Vol 1 out Pond cf 0,000 0,000 0,000 0,000 21,222 29,195 51,890 68,806 84,868 99,632 113,126 129,827 149,049	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -105.28 -104.51 -103.96 -103.22	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21
(1) fime crem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93	(4) Starting Pond Depth ft. 0.000 0.002 0.002 0.021 0.021 0.021 0.021 0.021 0.027 0.021 0.027 0.036 0.027 0.036 0.047 0.027 0.036 0.047 0.027 0.036 0.047 0.027 0.036 0.047 0.027 0.036 0.047 0.059 0.047 0.059 0.05	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790	(7) 0.000 0.000 0.001 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.518	(8) Increm. Vol 1 out Pond cf 0,000 0.000 0.000 0.960 21,222 29,195 51.890 68.806 84.868 99.632 113.126 129.827 149.049 166.519	(6a) -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.22 -102.47	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41
(1) fime crem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150	(3) Increm. Vol into Pond cf 0.00 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59	(4) Starting Pond Depth ft. 0.000 0.001 0.002 0.021 0.021 0.027 0.036 0.047 0.035 0.047 0.059 0.070	(6) 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790 4.525	(7) 0.000 0.000 0.001 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.127	(8) Increm. Vol 1 out Pond cf 0,000 0.000 0.000 0.960 21,222 29,195 51.890 68.806 84.868 99.632 113.126 129.827 149.049 166.519 181,933	(6a) -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.22 -102.47 -101.74	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65
(1) fime crem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27	(4) Starting Pond Depth ft. 0.000 0.001 0.002 0.006 0.011 0.027 0.036 0.047 0.059 0.070 0.070 0.070 0.059 0.070 0.070 0.070 0.027 0.036 0.070 0.070 0.059 0.070 0.070 0.070 0.070 0.027 0.036 0.070 0.070 0.070 0.036 0.070 0.070 0.059 0.070 0.070 0.070 0.070 0.059 0.070 0.070 0.070 0.070 0.070 0.070 0.070 0.059 0.070 0.081 0.000 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.081 0.000 0.081 0.000 0.081 0.000 0.000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000000	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790 4.525 5.229	(7) 0.000 0.000 0.000 0.011 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.518 1.743 1.947 2.127 2.287	(8) Increm. Vol 1 out Pond cf 0,000 0.000 0.000 0.960 21.222 29.195 51.890 68.806 84.868 99.632 113.126 129.827 149.049 166.519 181.933 195.588	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.96 -102.47 -101.74 -101.74 -101.03	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 62.69
(1) Fime crem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27 286.17	(4) Starting Pond Depth ft. 0.000 0.001 0.002 0.001 0.021 0.027 0.036 0.047 0.059 0.070 0.081 0.092	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790 4.525 5.229 5.902	(7) 0.000 0.000 0.000 0.011 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.287 2.287 2.287	(8) Increm. Vol 1 out Pond cf 0,000 0.000 0.960 21.222 29.195 51.890 68.806 84.868 99.632 113.126 129.827 149.049 166.519 181.933 195.588 207.789	(6a) -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.96 -102.47 -101.03 -100.36	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 62.68 78.38
(1) Fime crem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27 286.17 320.09	(4) Starting Pond Depth ft. 0.000 0.001 0.002 0.006 0.010 0.021 0.027 0.036 0.047 0.059 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.095 0.070 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.095 0.092 0.095 0.092 0.095 0.081 0.092 0.095 0.092 0.095 0.092 0.095 0.092 0.092 0.095 0.092 0.092 0.095 0.092 0.095 0.092 0.095 0.092 0.095 0.092 0.095 0.095 0.095 0.092 0.095 0.055 0.05	(6) 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 1.749 2.304 3.037 3.790 4.525 5.229 5.902 6.743	(7) 0.000 0.000 0.000 0.011 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.127 2.287 2.287 2.287 2.597	(8) Increm. Vol 1 out Pond cf 0.000 0.000 0.960 21.222 29.195 51.890 68.806 84.868 99.632 113.126 129.827 149.049 166.519 181.933 195.588 207.789 222.105	(6a) -106.26 -106.26 -106.26 -106.20 -106.14 -105.28 -105.61 -105.28 -104.90 -104.51 -103.96 -103.96 -103.22 -102.47 -101.74 -101.03 -100.36 -99.52	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 68.27 70.21 68.41 65.65 878.38 97.98
(1) Fime crem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27 286.17 320.09 337.51	(4) Starting Pond Depth ft. 0.000 0.001 0.002 0.006 0.010 0.027 0.036 0.047 0.059 0.070 0.081 0.092 0.081 0.092 0.081 0.092 0.081 0.092 0.070 0.081 0.092 0.070 0.081 0.092 0.005 0.071 0.025 0.021 0.025 0.105 0.105 0.105 0.105 0.121 0.105 0.121	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790 4.525 5.229 5.902 6.743 7.795	(7) 0.000 0.000 0.000 0.011 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.127 2.287 2.287 2.597 2.597 2.792	(8) Increm. Vol 1 out Pond cf 0.000 0.000 0.960 21.222 29.195 51.890 68.806 84.868 99.632 113.126 129.827 149.049 166.519 181.933 195.588 207.789 222.105 238.797	(6a) -106.26 -106.26 -106.26 -106.20 -106.14 -105.28 -105.61 -105.28 -104.90 -104.51 -103.96 -103.22 -102.47 -101.74 -101.03 -100.36 -99.52 -98.46	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 62.68 78.38 97.98 98.71
(1) Fime icrem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27 266.17 320.09 337.51 348.63	(4) Starting Pond Depth ft. 0.000 0.001 0.027 0.036 0.047 0.059 0.070 0.081 0.092 0.105 0.121 0.092 0.105 0.121 0.029 0.105 0.121 0.029 0.105 0.121 0.029 0.105 0.121 0.029 0.105 0.121 0.029 0.105 0.121 0.029 0.105 0.121 0.027 0.135 0.121 0.029 0.105 0.121 0.027 0.135 0.121 0.027 0.036 0.121 0.029 0.105 0.121 0.125 0.121 0.125 0.121 0.027 0.036 0.121 0.027 0.135 0.121 0.121 0.127 0.125 0.121 0.127 0.125 0.121 0.127 0.125 0.121 0.127 0.127 0.125 0.121 0.127 0.12	(6) 0.000 0.000 0.000 0.002 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790 4.525 5.229 5.902 6.743 7.795 8.855	(7) 0.000 0.000 0.000 0.011 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.127 2.287 2.429 2.597 2.597 2.792 2.976	(8) Increm. Vol 1 out Pond cf 0.000 0.000 0.960 21.222 29.195 51.890 68.806 84.868 99.632 113.126 129.827 149.049 166.519 181.933 195.588 207.789 222.105 238.797 254.509	(6a) -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.22 -102.47 -101.74 -101.03 -100.36 -99.52 -98.46 -97.41	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 62.68 78.38 97.98 98.71 94.13
(1) Fime icrem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27 286.17 320.09 337.51 348.63 357.00	(4) Starting Pond Depth ft. 0.000 0.001 0.002 0.006 0.010 0.027 0.036 0.047 0.059 0.070 0.081 0.092 0.005 0.021 0.059 0.021 0.092 0.005 0.010 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.021 0.025 0.121 0.025 0.121 0.125 0.121 0.125 0.121 0.125 0.121 0.125 0.121 0.125 0.121 0.125 0.121 0.125 0.121 0.137 0.153	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790 4.525 5.229 5.902 6.743 7.795 8.855 9.865	(7) 0.000 0.000 0.000 0.011 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.127 2.287 2.429 2.597 2.792 2.597 2.976 3.141	(8) Increm. Vol 1 out Pond cf 0.000 0.000 0.960 21.222 29.195 51.890 68.806 84.868 99.632 113.126 129.827 149.049 166.519 181.933 195.588 207.789 222.105 238.797 254.509 268.636	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.22 -102.47 -101.74 -101.03 -100.36 -99.52 -98.46 -97.41 -96.40	0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 62.68 78.38 97.98 98.71 94.13 88.36
(1) Fime icrem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27 286.17 320.09 337.51 348.63 357.00 363.88	(4) Starting Pond Depth ft. 0.000 0.001 0.027 0.036 0.047 0.059 0.070 0.081 0.092 0.105 0.121 0.092 0.105 0.121 0.027 0.036 0.105 0.105 0.121 0.092 0.105 0.121 0.153 0.153 0.153 0.153 0.168	(6) 0,000 0,000 0,000 0,000 0,002 0,117 0,368 0,647 0,985 1,357 1,749 2,304 3,037 3,790 4,525 5,229 5,902 6,743 7,795 8,855 9,865 10,813	(7) 0.000 0.000 0.000 0.011 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.127 2.287 2.429 2.597 2.792 2.976 3.141 3.288	(8) Increm. Vol 1 out Pond cf 0.000 0.000 0.960 21.222 29.195 51.890 68.806 84.868 99.632 113.126 129.827 149.049 166.519 181.933 195.588 207.789 222.105 238.797 254.509 268.636 281 253	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.22 -102.47 -101.74 -101.03 -100.36 -99.52 -98.46 -97.41 -96.40 -95.45	0.000 0.000	0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 62.68 97.98 98.71 94.13 88.36 82.67
(1) Fime icrem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27 286.17 320.09 337.51 348.63 357.00 363.88 390.81	(4) Starting Pond Depth ft. 0.000 0.001 0.027 0.036 0.047 0.059 0.070 0.081 0.092 0.105 0.121 0.092 0.105 0.121 0.137 0.153 0.168 0.182	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790 4.525 5.229 5.902 6.743 7.795 8.855 9.865 10.813 11.700	(7) 0.000 0.000 0.000 0.011 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.127 2.287 2.429 2.597 2.792 2.976 3.141 3.288 3.421	(8) Increm. Vol 1 out Pond cf 0.000 0.000 0.960 21.222 29.195 51.890 68.806 84.868 99.632 113.126 129.827 149.049 166.519 181.933 195.588 207.789 222.105 238.797 254.509 268.636 281.253 292.560	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.22 -102.47 -101.74 -101.03 -100.36 -99.52 -98.46 -97.41 -96.40 -95.45 -94.56	0.000 0.000	0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 62.68 78.38 97.98 98.71 94.13 88.36 82.63 98.25
(1) Fime icrem. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27 286.17 320.09 337.51 348.63 357.00 363.88 390.81 424.52	(4) Starting Pond Depth ft. 0.000 0.001 0.027 0.036 0.047 0.059 0.070 0.081 0.092 0.105 0.121 0.092 0.105 0.121 0.137 0.153 0.168 0.182 0.198	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790 4.525 5.229 5.902 6.743 7.795 8.855 9.865 10.813 11.700 12.755	(7) 0.000 0.000 0.000 0.011 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.127 2.287 2.429 2.597 2.792 2.976 3.141 3.288 3.421 3.571	(8) Increm. Vol 1 out Pond cf 0,000 0,000 0,000 0,960 21,222 29,195 51,890 68,806 84,868 99,632 113,126 129,827 149,049 166,519 181,933 195,588 207,789 222,105 238,797 254,509 268,636 281,253 292,560	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.22 -102.47 -101.74 -101.03 -100.36 -99.52 -98.46 -97.41 -96.40 -95.45 -93.51	0.000 0.000	0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 62.68 78.38 97.98 98.71 94.13 88.36 82.63 98.25
(1) Time increm. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27 286.17 320.09 337.51 348.63 357.00 363.88 390.81 424.52 439.57	(4) Starting Pond Depth ft. 0.000 0.001 0.027 0.036 0.047 0.059 0.070 0.081 0.092 0.105 0.121 0.027 0.137 0.153 0.168 0.182 0.198 0.218	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790 4.525 5.229 5.902 6.743 7.795 8.855 9.865 10.813 11.700 12.755 14.033	 (7) 0.000 0.000 0.000 0.001 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.127 2.287 2.429 2.597 2.792 2.976 3.141 3.288 3.421 3.571 3.746 	(8) Increm. Vol 1 out Pond cf 0,000 0,000 0,000 0,960 21,222 29,195 51,890 68,806 84,868 99,632 113,126 129,827 149,049 166,519 181,933 195,588 207,789 222,105 238,797 254,509 268,636 281,253 292,560 305,460 320,397	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.22 -102.47 -101.74 -101.03 -100.36 -99.52 -98.46 -97.41 -96.40 -95.45 -94.56 -93.51 -92.22	0.000 0.000	0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 62.68 78.38 97.98 98.71 94.13 88.36 82.63 98.25 119.05
(1) Time increm. 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 24 25 25 25 25 25 25 25 25 25 25	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 250	(3) Increm. Vol into Pond cf 0.00 0.01 6.68 26.34 52.63 77.89 100.24 119.56 136.20 164.80 198.10 219.26 234.93 247.59 258.27 286.17 320.09 337.51 348.63 357.00 363.88 390.81 424.52 439.57	(4) Starting Pond Depth ft. 0.000 0.001 0.027 0.036 0.047 0.059 0.070 0.081 0.092 0.105 0.121 0.137 0.153 0.168 0.182 0.238 0.238	(6) 0.000 0.000 0.000 0.000 0.062 0.117 0.368 0.647 0.985 1.357 1.749 2.304 3.037 3.790 4.525 5.229 5.902 6.743 7.795 8.855 9.865 10.813 11.700 12.755 14.033 45.212	 (7) 0.000 0.000 0.000 0.001 0.248 0.341 0.607 0.804 0.992 1.165 1.323 1.518 1.743 1.947 2.127 2.287 2.429 2.597 2.792 2.976 3.141 3.288 3.421 3.571 3.746 3.912 	(8) Increm. Vol 1 out Pond cf 0,000 0,000 0,000 0,960 21,222 29,195 51,890 68,806 84,868 99,632 113,126 129,827 149,049 166,519 181,933 195,588 207,789 222,105 238,797 254,509 268,636 281,253 292,560 305,460 320,397	(6a) -106.26 -106.26 -106.26 -106.26 -106.20 -106.14 -105.89 -105.61 -105.28 -104.90 -104.51 -103.96 -103.22 -102.47 -101.74 -101.03 -102.47 -101.74 -101.36 -99.52 -98.46 -97.41 -96.40 -95.45 -94.56 -93.51 -92.23 -90.96	0.000 0.000	0.000 0.000	(9) Delta Vol cf 0.00 0.01 5.72 5.12 23.44 26.00 31.44 34.69 36.56 51.67 68.27 70.21 68.41 65.65 62.68 78.38 97.98 98.71 94.13 88.36 82.63 98.25 119.06 119.17
(1) Time Increm.	(2) Time	(3) Increm. Vol into Pond	(4) Starting Pond Depth	(6)	(7)	(8) Increm. Vol out Pond				(9) Delta Vol
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	min.	cf	ft.			cf				cf
28	280	458.60	0.274	17.665	4.203	359.484	-88.59	0.000	0.000	99.1
29	290	492.99	0.291	18.729	4.328	370.150	-87.53	0.000	0.000	122.84
30	300	541.11	0.311	20.048	4.477	382.957	-86.21	0.000	0.000	158.16
31	310	567.74	0.338	21,745	4.663	398.841	-84.51	0.000	0.000	168.90
32	320	586.66	0.366	23.558	4.854	415.134	-82.70	0.000	0.000	171.53
33	330	602.52	0.394	25.399	5.040	431.050	-80.86	0.000	0.000	171.4
34	340	616.91	0.423	27.240	5.219	446.394	-79.02	0.000	0.000	170.5
35	350	664.79	0.451	29.070	5.392	461.147	-77.19	0.000	0.000	203.6
36	360	724.80	0.485	31.255	5.591	478.170	-75.00	0.000	0.000	246.6
37	370	755.39	0.526	33.903	5.823	498.007	-72.36	0.000	0.000	257.39
38	380	775.69	0.569	36.665	6.055	517.900	-69.59	0.000	0.000	257.79
39	390	792.09	0.612	39.432	6.280	537.086	-66.83	0.000	0.000	255.0
40	400	806.78	0.655	42.169	6.494	555.414	-64.09	0.000	0.000	251.3
41	410	935.82	0.697	44,867	6.698	572,906	-61.39	0.000	0.000	362.9
42	420	1106.59	0.757	48.763	6.983	597.258	-57.50	0.000	0.000	509.3
43	430	1179.29	0.842	54.229	7.364	629.848	-52.03	0.000	0.000	549.44
44	440	1362.98	0.934	60.127	7.754	663.212	-46.13	0.000	0.000	699.7
45	450	1588.21	1.050	67.638	8.224	703.417	-38.62	0.000	0.000	884.79
46	460	2215.43	1.198	77.134	8.783	751.178	-29.13	0.000	0.000	1464.2
47	470	3691.63	1.442	92.851	9.636	824.159	-13.41	0.000	0.000	2867.47
48	480	4020.13	1.920	123.628	11.119	950.993	17.37	4.168	1178.340	1890.8
49	490	2932.14	2.235	143.923	11.997	********	37.66	6.137	1735.199	170.8
50	500	2103.29	2.263	145.757 .	12.073	********	39.50	6.285	1776.942	-706.2
51	510	1671.43	2.146	138.176	11.755	*******	31.92	5.649	1597.345	-931.3
52	520	1535.10	1.990	128.180	11.322	968.343	21.92	4.682	1323.776	-757.02
53	530	1326.86	1.864	120.055	10.957	937.149	13.79	3.714	1050.148	-660.43
54	540	1092.43	1.754	112.966	10.629	909.061	6.71	2.590	732.198	-548.83
55	550	1017.26	1.663	107.075	10.348	885.041	0.82	0.903	255.300	-123.00
56	560	995.12	1.642	105.754	10.284	879.565	-0.51	0.000	0.000	115.5
57	570	990.58	1.661	106.995	10.344	884.708	0.73	0.857	242.337	-136.40
58	580	991.84	1.639	105.530	10.273	878.631	-0.73	0.000	0.000	113.2
59	590	994.96	1.658	106.745	10.332	883.675	0.49	0.696	196.910	-85.62
60	600	998.64	1.643	105.826	10.287	879.863	-0.43	0.000	0.000	118.78
61	610	1002.45	1.663	107.101	10.349	885.147	0.84	0.917	259.279	-141.98
62	620	1006.23	1.639	105.577	10.275	878.827	-0.68	0.000	0.000	127.4
63	630	1009.95	1.661	106.944	10.341	884.500	0.68	0.827	233.924	-108.47
64	640	1013.59	1.643	105,780	10.285	879.672	-0.48	0.000	0.000	133.93
65	650	955.21	1.665	107.218	10.355	885.629	0.96	0.979	276.689	-207.1
66	660	875.73	1.630	104.995	10.247	876.400	-1.27	0.000	0.000	-0.6
67	670	850.74	1.630	104.987	10.246	876.370	-1.27	0.000	0.000	-25.63
68	680	843.90	1.626	104.712	10.233	875.221	-1.55	0.000	0.000	-31.33
69	690	843.07	1.621	104.376	10.216	873.815	-1.88	0.000	0.000	-30.7
70	700	844.22	1.616	104.046	10.200	872.432	-2.21	0.000	0.000	-28.2
71	710	846.01	1.611	103.743	10.185	871.162	-2.52	0.000	0.000	-25.1
72	720	847.98	1.607	103.473	10.172	870.028	-2.79	0.000	0.000	-22.04
73	730	850.00	1.603	103.237	10.161	869.033	-3.02	0.000	0.000	-19.04
74	740	852.00	1.600	103.032	10.150	868.172	-3.23	0.000	0.000	-16.18
75	750	853.97	1.597	102.859	10.142	867.440	-3.40	0.000	0.000	-13.4
76	760	855.91	1.595	102.714	10.135	866.830	-3.55	0.000	0.000	-10.9
77	770	798.07	1.593	102.597	10.129	866.336	-3.66	0.000	0.000	-68.2
78	780	720.04	1.582	101.864	10.093	863,237	-4.40	0.000	0.000	-143.19
79	790	694.80	1.558	100.327	10.016	856.700	-5.93	0.000	0.000	-161.90
80	800	687.15	1.531	98.590	9.929	849.248	-7.67	0.000	0.000	-162.10
81	810	685.34	1.504	96.850	9.841	841.721	-9.41	0.000	0.000	-156.38

Time Increm.	(2) Time	(3) Increm. Vol into Pond	(4) Starting Pond Depth	(6)	(7)	(8) Increm. Vol out Pond				(9) Delta Vol
	min.	cf	ft.			cf	_			cf
82	820	685.48	1.478	96.850	9.841	841.721	-11.09	0.000	0.000	-156.24
83	830	686.25	1.452	93.494	9.669	827.012	-12.77	0.000	0.000	-140.76
84	840	687.23	1.428	91.984	9.591	820.302	-14.28	0.000	0.000	-133.07
85	850	688.26	1.406	90.555	9.516	813.909	-15.70	0.000	0.000	-125.65
86	860	689.30	1.385	89.207	9.445	807.825	-17.05	0.000	0.000	-118.52
87	870	690.34	1.365	87.935	9.377	802.045	-18.33	0.000	0.000	-111.70
88	880	691.37	1.347	86.736	9.313	796.558	-19.52	0.000	0.000	-105.19
89	890	663.98	1.329	85.607	9.252	791.357	-20.65	0.000	0.000	-127.38
90	900	627.04	1.308	84.239	9.178	785.012	-22.02	0.000	0.000	-157.97
91	910	615.23	1.282	82.544	9.085	777.072	-23.72	0.000	0.000	-161.84
92	920	611.79	1.255	80.807	8.989	768.851	-25.45	0.000	0.000	-157.06
93	930	611.14	1.229	79,121	8.895	760.789	-27.14	0.000	0.000	-149.65
94	940	611.41	1.204	77.515	8.804	753.027	-28.75	0.000	0.000	-141.62
95	950	611.98	1,180	75,995	8,717	745,607	-30.27	0.000	0.000	-133.62
96	960	612.65	1,158	74,560	8.635	738,538	-31.70	0.000	0.000	-125.89
97	970	613.35	1,137	73,209	8,556	731,816	-33.05	0.000	0.000	-118.47
98	980	614.05	1.117	71,938	8,482	725,432	-34.32	0.000	0.000	-111.39
99	990	614.74	1.098	70.742	8.411	719.379	-35.52	0.000	0.000	-104.64
100	1000	615.43	1.081	69.619	8.344	713.646	-36.64	0.000	0.000	-98.22
101	1010	574.97	1.065	68,565	8.280	708.222	-37.70	0.000	0.000	-133.25
102	1020	520.72	1.042	67,135	8,194	700,797	-39,13	0.000	0.000	-180.08
103	1030	502 92	1.012	65.202	8.075	690,635	-41.06	0.000	0.000	-187.72
104	1040	497.27	0.981	63.187.	7,949	679.881	-43.07	0.000	0.000	-182.61
105	1050	495.66	0.951	61,227	7 825	669.253	-45.03	0.000	0.000	-173.59
106	1060	495.40	0.922	59.364	7,705	658,991	-46,90	0.000	0.000	-163.59
107	1070	495.59	0.895	57.608	7.590	649,172	-48.65	0.000	0.000	-153.58
108	1080	495.93	0.869	55,959	7.481	639.817	-50.30	0.000	0.000	-143.89
109	1090	496.31	0.845	54,415	7.377	630,926	-51.84	0.000	0.000	-134.62
110	1100	496.70	0.823	52.970	7.278	622,493	-53.29	0.000	0.000	-125.79
111	1110	497 10	0.802	51,620	7.185	614,508	-54.64	0.000	0.000	-117.41
112	1120	497 49	0.782	50,360	7.096	606,961	-55.90	0.000	0.000	-109.47
113	1130	497.89	0.764	49,185	7.013	599.839	-57.08	0.000	0.000	-101.95
114	1140	498 28	0.747	48.091	6.935	593,128	-58.17	0.000	0.000	-94.85
115	1150	498.66	0.731	47.072	6.861	586.817	-59.19	0.000	0.000	-88.15
116	1160	499.05	0.716	46 126	6,792	580,889	-60.13	0.000	0.000	-81.84
117	1170	499 43	0 703	45.248	6.727	575 331	-61.01	0.000	0.000	-75.91
118	1180	499.80	0.690	44 433	6 666	570,128	-61.83	0.000	0.000	-70.33
110	1100	500 18	0.678	43 678	6 609	565 264	-62.58	0.000	0.000	-65.09
120	1200	500.55	0.667	42 980	6 556	560 726	-63.28	0.000	0.000	-60.18
121	1210	500.91	0.657	42 334	6.506	556.496	-63.93	0.000	0.000	-55.58
122	1220	501.28	0.648	41.737	6.460	552 561	-64.52	0.000	0.000	-51.28
123	1230	501.64	0.640	41.187	6.418	548,905	-65.07	0.000	0.000	-47.27
124	1240	502.00	0.632	40.679	6 378	545 514	-65.58	0.000	0.000	-43 52
125	1250	502.35	0.624	40 212	6.341	542 374	-66.05	0.000	0.000	-40.02
126	1260	502.71	0.618	39 783	6.307	539 469	-66.48	0.000	0.000	-36.76
127	1270	503.06	0.612	39 388	6 276	536 787	-66.87	0.000	0.000	-33 73
128	1280	503 40	0.606	39.026	6.247	534.314	-67 23	0.000	0.000	-30.91
120	1200	503.75	0.601	38 694	6 220	532 038	-67 57	0.000	0.000	-28 20
130	1300	504 09	0.596	38 301	6 196	529 947	-67.87	0 000	0.000	-25 86
121	1310	504.43	0.592	38 113	6 174	528 028	-68 15	0.000	0.000	-23.60
132	1320	504 77	0.588	37 860	6 153	526 270	-68 40	0.000	0.000	-21 51
132	1330	505 10	0.584	37 629	6 134	524 664	-68 63	0.000	0.000	-19.56
134	1340	505 43	0.581	37 410	6 117	523 197	-68.84	0.000	0.000	-17 77
1.04	1540	505.45	0.501	01.410	0.111	020.101	00.04	0.000	0.000	

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(1) Time Increm.	(2) Time min.	(3) Increm. Vol into Pond cf	(4) Starting Pond Depth ft.		(6)	(7)	(8) Increm. Vol out Pond cf		×		(9) Delta Vol
135	1350	505.76	0.578		37.228	6.102	521.863	-69.03	0.000	0.000	-16.10
136	1360	506.08	0.575	8	37.056	6.087	520.650	-69.20	0.000	0.000	-14.57
137	1370	506.41	0.573		36.899	6.074	519.550	-69.36	0.000	0.000	-13.14
138	1380	506.73	0.571		36.758	6.063	518.556	-69.50	0.000	0.000	-11.83
139	1390	507.05	0.569		36.631	6.052	517.660	-69.63	0.000	0.000	-10.61
140	1400	507.36	0.567		36.517	6.043	516.854	-69.74	0.000	0.000	-9.49
141	1410	507.67	0.565		36.415	6.035	516.132	-69.84	0.000	0.000	-8.46
142	1420	507.98	0.564		36.325	6.027	515.489	-69.94	0.000	0.000	-7.50
143	1430	508.29	0.563		36.244	6.020	514.917	-70.02	0.000	0.000	-6.62
144	1440	508.60	0.562		36.173	6.014	514.411	-70.09	0.000	0.000	-5.81

99502.30

(10) Remain Total Vol in.	(11) Remain Pond Depth ft	(12) CFS Discharge
0.0	0.000	0.00
0.0	0.000	0.00
0.0	0.000	0.00
5.7	0.001	0.00
10.9	0.002	0.04
34.3	0.006	0.05
60.3	0.010	0.09
91.7	0.015	0.11
126.4	0.021	0.14
163.0	0.027	0.17
214.7	0.036	0.19
282.9	0.047	0.22
353.1	0.059	0.25
421.6	0.070	0.28
487.2	0.081	0.30
549.9	0.092	0.33
628.3	0.105	0.35
726.2	0.121	0.37
825.0	0.137	0.40
919.1	0.153	0.42
1007.4	0.168	0.45
1090.1	0.182	0.47
1188.3	0.198	0.49
1307.4	0.218	0.51
1420.0	0.238	0.53
1539.6	0.237	0.50

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(10) Remain Total Vol in.	(11) Remain Pond Depth ft	(12) CFS Discharge	
1744.9 1867.8 2025.9 2194.8 2366.4 2537.8 2708.4 2912.0 3158.6 3416.0 3673.8 3928.8 4180.2 4543.1 5052.4 5601.9 6301.6 7186.4 8650.7 11518.2 13409.0 13579.8 12873.6 11942.2 10524.8 9976.0 9852.9 9968.4 9832.0 9945.2 9859.6 9978.3 9836.4 9963.8 9855.3 9836.4 9963.8 9855.3 9885.3 9885.3 9885.3 9885.3 9885.3 9885.3 9885.3 9885.3 9885.3 9885.3 9885.3 9855.3 9855.3 9640.4 9755.8 9724.5 9693.7 9665.5 9640.4 9598.3 9583.1 9586.7 9558.7 9558.7 9490.5 9347.3 9185.4 9023.3 8866.9	0.291 0.311 0.338 0.366 0.394 0.423 0.423 0.423 0.423 0.423 0.526 0.569 0.612 0.655 0.697 0.757 0.842 0.934 1.050 1.198 1.442 1.920 2.235 2.146 1.990 1.864 1.754 1.663 1.639 1.663 1.643 1.663 1.639 1.665 1.630 1.639 1.665 1.630 1.630 1.665 1.630 1.630 1.626 1.630 1.621 1.663 1.630 1.658 1.630 1.625 1.630 1.630 1.625 1.630 1.630 1.625 1.630 1.625 1.630 1.643 1.665 1.630 1.658 1.643 1.665 1.630 1.658 1.643 1.665 1.630 1.625 1.630 1.625 1.630 1.625 1.630 1.625 1.630 1.625 1.630 1.625 1.630 1.625 1.630 1.625 1.630 1.643 1.643 1.655 1.630 1.658 1.630 1.625 1.593 1.595 1.593 1.582 1.558 1.531 1.504 1.478	0.60 0.62 0.64 0.66 0.69 0.72 0.74 0.77 0.80 0.93 0.95 1.00 1.05 1.11 1.17 1.25 1.37 1.58 1.61 1.56 1.52 1.48 1.47 1.47 1.48 1.46 1.46 1.45 1	

Restroted a -

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(10) Remain Total Vol in.	(11) Remain Pond Depth ft	(12) CFS Discharge
8710.7 8569.9 8436.8 8311.2 8192.7 8081.0 7975.8 7848.4 7690.4 7528.6 7371.5 7221.9 7080.2 6946.6 6820.7 6702.3 6590.9 6486.2 6388.0 6254.8 6074.7 5887.0 5704.4 5530.8 5367.2 5213.6 5069.7 4035.1 4809.3 4691.9 4582.4 4480.5 4385.6 4139.7 4069.4 4004.3 3944.1 3888.6 3370.0 3746.5 3669.7 3636.0 3645.1 3576.8 3590.9 3527.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3505.8 3486.3 3486.3 3505.8 3486.3 3486.3 3505.8 3505.8	1.452 1.428 1.406 1.385 1.365 1.347 1.329 1.308 1.282 1.255 1.229 1.204 1.180 1.158 1.377 1.117 1.098 1.042 1.012 0.981 0.951 0.922 0.895 0.845 0.823 0.802 0.764 0.747 0.731 0.716 0.703 0.690 0.678 0.667 0.657 0.648 0.6612 0.606 0.601 0.596 0.584 0.581	1.40 1.38 1.37 1.36 1.35 1.34 1.33 1.32 1.31 1.30 1.28 1.27 1.26 1.24 1.23 1.22 1.21 1.20 1.19 1.18 1.17 1.15 1.13 1.12 1.10 1.08 1.07 1.05 1.04 1.02 1.01 1.00 0.99 0.98 0.97 0.96 0.95 0.94 0.93 0.93 0.92 0.91 0.91 0.90 0.89

(10) Remain Total Vol in.	(11) Remain Pond Depth ft	(12) CFS Discharge
3452.4 3437.8 3424.7 3412.8 3402.2 3392.7 3384.3 3376.8 3376.1 3364.3	0.575 0.573 0.571 0.569 0.567 0.565 0.564 0.563 0.562 0.561	0.87 0.87 0.86 0.86 0.86 0.86 0.86 0.86 0.86

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	Date:	Jun-04	100		1.00			1999	State of the second second		
	Given:	Project =		WOOD MS	5						
		Area =	11.34	acres							
		Pt =	3.9	inches	25-Year /	24 Hour S	storm				
		dt =	10	min.							
		Tc =	40	min. (Pre-	-Developed	d Site Con	ditions)				
		PERVIOUS	S Parcel		IMPERVIC	OUS Parc	el				
		Area =	11.34	acres	Area =	0	acres				
		CN =	82		CN =	98					
		S =	2.20		S =	0.20					
		0.2S =	0.44		0.2S =	0.04					
	Compute	Developed	Condition	s Runoff hy	drograph						
		Column (3)	= SCS T	ype IA Rain	fall Distribu	ution					
		Column (4)) = Col. (3) x Pt = 10 y	ear - 24 H	our Hyeto	graph at thi	is location.			
		Column (5)) = Accum	ulated Sum	of Col. (4)						
		Column (6)) = [If P <=	= 0.2S] = 0;	Note, use	PERVIOU	S Area "S"	value.			
		[If	P > 0.2S]	= (Col.(5) -	0.2S)^2/(C	(01.(5) + 0.	8S); Using	the PERV	IOUS Area	"S" value.	
		Column (7) = Col.(6)	of Present	Time Step	- Col.(6) c	of Previous	Time Step			
		Column (8)	= Same	method as f	or Col.(6),	except us	e the IMPE	RVIOUS	vea "S" va	alue.	
		Column (9)) = Col.(8)	of the pres	ent time sti	ep - Col.(8	(7)) of the pre	vious time	step.	int needs	0-1/011
		Column (1)	(PEh) = ((PEh)) = (60.5)	Col (10)	a / Iotal an	ea) x Col.	- 10 minut	ERVIOUS	area/10	tal area) x (-ol.(9))
		Column (1	1) = (60.5)	x Col.(10) x	I otal Area	a)/10 (dt	= 10 minut	es)			
		Routing	Constant,	w = dt / (21)	c + at) =	ton i luu	0.1111	Dentinue	Time Cha		
		Column (1.	Col(11)o	f Present Ti	me Sten -	12 x Col (1	12) of Provi	oue Time	Ston)]]	μ	
			00	in rosone in	nie otep	le v coul	12/01/101	ous mile	5100/11		
					-						
145	(2)	(3)	(4)	(5)	Pervious	Area	Imperviou	s Area	(10)	(11)	(12)
(1) Time	(2) Time	(3) Painfall	(4)	(5)	Pervious (6)	Area (7)	Imperviou (8)	(9)	(10) Total	(11)	(12)
(1) Time	(2) Time	(3) Rainfall	(4) Incre-	(5) Accumu-	Pervious (6) Accumu-	Area (7) Incre-	(8) Accumu-	(9) Incre-	(10) Total	(11) Instant	(12) design
(1) Time ncremen	(2) Time	(3) Rainfall distri-	(4) Incre- mental Rainfall	(5) Accumu- lated Rainfall	Pervious (6) Accumu- lated Bunoff	Area (7) Incre- mental Bunoff	(8) Accumu- lated Bunoff	IS Area (9) Incre- mental Bunoff	(10) Total Runoff	(11) Instant hydro-	(12) design hydro- graph
(1) Time ncremen	(2) Time t	(3) Rainfall distri- bution % of Pt	(4) Incre- mental Rainfall in.	(5) Accumu- lated Rainfall in.	Pervious (6) Accumu- lated Runoff in.	Area (7) Incre- mental Runoff in.	Imperviou (8) Accumu- lated Runoff in.	is Area (9) Incre- mental Runoff in.	(10) Total Runoff in.	(11) Instant hydro- graph cfs	(12) design hydro- graph cfs
(1) Time ncremen	(2) Time t min.	(3) Rainfall distri- bution % of Pt	(4) Incre- mental Rainfall in.	(5) Accumu- lated Rainfall in.	Pervious (6) Accumu- lated Runoff in.	Area (7) Incre- mental Runoff in.	Imperviou (8) Accumu- lated Runoff in.	is Area (9) Incre- mental Runoff in.	(10) Total Runoff in.	(11) Instant hydro- graph cfs	(12) design hydro- graph cfs
(1) Time Incremen	(2) Time t min. 10	(3) Rainfall distri- bution % of Pt 0.0040	(4) Incre- mental Rainfall in. 0.0156	(5) Accumu- lated Rainfall in. 0.0156	Pervious (6) Accumu- lated Runoff in. 0.0000	Area (7) Incre- mental Runoff in. 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000	(9) Incre- mental Runoff in. 0.0000	(10) Total Runoff in. 0.0000	(11) Instant hydro- graph cfs 0.0	(12) design hydro- graph cfs 0.000
(1) Time Incremen 1 2	(2) Time t min. 10 20	(3) Rainfall distri- bution % of Pt 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0156 0.0156	(5) Accumu- lated Rainfall in. 0.0156 0.0312	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000	Area (7) Incre- mental Runoff in. 0.0000 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0000	Is Area (9) Incre- mental Runoff in. 0.0000 0.0000	(10) Total Runoff in. 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000
(1) Time Incremen	(2) Time t min. 10 20 30	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000	Area (7) Incre- mental Runoff in. 0.0000 0.0000 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0000 0.0002	s Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0002	(10) Total Runoff in. 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000 0.000
(1) Time Incremen 1 2 3 4	(2) Time t min. 10 20 30 40	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000	Area (7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0000 0.0002 0.0021	s Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0002 0.0019	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000 0.000
(1) Time Incremen 1 2 3 4 5	(2) Time min. 10 20 30 40 50	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000	Area (7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0000 0.0002 0.0021 0.0057	IS Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0002 0.0019 0.0037	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000
(1) Time Incremen 1 2 3 4 5 6	(2) Time min. 10 20 30 40 50 60	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Area (7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0000 0.0002 0.0021 0.0057 0.0108	IS Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0002 0.0019 0.0037 0.0051	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000 0.000 0.000
(1) Time Incremen 1 2 3 4 5 6 7	(2) Time min. 10 20 30 40 50 60 70	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936 0.1092	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Area (7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0000 0.0002 0.0021 0.0057 0.0108 0.0172	IS Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0002 0.0019 0.0037 0.0051 0.0063	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000 0.000 0.000 0.000
(1) Time Incremen 1 2 3 4 5 6 7 8	(2) Time min. 10 20 30 40 50 60 70 80	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936 0.1092 0.1248	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Area (7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0002 0.0021 0.0057 0.0108 0.0172 0.0245	IS Area (9) Incre- mental Runoff in. 0.0000 0.0002 0.0002 0.0019 0.0037 0.0051 0.0063 0.0073	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
(1) Time Incremen 1 2 3 4 5 6 7 8 9	(2) Time min. 10 20 30 40 50 60 70 80 90	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936 0.1092 0.1248 0.1404	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Area (7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0002 0.0021 0.0057 0.0108 0.0172 0.0245 0.0327	IS Area (9) Incre- mental Runoff in. 0.0000 0.0002 0.0002 0.0019 0.0037 0.0051 0.0063 0.0073 0.0082	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
(1) Time Incremen 1 2 3 4 5 6 7 8 9 10	(2) Time min. 10 20 30 40 50 60 70 80 90 100	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936 0.1092 0.1248 0.1404 0.1560	Pervious (6) Accumu- lated Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Area (7) Incre- mental Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0002 0.0021 0.0057 0.0108 0.0172 0.0245 0.0327 0.0416	IS Area (9) Incre- mental Runoff in. 0.0000 0.0002 0.0019 0.0037 0.0051 0.0063 0.0073 0.0082 0.0089	(10) Total Runoff in. 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
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(1) Time Incremen 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0155 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0234 0.0234 0.0234	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936 0.1092 0.1248 0.1404 0.1560 0.1755 0.1950 0.2145 0.2340 0.2535 0.2730 0.2964 0.3198 0.3432 0.3666 0.2900	Pervious (6) Accumu- lated Runoff in. 0.0000	Area (7) Incre- mental Runoff in. 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0002 0.0021 0.0057 0.0108 0.0172 0.0245 0.0327 0.0416 0.0535 0.0664 0.0799 0.0939 0.1085 0.1236 0.1421 0.1611 0.1805 0.2003 0.2004	IS Area (9) Incre- mental Runoff in. 0.0000 0.0002 0.0019 0.0037 0.0051 0.0063 0.0073 0.0051 0.0063 0.0073 0.0082 0.0089 0.0120 0.0128 0.0128 0.0141 0.0146 0.0150 0.0194 0.0194 0.0198	(10) Total Runoff in. 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.000 0.0000 0.000000
(1) Time Incremen 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0234 0.0234 0.0234 0.0234	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936 0.1092 0.1248 0.1404 0.1560 0.1755 0.1950 0.2145 0.2340 0.2535 0.2730 0.2964 0.3198 0.3432 0.3666 0.3900 0.4134	Pervious (6) Accumu- lated Runoff in. 0.0000	Area (7) Incre- mental Runoff in. 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0002 0.0021 0.0057 0.0108 0.0172 0.0245 0.0327 0.0416 0.0535 0.0664 0.0799 0.0939 0.1085 0.1236 0.1421 0.1611 0.1805 0.2003 0.2204 0.2407	IS Area (9) Incre- mental Runoff in. 0.0000 0.0002 0.0019 0.0037 0.0051 0.0063 0.0073 0.0051 0.0063 0.0073 0.0082 0.0089 0.0120 0.0128 0.0135 0.0141 0.0146 0.0150 0.0194 0.0194 0.0201 0.0201	(10) Total Runoff in. 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.0000 0.0000 0.000000
(1) Time Incremen 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 22	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0155 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0234 0.0234 0.0234 0.0234	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936 0.1092 0.1248 0.1404 0.1560 0.1755 0.1950 0.2145 0.2340 0.2535 0.2730 0.2964 0.3198 0.3432 0.3666 0.3900 0.4134 0.4407	Pervious (6) Accumu- lated Runoff in. 0.0000	Area (7) Incre- mental Runoff in. 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0002 0.0021 0.0057 0.0108 0.0172 0.0245 0.0327 0.0416 0.0535 0.0664 0.0799 0.0939 0.1085 0.1236 0.1421 0.1611 0.1805 0.2003 0.2204 0.2407 0.2648	IS Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0002 0.0019 0.0037 0.0051 0.0063 0.0073 0.0082 0.0120 0.0128 0.0128 0.0128 0.0141 0.0146 0.0150 0.0190 0.0194 0.0203 0.0203	(10) Total Runoff in. 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000
(1) Time Incremen 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 230	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0155 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0234 0.0234 0.0234 0.0234 0.0234	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936 0.0936 0.0936 0.1092 0.1248 0.1404 0.1560 0.1755 0.1950 0.2145 0.2340 0.2535 0.2730 0.2964 0.3198 0.3432 0.3666 0.3900 0.4134 0.4690	Pervious (6) Accumu- lated Runoff in. 0.0000	Area (7) Incre- mental Runoff in. 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0002 0.0021 0.0057 0.0108 0.0172 0.0245 0.0327 0.0416 0.0535 0.0664 0.0799 0.0939 0.1085 0.1236 0.1421 0.1611 0.1805 0.2003 0.2204 0.2407 0.2648 0.2891	IS Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0002 0.0019 0.0037 0.0051 0.0063 0.0073 0.0082 0.0082 0.0120 0.0128 0.0128 0.0128 0.0135 0.0141 0.0146 0.0150 0.0194 0.0198 0.0201 0.0242	(10) Total Runoff in. 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000
(1) Time Incremen 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 24 25	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 240	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0070 0.0070	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0155 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0234 0.0234 0.0234 0.0234 0.0234 0.0234	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936 0.1092 0.1248 0.1404 0.1560 0.1755 0.1950 0.2145 0.2340 0.2535 0.2730 0.2964 0.3198 0.3432 0.3666 0.3900 0.4134 0.4407 0.4680 0.4052	Pervious (6) Accumu- lated Runoff in. 0.0000	Area (7) Incre- mental Runoff in. 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0002 0.0021 0.0057 0.0108 0.0172 0.0245 0.0327 0.0416 0.0535 0.0664 0.0799 0.0939 0.1085 0.1236 0.1421 0.1611 0.1805 0.2003 0.2204 0.2407 0.2648 0.2891 0.3136	IS Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0002 0.0019 0.0037 0.0063 0.0063 0.0063 0.0063 0.0082 0.0089 0.0120 0.0128 0.0128 0.0135 0.0141 0.0146 0.0150 0.0190 0.0194 0.0201 0.0203 0.0240 0.0243 0.0246	(10) Total Runoff in. 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000
(1) Time Incremen 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	(2) Time min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 250	(3) Rainfall distri- bution % of Pt 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0040 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0050 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0060 0.0070 0.0070 0.0070	(4) Incre- mental Rainfall in. 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0156 0.0155 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0195 0.0234 0.0234 0.0234 0.0234 0.0233 0.0273 0.0273 0.0273	(5) Accumu- lated Rainfall in. 0.0156 0.0312 0.0468 0.0624 0.0780 0.0936 0.1092 0.1248 0.1404 0.1560 0.1755 0.1950 0.2145 0.2340 0.2535 0.2730 0.2964 0.3198 0.3432 0.3666 0.3900 0.4134 0.4407 0.4680 0.4953 0.5226	Pervious (6) Accumu- lated Runoff in. 0.00000 0.00000 0.00000 0.000000	Area (7) Incre- mental Runoff in. 0.0000	Imperviou (8) Accumu- lated Runoff in. 0.0000 0.0002 0.0021 0.0057 0.0108 0.0172 0.0245 0.0327 0.0416 0.0535 0.0664 0.0799 0.0939 0.1085 0.1236 0.1421 0.1611 0.1805 0.2003 0.2204 0.2407 0.2648 0.2891 0.3136 0.2324	IS Area (9) Incre- mental Runoff in. 0.0000 0.0000 0.0002 0.0019 0.0037 0.0051 0.0063 0.0073 0.0063 0.0073 0.0082 0.0082 0.0120 0.0128 0.0120 0.0128 0.0135 0.0141 0.0146 0.0150 0.0194 0.0203 0.0240 0.0248 0.0248	(10) Total Runoff in. 0.0000	(11) Instant hydro- graph cfs 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	(12) design hydro- graph cfs 0.0000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000

					Pervious	Area	Impervior	IS Area			
(1) Time ncrement	(2) Time min.	(3) Rainfall distri- bution	(4) Incre- mental Rainfall in.	(5) Accumu- lated Rainfall in.	(6) Accumu- lated Runoff in.	(7) Incre- mental Runoff in.	(8) Accumu- lated Runoff in.	(9) Incre- mental Runoff in.	(10) Total Runoff in.	(11) Instant hydro- graph cfs	(12) design hydro- graph cfs
							0.0005	0.0054	0.0000		0.004
28	280	0.0070	0.0273	0.5772	0.0082	0.0029	0.3885	0.0251	0.0029	0.2	0.081
29	290	0.0082	0.0320	0.6092	0.0122	0.0041	0.4182	0.0297	0.0041	0.3	0.115
30	300	0.0082	0.0320	0.6412	0.0170	0.0048	0.4480	0.0298	0.0048	0.3	0.157
31	310	0.0082	0.0320	0.6731	0.0226	0.0055	0.4780	0.0300	0.0055	0.4	0.201
32	320	0.0082	0.0320	0.7051	0.0288	0.0062	0.5082	0.0301	0.0062	0.4	0.246
33	330	0.0082	0.0320	0.7371	0.0356	0.0069	0.5385	0.0303	0.0069	0.5	0.291
34	340	0.0082	0.0320	0.7691	0.0431	0.0075	0.5689	0.0304	0.0075	0.5	0.336
35	350	0.0095	0.0371	0.8061	0.0526	0.0095	0.6042	0.0353	0.0095	0.6	0.390
36	360	0.0095	0.0371	0.8432	0.0628	0.0102	0.6397	0.0355	0.0102	0.7	0.454
37	370	0.0095	0.0371	0.8802	0.0738	0.0110	0.6752	0.0356	0.0110	0.8	0.515
38	380	0.0095	0.0371	0.9173	0.0856	0.0117	0.7109	0.0357	0.0117	0.8	0.574
39	390	0.0095	0.0371	0.9543	0.0980	0.0124	0.7467	0.0358	0.0124	0.9	0.630
40	400	0.0095	0.0371	0.9914	0.1110	0.0131	0.7826	0.0359	0.0131	0.9	0.684
41	410	0.0134	0.0523	1.0436	0.1306	0.0195	0.8333	0.0507	0.0195	1.3	0.781
42	420	0.0134	0.0523	1.0959	0.1513	0.0207	0.8841	0.0508	0.0207	1.4	0.914
43	430	0.0134	0.0523	1.1482	0.1732	0.0219	0.9350	0.0509	0.0219	1.5	1.036
44	440	0.0180	0.0702	1.2184	0.2042	0.0310	1.0036	0.0686	0.0310	2.1	1.209
45	450	0.0180	0.0702	1.2886	0.2370	0.0328	1.0723	0.0687	0.0328	2.3	1.427
46	460	0.0340	0.1326	1.4212	0.3036	0.0666	1.2025	0.1302	0.0666	4.6	1.868
47	470	0.0540	0.2106	1.6318	0.4199	0.1163	1.4101	0.2075	0.1163	8.0	2.847
48	480	0.0270	0.1053	1.7371	0.4823	0.0624	1.5141	0.1040	0.0624	4.3	3.577
49	490	0.0180	0.0702	1.8073	0.5254	0.0430	1.5835	0.0694	0.0430	3.0	3,586
50	500	0.0134	0.0523	1.8595	0.5581	0.0327	1.6352	0.0517	0.0327	2.2	3.366
51	510	0.0134	0.0523	1.9118	0.5914	0.0333	1.6870	0.0517	0.0333	2.3	3.121
52	520	0.0134	0.0523	1.9640	0.6252	0.0338	1.7387	0.0518	0.0338	2.3	2.939
53	530	0.0088	0.0343	1.9984	0.6476	0.0225	1.7727	0.0340	0.0225	1.5	2.715
54	540	0.0088	0.0343	2.0327	0.6703	0.0227	1.8067	0.0340	0.0227	1.6	2.456
55	550	0.0088	0.0343	2.0670	0.6932	0.0229	1.8408	0.0340	0.0229	1.6	2.258
56	560	0.0088	0.0343	2.1013	0.7163	0.0231	1.8748	0.0340	0.0231	1.6	2.107
57	570	0.0088	0.0343	2.1356	0.7396	0.0233	1.9089	0.0340	0.0233	1.6	1.992
58	580	0.0088	0.0343	2.1700	0.7631	0.0235	1.9429	0.0341	0.0235	1.6	1.906
59	590	0.0088	0.0343	2.2043	0.7868	0.0237	1.9770	0.0341	0.0237	1.6	1.842
60	600	0.0088	0.0343	2.2386	0.8107	0.0239	2.0110	0.0341	0.0239	1.6	1.795
61	610	0.0088	0.0343	2.2729	0.8347	0.0240	2.0451	0.0341	0.0240	1.6	1.762
62	620	0.0088	0.0343	2.3072	0.8590	0.0242	2.0792	0.0341	0.0242	1.7	1.738
63	630	0.0088	0.0343	2.3416	0.8833	0.0244	2.1133	0.0341	0.0244	1.7	1.722
64	640	0.0088	0.0343	2.3759	0.9079	0.0246	2.1474	0.0341	0.0246	1.7	1.713
65	650	0.0072	0.0281	2.4040	0.9281	0.0202	2.1753	0.0279	0.0202	1.4	1.673
66	660	0.0072	0.0281	2.4320	0.9484	0.0203	2.2032	0.0279	0.0203	1.4	1.610
67	670	0.0072	0.0281	2.4601	0.9688	0.0204	2.2311	0.0279	0.0204	1.4	1.563
68	680	0.0072	0.0281	2.4882	0.9894	0.0205	2.2590	0.0279	0.0205	1.4	1.528
69	690	0.0072	0.0281	2.5163	1.0100	0.0206	2.2869	0.0279	0.0206	1.4	1.502
70	700	0.0072	0.0281	2.5444	1.0307	0.0207	2.3148	0.0279	0.0207	1.4	1.483
71	710	0.0072	0.0281	2.5724	1.0515	0.0208	2.3428	0.0279	0.0208	1.4	1.470
72	720	0.0072	0.0281	2.6005	1.0724	0.0209	2.3707	0.0279	0.0209	1,4	1.461
73	730	0.0072	0.0281	2.6286	1.0934	0.0210	2.3986	0.0279	0.0210	1.4	1.456
74	740	0.0072	0.0281	2.6567	1.1145	0.0211	2.4266	0.0279	0.0211	1.4	1.453
75	750	0.0072	0.0281	2.6848	1.1357	0.0212	2.4545	0.0279	0.0212	1.5	1.453
76	760	0.0072	0.0281	2.7128	1.1569	0.0213	2.4824	0.0279	0.0213	1.5	1.453
77	770	0.0057	0.0222	2.7351	1.1738	0.0169	2.5045	0.0221	0.0169	1.2	1.421
78	780	0.0057	0.0222	2.7573	1.1908	0.0169	2.5267	0.0221	0.0169	1.2	1.363
79	790	0.0057	0.0222	2.7795	1.2078	0.0170	2.5488	0.0221	0.0170	1.2	1.319
80	800	0.0057	0.0222	2.8018	1.2248	0.0170	2.5709	0.0221	0.0170	1.2	1.285
P1	810	0.0057	0.0222	2.8240	1.2419	0.0171	2.5930	0.0221	0.0171	1.2	1.260

1.0					Pervious	Area	Imperviou				
(1) Time Increment	(2) Time	(3) Rainfall distri- bution	(4) Incre- mental Rainfall in	(5) Accumu- lated Rainfall in.	(6) Accumu- lated Runoff in	(7) Incre- mental Runoff in.	(8) Accumu- lated Runoff in.	(9) Incre- mental Runoff in.	(10) Total Runoff in.	(11) Instant hydro- graph cfs	(12) design hydro- graph cfs
									10.	010	0.0
82	820	0.0057	0.0222	2.8462	1.2591	0.0171	2.6152	0.0221	0.0171	1.2	1.241
83	830	0.0057	0.0222	2.8685	1.2763	0.0172	2.6373	0.0221	0.0172	1.2	1.227
84	840	0.0057	0.0222	2.8907	1.2935	0.0172	2.6594	0.0221	0.0172	1.2	1.217
85	850	0.0057	0.0222	2,9129	1,3108	0.0173	2.6816	0.0221	0.0173	1.2	1.210
86	860	0.0057	0.0222	2,9351	1.3281	0.0173	2,7037	0.0221	0.0173	1.2	1.205
87	870	0.0057	0.0222	2 9574	1.3455	0.0174	2,7258	0.0221	0.0174	1.2	1,202
88	880	0.0057	0.0222	2 9796	1.3630	0.0174	2,7480	0.0221	0.0174	1.2	1,200
89	890	0.0050	0.0195	2 9991	1 3783	0.0153	2 7674	0.0194	0.0153	1.1	1,183
00	900	0.0050	0.0195	3.0186	1.3936	0.0154	2 7868	0.0194	0.0154	1.1	1.154
01	010	0.0050	0.0105	3.0381	1 4000	0.0154	2 8062	0.0194	0.0154	11	1 132
91	020	0.0050	0.0105	3.0576	1 4030	0.0154	2.0002	0.0194	0.0154	4.4	1 116
92	920	0.0050	0.0195	3.0370	1.4240	0.0154	2.0250	0.0194	0.0155	1.1	1 103
93	930	0.0050	0.0195	3.0771	1.4399	0.0155	2.0401	0.0194	0.0155	4.4	1.105
94	940	0.0050	0.0195	3.0900	1,4504	0.0155	2.0040	0.0194	0.0155	4.4	1.094
95	950	0.0050	0.0195	3.1161	1.4709	0.0155	2.0039	0.0194	0.0155	1.1	1.007
96	960	0.0050	0.0195	3.1356	1.4865	0.0156	2.9033	0.0194	0.0156	14	1.083
97	970	0.0050	0.0195	3.1551	1.5021	0.0156	2.9228	0.0194	0.0156	1.1	1.079
98	980	0.0050	0.0195	3.1746	1.5177	0.0156	2.9422	0.0194	0.0156	1,1	1.078
99	990	0.0050	0.0195	3.1941	1.5334	0.0157	2.9616	0.0194	0.0157	1.1	1.076
100	1000	0.0050	0.0195	3.2136	1.5490	0.0157	2.9810	0.0194	0.0157	1.1	1.076
101	1010	0.0040	0.0156	3.2292	1.5616	0.0126	2.9966	0.0155	0.0126	0.9	1.052
102	1020	0.0040	0.0156	3.2448	1.5742	0.0126	3.0121	0.0155	0.0126	0.9	1.010
103	1030	0.0040	0.0156	3.2604	1.5868	0.0126	3.0277	0.0155	0.0126	0.9	0.978
104	1040	0.0040	0.0156	3.2760	1.5994	0.0126	.3.0432	0.0155	0.0126	0.9	0.953
105	1050	0.0040	0.0156	3.2916	1.6121	0.0126	3.0588	0.0155	0.0126	0.9	0.934
106	1060	0.0040	0.0156	3.3072	1.6247	0.0127	3.0743	0.0155	0.0127	0.9	0.919
107	1070	0.0040	0.0156	3.3228	1.6374	0.0127	3.0898	0.0155	0.0127	0.9	0.908
108	1080	0.0040	0.0156	3.3384	1.6501	0.0127	3.1054	0.0155	0.0127	0.9	0.900
109	1090	0.0040	0.0156	3.3540	1.6628	0.0127	3.1209	0.0155	0.0127	0.9	0.893
110	1100	0.0040	0.0156	3 3696	1.6755	0.0127	3,1365	0.0155	0.0127	0.9	0.889
111	1110	0.0040	0.0156	3.3852	1.6883	0.0127	3.1520	0.0155	0.0127	0.9	0.885
112	1120	0.0040	0.0156	3 4008	1 7010	0.0128	3.1676	0.0155	0.0128	0.9	0.883
112	1130	0.0040	0.0156	3 4164	1 7138	0.0128	3 1831	0.0155	0.0128	0.9	0.882
114	1140	0.0040	0.0156	3 4320	1 7266	0.0128	3 1987	0.0155	0.0128	0.9	0.881
116	1150	0.0040	0.0156	3 4476	1 7304	0.0128	3 2142	0.0155	0.0128	0.0	0.880
110	1100	0.0040	0.0150	2 4622	1 7523	0.0120	3 2208	0.0155	0.0128	0.0	0.880
110	1100	0.0040	0.0150	3 4700	1 7651	0.0120	3 2452	0.0156	0.0128	0.0	0.880
117	11/0	0.0040	0.0150	3.4700	1 7700	0.0120	3 2600	0.0156	0.0120	0.0	0.881
118	1180	0.0040	0.0156	3.4944	1,7700	0.0129	2.0764	0.0150	0.0129	0.9	0.001
119	1190	0.0040	0.0156	3.5100	1.7909	0.0129	3.2/04	0.0150	0.0129	0.9	0.001
120	1200	0.0040	0.0156	3.5256	1.8038	0.0129	3.2920	0.0156	0.0129	0.9	0.062
121	1210	0.0040	0.0156	3.5412	1.8167	0.0129	3.3075	0.0156	0.0129	0.9	0.883
122	1220	0.0040	0.0156	3.5568	1.8296	0.0129	3.3231	0.0156	0.0129	0.9	0.884
123	1230	0.0040	0.0156	3.5724	1.8426	0.0129	3.3387	0.0156	0.0129	0.9	0.884
124	1240	0.0040	0.0156	3.5880	1.8555	0.0130	3.3542	0.0156	0.0130	0.9	0.885
125	1250	0.0040	0.0156	3.6036	1.8685	0.0130	3.3698	0.0156	0.0130	0.9	0.886
126	1260	0.0040	0.0156	3.6192	1.8815	0.0130	3.3853	0.0156	0.0130	0.9	0.887
127	1270	0.0040	0.0156	3.6348	1.8945	0.0130	3.4009	0.0156	0.0130	0.9	0.888
128	1280	0.0040	0.0156	3.6504	1.9075	0.0130	3.4164	0.0156	0.0130	0.9	0.889
129	1290	0.0040	0.0156	3.6660	1.9205	0.0130	3.4320	0.0156	0.0130	0.9	0.890
130	1300	0.0040	0.0156	3.6816	1.9336	0.0131	3.4475	0.0156	0.0131	0.9	0.891
131	1310	0.0040	0.0156	3.6972	1.9467	0.0131	3.4631	0.0156	0.0131	0.9	0.892
132	1320	0.0040	0.0156	3.7128	1.9597	0.0131	3.4786	0.0156	0.0131	0.9	0.893
133	1330	0.0040	0.0156	3.7284	1.9728	0.0131	3.4942	0.0156	0.0131	0.9	0.894
134	1340	0.0040	0.0156	3,7440	1.9859	0.0131	3.5098	0.0156	0.0131	0.9	0.895

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					Pervious	Area	Imperviou	s Area			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)
Time	Time	Rainfall	Incre-	Accumu-	Accumu-	Incre-	Accumu-	Incre-	Total	Instant	design
Increment		distri-	mental	lated	lated	mental	lated	mental	Runoff	hydro-	hydro-
1		bution	Rainfall	Rainfall	Runoff	Runoff	Runoff	Runoff		graph	graph
	min.		in.	in.	in.	in.	in.	in.	in.	cfs	cfs
135	1350	0.0040	0.0156	3.7596	1.9991	0.0131	3.5253	0.0156	0.0131	0.9	0.896
136	1360	0.0040	0.0156	3.7752	2.0122	0.0131	3.5409	0.0156	0.0131	0.9	0.897
137	1370	0.0040	0.0156	3.7908	.2.0253	0.0132	3.5564	0.0156	0.0132	0.9	0.898
138	1380	0.0040	0.0156	3.8064	2.0385	0.0132	3.5720	0.0156	0.0132	0.9	0.899
139	1390	0.0040	0.0156	3.8220	2.0517	0.0132	3.5876	0.0156	0.0132	0.9	0.900
140	1400	0.0040	0.0156	3.8376	2.0649	0.0132	3.6031	0.0156	0.0132	0.9	0.901
141	1410	0.0040	0.0156	3.8532	2.0781	0.0132	3.6187	0.0156	0.0132	0.9	0.902
142	1420	0.0040	0.0156	3.8688	2.0913	0.0132	3.6342	0.0156	0.0132	0.9	0.903
143	1430	0.0040	0.0156	3.8844	2.1045	0.0132	3.6498	0.0156	0.0132	0.9	0.904
144	1440	0.0040	0.0156	3.9000	2.1178	0.0132	3.6654	0.0156	0.0132	0.9	0.905
								Total Vo	lume of Ru	unoff =	85003.654
								(Found b	v summin	a this colur	nn and
								multiply	ng by 600	. 600 is the	5885 T 1075
								convers	ion require	ed to conve	rt
								SUM(Q)	in cfs to t	otal volume	3
								in cubic	feet as fol	lows:	
								V = SUM	A(Q) x dt		
							(cu.ft.)	= (cu.ft/s)	x (10 min.) x (60 s/m	in.)
							State in the second second			and the second second second second	~~~*
							20				

-	Date:	Nov-03	LOULAIN	and meetings	- OANTA	DARDAR	ATTORU	GIVAFGH	Mic Inou		-
	Given:	Project =		WOOD M	5						
	Given.	Area =	11 34	acres							
		D+ =	3.0	inches	25-Voor/	24 Hours	torm				
			3.9	min	23-16417	24 11001 0	Storm				
		at =	10	min.		-	- distances				
		IC =	10	min. (Pos	st-Develope	ed Site Co	naitions)				
		PERVIOU	S Parcel		IMPERVIC	OUS Parc	el				
		Area =	5.51	acres	Area =	5.83	acres				
		CN =	80		CN =	98					
		S =	2.50		S =	0.20					
		0.2S =	0.50		0.25 =	0.04					
	Compute	Developed	Condition	s Runoff h	vdrograph						
	2.242.4										
		Column (3) = SCST	ype IA Rain	Itall Distrib	ution	the second s	to to a stress			
		Column (4) = Col. (3)	$) \times Pt = 10$	year - 24 F	four Hyeto	ograph at tr	nis location	I .		
		Column (5) = Accum	ulated Sun	1 of Col. (4)					
		Column (6) = [If P <=	= 0.2SJ = 0;	Note, use	PERVIOL	JS Area "S	value.			
		[f	P > 0.2S]	= (Col.(5) -	0.25)^2/(0	Col.(5) + C	1.8S); Using	the PER	/IOUS Are	ea "S" value	6
		Column (7) = Col.(6)	of Present	Time Step	- Col.(6)	of Previous	Time Ste	p	1.11	
		Column (8) = Same	method as	for Col.(6),	except us	se the IMPI	ERVIOUS	Area "S" v	alue.	
		Column (9) = Col.(8)	of the pres	ent time st	ep - Col.(8) of the pr	evious tim	e step.		
		Column (1	0) = ((PEF))	RVIOUS are	ea / Total a	rea) x Col	.(7)) + ((IM	PERVIOU	S area / T	otal area) x	Col.(9))
		Column (1	1) = (60.5)	x Col.(10)	x Total Are	a)/10(dt	= 10 minu	tes)			
		Routing	Constant.	w = dt / (21)	c + dt) =		0.3333				
		Column (1	2) = Col.(1)	2) of Previ	ous Time S	Step + (w :	(Col.(11)	of Previou	s Time Ste	ep.	
		+	Col.(11) c	f Present T	ime Step -	(2 x Col.(12) of Prev	ious Time	Step)])		
			199.2	12, 12, 1							_
/15	(2)	(3)	(4)	(5)	Pervious (6)	Area (7)	Imperviou (8)	IS Area	(10)	(11)	(12)
Timo	Time	Daiofall	(4)	107	Accumu	Incro	Accumu	(5)	Total	Inctant	docion
Time	Time	diate	montel	Accumu-	Accumu-	montel	Accumu-	montol	Duroff	hudro	design
ncrement		aistn-	mental	Deletell	lated	mental	lated	mental	Runon	nyaro-	nyaro-
	10010	bution	Raintall	Rainfall	Runoff	Runoff	Runon	Runoff	14	graph	graph
	min.	% of Pt	ın.	in.	in.	in.	in.	in.	IN.	CIS	CIS
1	10	0.0040	0.0156	0.0156	0.0000	0.0000	0.0000	0.0000	0.0000	0.0	0.000
2	20	0.0040	0.0156	0.0312	0.0000	0.0000	0.0000	0.0000	0.0000	0.0	0.000
3	30	0.0040	0.0156	0.0468	0.0000	0.0000	0.0002	0.0002	0.0001	0.0	0.002
4	40	0.0040	0.0156	0.0624	0.0000	0.0000	0.0021	0.0002	0.0010	0.1	0.002
-	40	0.0040	0.0150	0.0024	0.0000	0.0000	0.0021	0.0013	0.0010	0.1	0.02
2	50	0.0040	0.0156	0.0780	0.0000	0.0000	0.0057	0.0037	0.0019	0.1	0.074
0	00	0.0040	0.0156	0.0930	0.0000	0.0000	0.0108	0.0051	0.0026	0.2	0.120
1	/0	0.0040	0.0156	0.1092	0.0000	0.0000	0.0172	0.0063	0.0032	0.2	0.177
8	80	0.0040	0.0156	0.1248	0.0000	0.0000	0.0245	0.0073	0.0038	0.3	0.215
9	90	0.0040	0.0156	0.1404	0.0000	0.0000	0.0327	0.0082	0.0042	0.3	0.255
10	100	0.0040	0.0156	0.1560	0.0000	0.0000	0.0416	0.0089	0.0046	0.3	0.286
11	110	0.0050	0.0195	0.1755	0.0000	0.0000	0.0535	0.0120	0.0062	0.4	0.341
12	120	0.0050	0.0195	0.1950	0.0000	0.0000	0.0664	0.0128	0.0066	0.5	0.405
13	130	0.0050	0.0195	0.2145	0.0000	0.0000	0.0799	0.0135	0.0069	0.5	0.444
14	140	0.0050	0.0195	0.2340	0.0000	0.0000	0.0939	0.0141	0.0072	0.5	0.472
15	150	0.0050	0.0195	0.2535	0.0000	0.0000	0.1085	0.0146	0.0075	0.5	0.495
16	160	0.0050	0.0195	0.2730	0.0000	0.0000	0.1236	0.0150	0.0077	0.5	0.513
17	170	0.0060	0.0234	0.2964	0.0000	0.0000	0.1421	0.0185	0.0095	0.7	0.566
18	180	0.0060	0.0234	0.3198	0.0000	0,0000	0 1611	0.0190	0.0098	0.7	0.630
10	100	0.0060	0.0234	0 3432	0.0000	0.0000	0 1805	0.0194	0.0100	0.7	0.66
20	200	0.0000	0.0234	0.3666	0.0000	0.0000	0 2003	0.0109	0.0102	0.7	0.002
20	200	0.0000	0.0234	0.3000	0.0000	0.0000	0.2003	0.0196	0.0102	0.7	0.08
21	210	0.0060	0.0234	0.3900	0.0000	0.0000	0.2204	0.0201	0.0103	0.7	0.696
22	220	0.0060	0.0234	0.4134	0.0000	0.0000	0.2407	0.0203	0.0105	0.7	0.707
23	230	0.0070	0.0273	0.4407	0.0000	0.0000	0.2648	0.0240	0.0124	0.8	0.757
24	240	0.0070	0.0273	0.4680	0.0000	0.0000	0.2891	0.0243	0.0125	0.9	0.821
24	and the second se					the second se	The second se		the second se		
24	250	0.0070	0.0273	0.4953	0.0000	0.0000	0.3136	0.0246	0.0126	0.9	0.848
24 25 26	250 260	0.0070 0.0070	0.0273 0.0273	0.4953 0.5226	0.0000	0.0000	0.3136	0.0246	0.0126 0.0128	0.9 0.9	0.848

	-				Pervious	Area	Impervior	IS Area			
(1) Time ncrement	(2) Time	(3) Rainfall distri- bution	(4) Incre- mental Rainfall	(5) Accumu- lated Rainfall	(6) Accumu- lated Runoff	(7) Incre- mental Runoff	(8) Accumu- lated Runoff	(9) Incre- mental Runoff	(10) Totai Runoff	(11) Instant hydro- graph	(12) design hydro- graph
	1000		10.	ш.	и.	-01.	JIL			CIS	CIS
28	280	0.0070	0.0273	0.5772	0.0023	0.0013	0.3885	0.0251	0.0136	0.9	0.908
29	290	0.0082	0.0320	0.6092	0.0046	0.0023	0.4182	0.0297	0.0163	1.1	0.987
30	300	0.0082	0.0320	0.6412	0.0075	0.0030	0,4480	0.0298	0.0168	1.2	1,086
31	310	0.0082	0.0320	0.6731	0.0112	0.0037	0.4780	0.0300	0.0172	1.2	1,140
32	320	0.0082	0.0320	0.7051	0.0156	0.0043	0.5082	0.0301	0.0176	12	1.176
33	330	0.0082	0.0320	0 7371	0.0205	0.0050	0.5385	0.0303	0.0180	12	1 206
34	340	0.0082	0.0320	0 7691	0.0261	0.0056	0.5689	0.0304	0.0184	13	1 233
35	350	0.0002	0.0371	0.8061	0.0334	0.0072	0.6042	0.0353	0.0217	1.5	1 327
35	360	0.0095	0.0371	0.8432	0.0334	0.0072	0.6307	0.0355	0.0211	1.5	1.445
30	300	0.0095	0.0371	0.0452	0.0414	0.0000	0.0397	0.0355	0.0221	1.5	1.445
3/	370	0.0095	0.0371	0.0002	0.0502	0.0000	0.0752	0.0350	0.0220	1.0	1.504
38	380	0.0095	0.0371	0.91/3	0.0597	0.0095	0.7109	0.0357	0.0230	1.0	1.042
39	390	0.0095	0.0371	0.9543	0.0699	0.0102	0.7467	0.0358	0.0233	1.6	1.5/3
40	400	0.0095	0.03/1	0.9914	0.0807	0.0108	0.7826	0.0359	0.0237	1.6	1.600
41	410	0.0134	0.0523	1.0436	0.0971	0.0164	0.8333	0.0507	0.0340	2.3	1.854
42	420	0.0134	0.0523	1.0959	0.1147	0.0176	0.8841	0.0508	0.0347	2.4	2.189
43	430	0.0134	0.0523	1.1482	0.1334	0.0187	0.9350	0.0509	0.0353	2.4	2.330
44	440	0.0180	0.0702	1.2184	0.1603	0.0269	1.0036	0.0686	0.0483	3.3	2.689
45	450	0.0180	0.0702	1.2886	0.1891	0.0287	1.0723	0.0687	0.0493	3.4	3.129
46	460	0.0340	0.1326	1.4212	0.2480	0.0589	1.2025	0.1302	0.0956	6.6	4.356
47	470	0.0540	0.2106	1.6318	0.3527	0.1047	1.4101	0.2075	0.1575	10.8	7.241
48	480	0.0270	0.1053	1.7371	0.4095	0.0568	1.5141	0.1040	0.0811	5.6	7.870
49	490	0.0180	0.0702	1.8073	0.4489	0.0394	1.5835	0.0694	0.0548	3.8	5.731
50	500	0.0134	0.0523	1.8595	0.4789	0.0300	.1.6352	0.0517	0.0412	2.8	4.106
51	510	0.0134	0.0523	1.9118	0.5095	0.0306	1.6870	0.0517	0.0415	2.8	3.259
52	520	0.0134	0.0523	1.9640	0.5407	0.0312	1.7387	0.0518	0.0418	2.9	2.990
53	530	0.0088	0.0343	1,9984	0.5615	0.0208	1.7727	0.0340	0.0276	1.9	2.583
54	540	0.0088	0.0343	2.0327	0.5825	0.0210	1.8067	0.0340	0.0277	1.9	2,125
55	550	0.0088	0.0343	2 0670	0.6038	0.0212	1.8408	0.0340	0.0278	1.9	1.978
56	560	0.0088	0.0343	2 1013	0.6252	0.0215	1 8748	0.0340	0.0279	1.9	1,934
57	570	0.0088	0.0343	2 1356	0.6469	0.0217	1 9089	0.0340	0.0280	19	1 924
58	580	0.0088	0.0343	2 1700	0.6688	0.0219	1.9429	0.0341	0.0281	1.9	1,926
50	500	0.0088	0.0343	2 2043	0.6909	0.0221	1 9770	0.0341	0.0282	19	1 931
55	600	0.0000	0.0343	2 2396	0.7131	0.0223	20110	0.0341	0.0283	1.0	1 938
61	610	0.0088	0.0343	2 2720	0.7356	0.0225	2 0451	0.0341	0.0200	2.0	1 944
60	620	0.0008	0.0343	2.2729	0.7500	0.0223	2.0401	0.0341	0.0204	2.0	1.051
62	620	0.0000	0.0343	2.3012	0.7911	0.0227	2 1132	0.0341	0.0286	2.0	1 059
00	640	0.0000	0.0343	2.3410	0.0010	0.0220	2 1474	0.0341	0.0200	2.0	1 064
04	640	0.0008	0.0343	2.3/39	0.80042	0.0230	2.14/4	0.0341	0.0207	1.6	1.904
00	000	0.0072	0.0281	2,4040	0.0231	0.0190	2.1755	0.0279	0.0230	1.0	1.000
00	000	0.0072	0.0281	2.4320	0.0422	0.0191	2.2032	0.0279	0.0230	1.0	1.090
67	670	0.0072	0.0281	2.4601	0.8614	0.0192	2.2311	0.0279	0.0237	1.0	1.647
68	680	0.0072	0.0281	2.4882	0.8807	0.0193	2.2590	0.0279	0.0237	1.0	1.033
69	690	0.0072	0.0281	2.5163	0.9002	0.0194	2.2869	0.0279	0.0238	1.0	1.631
70	700	0.0072	0.0281	2.5444	0.9197	0.0195	2.3148	0.0279	0.0238	1.6	1.633
71	710	0.0072	0.0281	2.5724	0.9393	0.0196	2.3428	0.0279	0.0239	1.6	1.636
72	720	0.0072	0.0281	2.6005	0.9591	0.0197	2.3707	0.0279	0.0239	1.6	1.639
73	730	0.0072	0.0281	2.6286	0.9789	0.0198	2.3986	0.0279	0.0240	1.6	1.643
74	740	0.0072	0.0281	2.6567	0.9988	0.0199	2.4266	0.0279	0.0240	1.6	1.646
75	750	0.0072	0.0281	2.6848	1.0189	0.0200	2.4545	0.0279	0.0241	1.7	1.650
76	760	0.0072	0.0281	2.7128	1.0390	0.0201	2.4824	0.0279	0.0241	1.7	1.653
77	770	0.0057	0.0222	2.7351	1.0550	0.0160	2.5045	0.0221	0.0191	1.3	1.541
78	780	0.0057	0.0222	2.7573	1.0711	0.0161	2.5267	0.0221	0.0192	1.3	1.390
79	790	0.0057	0.0222	2.7795	1.0872	0.0161	2.5488	0.0221	0.0192	1.3	1.341
80	800	0.0057	0.0222	2,8018	1.1034	0.0162	2.5709	0.0221	0.0192	1.3	1.326
81	810	0.0057	0.0222	2,8240	1,1196	0.0162	2.5930	0.0221	0.0193	1.3	1.322

82 82 83 83 84 84 85 86 86 87 88 88 89 90 90 91 91 92 92 93 93 94 94 95 95 96 96 97 97 98 98 99 99 99 90 100 100 101 102 102 103 103 103 103 103 104 104 105 106 106 107 107 108 108 109 109 110 111 111 111 112 113 113 113 113 113 113 113 113 113 114 114 115 115 116 116 116 116 117 117 118 118 119 119 120 120 120 121 122 122 123	(2 Tim nt mir) 1e 1.	(3) Rainfall distri- bution	(4) Incre- mental Rainfall in.	(5) Accumu- lated Rainfall in.	(6) Accumu- lated Runoff in.	(7) Incre- mental Runoff in.	(8) Accumu- lated Runoff in.	(9) Incre- mental Runoff in.	(10) Total Runoff in.	(11) Instant hydro- graph cfs	(12) design hydro- graph cfs
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		000	0.0057	0.0000	0.0460	1 1250	0.0462	2 6162	0.0221	0.0102	12	1 200
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2	820	0.0057	0.0222	2.8462	1.1309	0.0103	2.0102	0.0221	0.0193	1.0	1.322
84 84 84 85 86 86 87 87 88 89 99 90 91 91 91 92 92 93 94 94 94 95 95 96 97 97 98 99 99 99 100 100 100 101 101 101 102 103 103 104 104 105 106 106 106 107 108 108 109 109 109 110 110 110 111 111 111 112 112 112 113 113 114 114 114 114 115 116 116 117 117 111 120 120 120	3	830	0.0057	0.0222	2.8685	1.1022	0.0163	2.03/3	0.0221	0.0193	1.3	1.324
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1	840	0.0057	0.0222	2.8907	1.1686	0.0164	2.6594	0.0221	0.0193	1.3	1.320
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5	850	0.0057	0.0222	2.9129	1.1851	0.0164	2.6816	0.0221	0.0194	1.3	1.327
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5	860	0.0057	0.0222	2.9351	1.2016	0.0165	2.7037	0.0221	0.0194	1.3	1.329
88 88 89 90 90 91 91 91 92 92 93 93 94 94 95 95 96 96 97 97 98 98 99 99 100 100 101 102 102 102 102 103 103 103 103 103 104 105 105 106 106 107 108 108 109 109 110 110 110 111 111 112 113 113 114 114 115 116 116 116 116 117 118 118 119 120 120 120 120 120 120 121 121 122 123 123 124 124 125 126 126	7	870	0.0057	0.0222	2.9574	1.2181	0.0166	2.7258	0.0221	0.0194	1.3	1.331
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3	880	0.0057	0.0222	2.9796	1.2347	0.0166	2.7480	0.0221	0.0194	1.3	1.332
90 90 90 91 91 91 92 92 93 93 94 94 95 95 96 96 97 97 98 98 99 99 100 100 100 101 102 102 103 103 104 104 105 105 106 106 106 107 108 108 109 109 110 110 110 110 111 112 113 113 114 114 115 115 116 116 116 117 118 118 119 119 120 120 120 120 121 122 123 123 124 124 124 126 126 126 126 126	9	890	0.0050	0.0195	2.9991	1.2493	0.0146	2.7674	0.0194	0.0171	1.2	1.2/9
91 91 91 92 92 93 93 94 94 95 95 96 96 97 97 98 98 99 99 100 100 101 101 102 102 103 103 104 104 105 105 106 106 107 107 108 108 109 109 110 110 111 111 112 113 113 113 114 114 115 116 116 116 117 118 118 119 119 120 120 120 121 122 123 123 124 124 125 126	2	900	0.0050	0.0195	3.0186	1.2640	0.0146	2.7868	0.0194	0.0171	1.2	1.208
92 92 93 93 94 94 95 95 96 96 97 97 98 98 99 99 100 100 101 102 103 103 104 104 105 106 106 106 107 107 108 108 109 109 110 111 112 112 113 113 114 114 115 116 116 117 118 118 119 120 120 121 122 123 122 123 123 124 124 125 126 126 126	1	910	0.0050	0.0195	3.0381	1.2786	0.0147	2.8062	0.0194	0.0171	1.2	1.185
93 93 94 94 95 95 96 96 97 97 98 98 99 99 100 100 101 101 102 102 103 103 104 104 105 106 107 107 108 108 109 109 110 111 112 112 113 113 114 114 115 116 116 117 118 118 119 119 120 120 121 122 123 123 124 124 124 125 126 126	2	920	0.0050	0.0195	3.0576	1.2934	0.0147	2.8256	0.0194	0.0171	1.2	1.178
94 94 95 95 96 96 97 97 98 98 99 99 100 100 101 101 102 102 103 103 104 104 105 106 107 107 108 108 109 109 110 110 111 112 113 113 114 114 115 116 116 117 118 118 119 119 120 120 122 123 123 124 124 124 125 126 126	3	930	0.0050	0.0195	3.0771	1.3081	0.0148	2.8451	0.0194	0.0172	1.2	1.177
95 95 96 96 97 97 98 98 99 99 100 100 101 101 102 102 103 103 104 104 105 105 106 106 107 107 108 108 109 109 110 110 111 112 113 113 114 114 115 116 116 117 118 118 119 119 120 120 121 122 123 123 124 124 125 126	4	940	0.0050	0.0195	3.0966	1.3229	0.0148	2.8645	0.0194	0.0172	1.2	1.177
96 96 97 97 98 98 99 99 100 100 100 101 101 101 102 103 103 104 104 104 105 105 106 107 107 108 109 109 109 110 110 111 112 112 113 114 114 115 116 116 116 117 118 118 119 119 120 120 120 120 121 122 123 124 124 124 125 126 126	5	950	0.0050	0.0195	3.1161	1.3377	0.0148	2.8839	0.0194	0.0172	1.2	1.178
97 97 98 98 99 99 100 100 101 101 102 102 103 103 104 104 105 105 106 106 107 107 108 108 109 109 110 110 111 111 112 112 113 113 114 114 115 116 116 117 118 118 119 119 120 120 121 122 123 123 124 124 124 125 126 126	6	960	0.0050	0.0195	3.1356	1.3526	0.0149	2.9033	0.0194	0.0172	1.2	1.179
98 98 99 99 100 100 101 101 102 102 103 103 104 104 105 105 106 106 107 107 108 108 109 109 110 110 111 111 112 112 113 113 114 114 115 116 116 116 117 118 119 119 120 120 121 121 122 123 124 124 125 126	7	970	0.0050	0.0195	3.1551	1.3675	0.0149	2.9228	0.0194	0.0172	1.2	1.181
99 99 100 100 101 101 102 102 103 103 104 104 105 105 106 106 107 107 108 108 109 109 110 110 111 111 112 112 113 113 114 114 115 116 116 116 117 118 119 119 120 120 121 122 123 123 124 124 125 126	8	980	0.0050	0.0195	3.1746	1.3824	0.0149	2.9422	0.0194	0.0172	1.2	1.182
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9	990	0.0050	0.0195	3.1941	1.3974	0.0150	2.9616	0.0194	0.0173	1.2	1.183
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 1	000	0.0050	0.0195	3.2136	1.4124	0.0150	2.9810	0.0194	0.0173	1.2	1.184
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 1	010	0.0040	0.0156	3.2292	1.4244	0.0120	2.9966	0.0155	0.0138	0.9	1.106
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 1	020	0.0040	0.0156	3.2448	1.4365	0.0120	3.0121	0.0155	0.0138	0.9	1.002
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3 1	030	0.0040	0.0156	3.2604	1.4485	0.0121	3.0277	0.0155	0.0139	1.0	0.967
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4 1	040	0.0040	0.0156	3.2760	1.4606	0.0121	.3.0432	0.0155	0.0139	1.0	0.956
106 106 107 107 108 109 109 109 110 110 111 111 112 112 113 113 114 114 115 116 116 116 117 118 119 119 120 120 121 121 122 123 124 124 125 126	5 1	050	0.0040	0.0156	3.2916	1.4727	0.0121	3.0588	0.0155	0.0139	1.0	0.953
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6 1	060	0.0040	0.0156	3.3072	1.4848	0.0121	3.0743	0.0155	0.0139	1.0	0.953
108 108 109 109 110 110 111 111 112 112 113 113 114 114 115 115 116 116 117 117 118 118 119 119 120 120 121 121 122 123 123 123 124 125 126 126	7 1	070	0.0040	0.0156	3.3228	1,4970	0.0121	3.0898	0.0155	0.0139	1.0	0.953
109 109 110 110 111 111 112 112 113 113 114 114 115 115 116 116 117 118 119 119 120 120 121 121 122 123 123 123 124 124 125 126	R 1	080	0.0040	0.0156	3.3384	1.5092	0.0122	3,1054	0.0155	0.0139	1.0	0.953
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9 1	090	0.0040	0.0156	3,3540	1.5214	0.0122	3,1209	0.0155	0.0139	1.0	0.954
111 111 112 112 113 113 114 114 115 115 116 116 117 117 118 118 119 119 120 120 121 122 123 123 124 124 125 125 126 126	0 1	100	0.0040	0.0156	3.3696	1.5336	0.0122	3,1365	0.0155	0.0139	1.0	0.955
112 112 113 113 114 114 115 115 116 116 117 117 118 118 119 119 120 120 121 121 122 123 124 124 125 126	1 1	110	0.0040	0.0156	3.3852	1.5458	0.0122	3,1520	0.0155	0.0139	1.0	0.955
113 113 114 114 115 115 116 116 117 117 118 118 119 119 120 120 121 121 122 122 123 123 124 124 125 125 126 126	2 1	120	0.0040	0.0156	3 4008	1,5580	0.0122	3.1676	0.0155	0.0139	1.0	0.956
114 114 115 115 116 116 117 117 118 118 119 119 120 120 121 121 122 122 123 123 124 124 125 125 126 126	3 1	130	0.0040	0.0156	3.4164	1.5703	0.0123	3,1831	0.0155	0.0140	1.0	0.957
115 115 116 116 117 117 118 118 119 119 120 120 121 121 122 122 123 123 124 124 125 125 126 126	4 1	140	0.0040	0.0156	3 4320	1.5826	0.0123	3,1987	0.0155	0.0140	1.0	0.957
116 116 117 117 118 118 119 119 120 120 121 121 122 122 123 123 124 124 125 125 126 126	5 1	150	0.0040	0.0156	3 4476	1 5949	0.0123	3 2142	0.0155	0.0140	1.0	0.958
117 117 118 118 119 119 120 120 121 121 122 122 123 123 124 124 125 125	5 1	160	0.0040	0.0156	3 4632	1.6072	0.0123	3,2298	0.0156	0.0140	1.0	0.959
118 118 119 119 120 120 121 121 122 122 123 123 124 124 125 125	7 1	170	0.0040	0.0156	3 4788	1 6196	0.0123	3 2453	0.0156	0.0140	1.0	0.959
110 110 119 119 120 120 121 121 122 122 123 123 124 124 125 125	a 1	180	0.0040	0.0156	3 4944	1 6319	0.0124	3 2609	0.0156	0.0140	1.0	0.960
120 120 121 121 122 122 123 123 124 124 125 125 126 126	a 1	190	0.0040	0.0156	3 5100	1 6443	0 0124	3 2764	0.0156	0.0140	10	0.961
120 120 121 121 122 122 123 123 124 124 125 125 126 126	0 1	200	0.0040	0.0156	3 5256	1 6567	0.0124	3 2920	0.0156	0.0140	10	0.961
122 122 123 123 124 124 125 125 126 126	1 1	210	0.0040	0.0156	3 5412	1.6691	0.0124	3.3075	0.0156	0.0140	1.0	0.962
123 123 124 124 125 125 126 126	2 4	220	0.0040	0.0156	3 5568	1 6815	0.0124	3 3231	0.0156	0.0140	10	0.962
124 124 125 125 126 126	3 4	230	0.0040	0.0156	3 5724	1 6940	0.0125	3,3387	0.0156	0.0140	1.0	0.963
125 125	4 1	240	0.0040	0.0156	3 5880	1 7065	0.0125	3.3542	0.0156	0.0141	1.0	0.964
125 125	5 4	250	0.0040	0.0156	3 6036	1 7100	0.0125	3 3698	0.0156	0.0141	10	0.964
		260	0.0040	0.0156	3 6102	1 7315	0.0125	3 3853	0.0156	0.0141	1.0	0.965
127 127	7 4	270	0.0040	0.0156	3 6349	1 7440	0.0125	3 4000	0.0156	0.0141	1.0	0.965
120 120		280	0.0040	0.0156	3 6504	1 7565	0.0125	3 4164	0.0156	0.0141	10	0.966
120 120		200	0.0040	0.0150	3.0004	1 7601	0.0125	3 /320	0.0156	0.0141	1.0	0.000
129 129		200	0.0040	0.0150	3.0000	1 7916	0.0120	3 1175	0.0156	0.0141	1.0	0.907
130 130		300	0.0040	0.0156	3.0010	1.7010	0.0120	3,4473	0.0150	0.0141	1.0	0.907
131 131	1 1	310	0.0040	0.0156	3.09/2	1.7942	0.0120	3.4031	0.0150	0.0141	1.0	0.900
132 132	c 1	320	0.0040	0.0156	3.7128	1.0008	0.0120	3.4/00	0.0150	0.0141	1.0	0.900
133 133	5 1	330	0.0040	0.0156	3.7284	1.0195	0.0126	3.4942	0.0150	0.0141	1.0	0.909

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	(2)		100	Pervious	Area	Imperviou	is Area	(10)	22.22	1920
(2) Time	(3) Rainfall distri-	(4) Incre- mental Rainfall	(5) Accumu- lated Rainfall	(6) Accumu- lated Runoff	(7) Incre- mental Runoff	(8) Accumu- lated Rupoff	(9) Incre- mental Runoff	(10) Total Runoff	(11) Instant hydro- graph	(12) design hydro-
min.	button	in.	in.	in.	in.	in.	in.	in.	cfs	Cfs
1350	0.0040	0.0156	3.7596	1.8447	0.0127	3.5253	0.0156	0.0141	1.0	0.970
1360	0.0040	0.0156	3.7752	1.8574	0.0127	3.5409	0.0156	0.0142	1.0	0.971
1370	0.0040	0.0156	3.7908	1.8701	0.0127	3.5564	0.0156	0.0142	1.0	0.971
1380	0.0040	0.0156	3.8064	1.8828	0.0127	3.5720	0.0156	0.0142	1.0	0.972
1390	0.0040	0.0156	3.8220	1.8955	0.0127	3.5876	0.0156	0.0142	1.0	0.972
1400	0.0040	0.0156	3.8376	1.9082	0.0127	3.6031	0.0156	0.0142	1.0	0.973
1410	0.0040	0.0156	3.8532	1.9210	0.0127	3.6187	0.0156	0.0142	1.0	0.973
1420	0.0040	0.0156	3.8688	1.9338	0.0128	3.6342	0.0156	0.0142	1.0	0.974
1430	0.0040	0.0156	3.8844	1.9465	0.0128	3.6498	0.0156	0.0142	1.0	0.974
1440	0.0040	0.0156	3.9000	1.9593	0.0128	3.6654	0.0156	0.0142	1.0	0.975
							Total Vo	lume of R	unoff =	116173.469 cu. ft.
						(cu.ft.)	(Found t multiply convers SUM(Q in cubic V = SUI = (cu.ft/s)	by summin ing by 600 ion require) in cfs to t feet as fo $M(Q) \times dt$ $\times (10 min$	ing this colu 0, 600 is the d to convector total volum llows: .) x (60 s/m	imn and e ert ne nin.)
	(2) Time min. 1350 1360 1370 1380 1400 1410 1420 1430 1440	(2) (3) Time Rainfall distri- bution min. 1350 0.0040 1360 0.0040 1370 0.0040 1380 0.0040 1400 0.0040 1410 0.0040 1420 0.0040 1430 0.0040 1440 0.0040	(2) (3) (4) Time Rainfall distri- bution Incre- mental Rainfall in. 1350 0.0040 0.0156 1360 0.0040 0.0156 1370 0.0040 0.0156 1380 0.0040 0.0156 1390 0.0040 0.0156 1400 0.0040 0.0156 1410 0.0040 0.0156 1420 0.0040 0.0156 1430 0.0040 0.0156 1440 0.0040 0.0156	(2) Time (3) Rainfall distri- bution (4) Incre- mental Rainfall in. (5) Accumu- lated Rainfall in. 1350 0.0040 0.0156 3.7596 1360 0.0040 0.0156 3.7596 1360 0.0040 0.0156 3.7598 1370 0.0040 0.0156 3.7908 1380 0.0040 0.0156 3.8064 1390 0.0040 0.0156 3.8376 1410 0.0040 0.0156 3.8532 1420 0.0040 0.0156 3.8688 1430 0.0040 0.0156 3.8844 1440 0.0040 0.0156 3.9000	(2) (3) (4) (5) (6) Time Rainfall distri- bution Incre- Rainfall Accumu- lated Accumu- lated 1350 0.0040 0.0156 3.7596 1.8447 1360 0.0040 0.0156 3.7596 1.8447 1360 0.0040 0.0156 3.7596 1.8447 1370 0.0040 0.0156 3.7908 1.8701 1380 0.0040 0.0156 3.8064 1.8828 1390 0.0040 0.0156 3.8376 1.9082 1410 0.0040 0.0156 3.8376 1.9082 1410 0.0040 0.0156 3.8688 1.9338 1430 0.0040 0.0156 3.8844 1.9465 1440 0.0040 0.0156 3.9000 1.9593	(2) (3) (4) (5) (6) (7) Time Rainfall Incre- bution Accumu- Rainfall Iated Rainfall Accumu- lated Incre- mental 1350 0.0040 0.0156 3.7596 1.8447 0.0127 1360 0.0040 0.0156 3.7752 1.8574 0.0127 1370 0.0040 0.0156 3.7908 1.8701 0.0127 1380 0.0040 0.0156 3.8064 1.8828 0.0127 1380 0.0040 0.0156 3.8376 1.9082 0.0127 1400 0.0040 0.0156 3.8376 1.9082 0.0127 1410 0.0040 0.0156 3.8532 1.9210 0.0127 1420 0.0040 0.0156 3.8688 1.9338 0.0128 1430 0.0040 0.0156 3.8000 1.9593 0.0128 1440 0.0040 0.0156 3.9000 1.9593 0.0128	(2) (3) (4) (5) (6) (7) (8) Time Rainfall Incre- distri- bution Accumu- Rainfall Accumu- lated Incre- Runoff Accumu- mental Incre- lated Accumu- mental Incre- mental Accumu- lated Incre- mental Incre- mental Accumu- lated Incre- mental Accumu- lated Incre- mental Accumu- lated Incre- mental Incre- Runoff Incre- Runoff Incre- Runoff <td< td=""><td>(2) (3) (4) (5) (6) (7) (8) (9) Time Rainfall Incre- bution Accumu- mental Accumu- lated Incre- mental Accumu- lated Incre- mental Accumu- mental Incre- mental Accumu- mental Incre- mental Accumu- mental Incre- mental 1350 0.0040 0.0156 3.7596 1.8447 0.0127 3.5253 0.0156 1360 0.0040 0.0156 3.7752 1.8574 0.0127 3.5409 0.0156 1370 0.0040 0.0156 3.8064 1.8828 0.0127 3.5720 0.0156 1380 0.0040 0.0156 3.8220 1.8955 0.0127 3.6371 0.0156 1400 0.0040 0.0156 3.8376 1.9082 0.0127 3.6187 0.0156 1420 0.0040 0.0156 3.8000 1.9593 0.0128 3.6498 0.0156 1430 0.0040 0.0156 3.9000 1.9593 0.0128 <</td><td>(2) (3) (4) (5) (6) (7) (8) (9) (10) Time Rainfall Incre- Accumu- Incre- Accumu- Incre- Incre-</td><td>(2) (3) (4) (5) (6) (7) (8) (9) (10) (11) Time Rainfall Incre- bution Accumu- lated Accumu- lated Incre- mental Accumu- lated Incre- mental Total Instant 1350 0.0040 0.0156 3.7596 1.8447 0.0127 3.5253 0.0156 0.0141 1.0 1360 0.0040 0.0156 3.7752 1.8574 0.0127 3.5253 0.0156 0.0142 1.0 1370 0.0040 0.0156 3.7908 1.8701 0.0127 3.5564 0.0156 0.0142 1.0 1380 0.0040 0.0156 3.8064 1.8828 0.0127 3.5720 0.0156 0.0142 1.0 1400 0.0040 0.0156 3.8237 1.9082 0.0127 3.6311 0.0156 0.0142 1.0 1440 0.0040 0.0156 3.8232 1.9210 0.0127 3.6317 0.0156 0.0142 1.0</td></td<>	(2) (3) (4) (5) (6) (7) (8) (9) Time Rainfall Incre- bution Accumu- mental Accumu- lated Incre- mental Accumu- lated Incre- mental Accumu- mental Incre- mental Accumu- mental Incre- mental Accumu- mental Incre- mental 1350 0.0040 0.0156 3.7596 1.8447 0.0127 3.5253 0.0156 1360 0.0040 0.0156 3.7752 1.8574 0.0127 3.5409 0.0156 1370 0.0040 0.0156 3.8064 1.8828 0.0127 3.5720 0.0156 1380 0.0040 0.0156 3.8220 1.8955 0.0127 3.6371 0.0156 1400 0.0040 0.0156 3.8376 1.9082 0.0127 3.6187 0.0156 1420 0.0040 0.0156 3.8000 1.9593 0.0128 3.6498 0.0156 1430 0.0040 0.0156 3.9000 1.9593 0.0128 <	(2) (3) (4) (5) (6) (7) (8) (9) (10) Time Rainfall Incre- Accumu- Incre- Accumu- Incre- Incre-	(2) (3) (4) (5) (6) (7) (8) (9) (10) (11) Time Rainfall Incre- bution Accumu- lated Accumu- lated Incre- mental Accumu- lated Incre- mental Total Instant 1350 0.0040 0.0156 3.7596 1.8447 0.0127 3.5253 0.0156 0.0141 1.0 1360 0.0040 0.0156 3.7752 1.8574 0.0127 3.5253 0.0156 0.0142 1.0 1370 0.0040 0.0156 3.7908 1.8701 0.0127 3.5564 0.0156 0.0142 1.0 1380 0.0040 0.0156 3.8064 1.8828 0.0127 3.5720 0.0156 0.0142 1.0 1400 0.0040 0.0156 3.8237 1.9082 0.0127 3.6311 0.0156 0.0142 1.0 1440 0.0040 0.0156 3.8232 1.9210 0.0127 3.6317 0.0156 0.0142 1.0

	Date.	37948.00	PC	OND ROUTING						
	Given:		Project = W	OOD MS - 25-YEAR		in states			1000	
	Ave	rage Pond Lo	ength (ft) =	120.000		System:	Pond 120' I	ong x 50'	wide	
	AV	erage Pond V	V(dtn(n) =	50.000						
		Drifice 2 Dia	meter (ft) =	1,000						
		Height to	Orifice 2 =	1.650						
	1	neight to	Office 2 -	1.000						
		Orifice 2 Are	а	0.785 SF						
		Orifice 1 Are	a =	0.238 SF						
		Avg Pond Ar	ea =	6000.000 SF						
		Column (3) =	Starting Pond	- Incremental CFS Into Po	ing Pond	Denth = C	01 (11)			
		Column $(5) =$	= Glarding r ond		ing rono	ocpan - or	ortin			
		Column (6) =	= 2 * g * Startin	gh						
		Column (7) =	Square Root	of 2gh						
		Column (8) =	Incremental V	/ol out = Col (7) * 0.60 * Or	ifice Area	* 600				
		Column (9) =	Delta Vol = In	cremental Vol in - Increme	ntal Vol o	out = Col (3) - Col (8)			
		Column (10)	= Remaining F	Pond Vol = Previous Remai	ning Vol	+ Col (9)				
		Column (11)	= Pond Depth	at End of Interval = Col (J)	/ Pond A	rea				
		Column (12)	- Fond GF3 L	ischarge - col(o) / coo						
-			ale.		6.0	140				
(1) Time	(2) Time	(3)	(4) Starting	(6)	(7)	(8)	(6a)			(9) Delta
Time	Time	increm.	Starting			increm.				Vol
nrien		VOLIDIO	Pond			VOL 1 OUT				V/ 6 11
ncrem.		Pond	Depth			Pond				VOI
increm.	min.	Vol into Pond cf	Depth ft.			Pond cf				cf
1	min. 10	Vol into Pond cf 0.00	Depth ft.	0.000	0.000	Pond cf 0.000	-106.26	0.000	0.000	cf 0.00
1 2	min. 10 20	Vol into Pond cf 0.00 0.00	0.000 0.000	0.000 0.000	0.000	0.000 0.000	-106.26 -106.26	0.000	0.000	0.00
1 2 3	min. 10 20 30	Vol into Pond cf 0.00 0.00 1.20	0.000 0.000 0.000 0.000	0.000 0.000 0.000	0.000 0.000 0.000	0.000 0.000 0.000 0.000	-106.26 -106.26 -106.26	0.000 0.000 0.000	0.000 0.000 0.000	0.00 0.00 0.00
1 2 3 4	min. 10 20 30 40	0.00 0.00 0.00 1.20 14.96	0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.013	0.000 0.000 0.000 0.114	Vol 1 out Pond cf 0.000 0.000 0.000 9.716	-106.26 -106.26 -106.26 -106.25	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25
1 2 3 4 5	min. 10 20 30 40 50	Vol into Pond cf 0.00 0.00 1.20 14.96 44.21	0.000 0.000 0.000 0.000 0.000 0.000 0.001	0.000 0.000 0.000 0.013 0.069	0.000 0.000 0.114 0.263	0.000 0.000 0.000 0.000 9.716 22.503	-106.26 -106.26 -106.26 -106.25 -106.19	0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21.71
1 2 3 4 5 6	min. 10 20 30 40 50 60	Vol into Pond cf 0.00 0.00 1.20 14.96 44.21 76.69	0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.005	0.000 0.000 0.000 0.013 0.069 0.302	0.000 0.000 0.114 0.263 0.550	Vol 1 out Pond cf 0.000 0.000 0.000 9.716 22.503 47.020	-106.26 -106.26 -106.26 -106.25 -106.19 -105.96	0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29.67
1 2 3 4 5 6 7	min. 10 20 30 40 50 60 70	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21	0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010	0.000 0.000 0.013 0.069 0.302 0.621	0.000 0.000 0.114 0.263 0.550 0.788	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21.71 29.67 38.83
1 2 3 4 5 6 7 8	min. 10 20 30 40 50 60 70 80	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61	0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016	0.000 0.000 0.013 0.069 0.302 0.621 1.037	0.000 0.000 0.114 0.263 0.550 0.788 1.019	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29,67 38.83 44.50
1 2 3 4 5 6 7 8 9	min. 10 20 30 40 50 60 70 80 90	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17	0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29,67 38,83 44,50 47,90
1 2 3 4 5 6 7 8 9 10	min. 10 20 30 40 50 60 70 80 90 100	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48	0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.024 0.032	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21.71 29.67 38.83 44.50 47.90 49.64
1 2 3 4 5 6 7 8 9 10 11	min. 10 20 30 40 50 60 70 80 90 100 110	Vol into Pond cf 0.00 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52	Pond Depth ft. 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21.71 29.67 38.83 44.50 47.90 49.64 67.62
1 2 3 4 5 6 7 8 9 10 11 12	min. 10 20 30 40 50 60 70 80 90 100 110 120	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11	Pond Depth ft. 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 5.25 21,71 29.67 38.83 44.50 47.90 49.64 67.62 88.03
1 2 3 4 5 6 7 8 9 10 11 12 13	min. 10 20 30 40 50 60 70 80 90 100 110 120 130	Vol into Pond cf 0.00 0.00 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62	Pond Depth ft. 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65
1 2 3 4 5 6 7 8 9 10 11 12 13 14	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140	Vol into Pond cf 0.00 0.00 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48	Pond Depth ft. 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65 88.34
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 296.83	Pond Depth ft. 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481	Voi 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05 -100.11	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65 88.34 84.66
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160	Vol into Pond cf 0.00 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95	Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110	0.000 0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.062	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05 -100.11 -99.20	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65 88.34 84.66 80.65
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170	Vol into Pond cf 0.00 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95 339.48	Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.062 7.928	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658 2.816	Voi 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298 240.826	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05 -100.11 -99.20 -98.33	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65 88.34 84.66 80.65 98.66
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180	Vol into Pond cf 0.00 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95 339.48 378.06 202.10	Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123 0.140	0.000 0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.928 8.987	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658 2.816 2.998	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298 240.826 256.405	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05 -100.11 -99.20 -98.33 -97.27	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21.71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65 88.34 84.66 80.65 98.66 121.65
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95 339.48 378.06 397.10	Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123 0.140 0.160	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.062 7.928 8.987 10.293	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658 2.816 2.998 3.208	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298 240.826 256.405 274.400	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05 -100.11 -99.20 -98.33 -97.27 -95.97	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29,67 38,83 44,50 47,90 49,64 67,62 88,03 90,65 88,34 84,66 80,65 98,66 121,65 122,70
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95 339.48 378.06 397.10 408.79	Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123 0.140 0.180 0.180	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.062 7.928 8.987 10.293 11.610	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658 2.816 2.998 3.208 3.208	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298 240.826 256.405 274.400 291.427	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05 -100.11 -99.20 -98.33 -97.27 -95.97 -94.65	0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29,67 38,83 44,50 47,90 49,64 67,62 88,03 90,65 88,34 84,66 80,65 98,66 121,65 122,70 117,36
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95 339.48 378.06 397.10 408.79 417.33	Pond Depth ft. 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123 0.140 0.123 0.140 0.180 0.200	0.000 0.000 0.000 0.003 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.062 7.928 8.987 10.293 11.610 12.869	0.000 0.000 0.114 0.263 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658 2.816 2.998 3.208 3.407 3.587	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298 240.826 256.405 274.400 291.427 306.830	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05 -100.11 -99.20 -98.33 -97.27 -95.97 -94.65 -93.39	0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	cf 0.00 0.00 1.20 5.25 21,71 29,67 38,83 44,50 47,90 49,64 67,62 88,03 90,65 88,34 84,66 80,65 98,66 121,65 122,70 117,36 110,50
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95 339.48 378.06 397.10 408.79 417.33 424.25	Pond Depth ft. 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123 0.140 0.123 0.140 0.180 0.200 0.218 0.200	0.000 0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.062 7.928 8.987 10.293 11.610 12.869 14.055	0.000 0.000 0.114 0.263 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658 2.816 2.998 3.208 3.407 3.587 3.749	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298 240.826 256.405 274.400 291.427 306.830 320.657	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05 -100.11 -99.20 -98.33 -97.27 -95.97 -94.65 -93.39 -92.20	0.000 0.000	0.000 0.000	cf 0.00 0.00 1.20 5.25 21.71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65 88.34 84.66 80.65 98.66 121.65 122.70 117.36 110.50 103.59
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95 339.48 378.06 397.10 408.79 417.33 424.25 454.49	Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123 0.140 0.123 0.140 0.160 0.180 0.200 0.218 0.236	0.000 0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.062 7.928 8.987 10.293 11.610 12.869 14.055 15.167	0.000 0.000 0.114 0.263 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658 2.816 2.998 3.208 3.407 3.587 3.749 3.895	Voi 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298 240.826 256.405 274.400 291.427 306.830 320.657 333.099	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05 -100.11 -99.20 -98.33 -97.27 -95.97 -94.65 -93.39 -92.20 -91.09	0.000 0.000	0.000 0.000	cf 0.00 0.00 1.20 5.25 21.71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65 88.34 84.66 80.65 98.66 121.65 122.70 117.36 110.50 103.59 121.39
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 24	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95 339.48 378.06 397.10 408.79 417.33 424.25 454.49 492.59	Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123 0.140 0.123 0.140 0.160 0.180 0.200 0.218 0.236 0.256	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.062 7.928 8.987 10.293 11.610 12.869 14.055 15.167 16.470	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658 2.816 2.998 3.208 3.407 3.587 3.749 3.895 4.058	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298 240.826 256.405 274.400 291.427 306.830 320.657 333.099 347.112	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -104.23 -103.70 -102.97 -102.03 -101.05 -100.11 -99.20 -98.33 -97.27 -95.97 -94.65 -93.39 -92.20 -91.09 -89.79	0.000 0.000	0.000 0.000	cf 0.00 0.00 1.20 5.25 21.71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65 88.34 84.66 80.65 98.66 121.65 122.70 117.36 110.50 103.59 121.39 121.39
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 250 250 250 250 250 250 25	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95 339.48 378.06 397.10 408.79 417.33 424.25 454.49 492.59 509.03	Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123 0.140 0.123 0.140 0.160 0.180 0.200 0.218 0.236 0.256 0.280	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.062 7.928 8.987 10.293 11.610 12.869 14.055 15.167 16.470 18.032	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658 2.816 2.998 3.208 3.407 3.587 3.749 3.895 4.058 4.246	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298 240.826 256.405 274.400 291.427 306.830 320.657 333.099 347.112 363.194	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -105.22 -104.74 -105.22 -104.74 -105.22 -104.74 -105.27 -102.03 -101.05 -100.11 -99.20 -98.33 -97.27 -95.97 -94.65 -93.39 -92.20 -91.09 -88.23	0.000 0.000	0.000 0.000	cf 0.00 0.00 1.20 5.25 21.71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65 88.34 87.62 88.03 90.65 88.34 80.65 98.66 121.65 122.70 117.36 110.50 103.59 121.39 145.48 145.84
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	min. 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 260 270 270 270 270 270 270 270 27	Vol into Pond cf 0.00 1.20 14.96 44.21 76.69 106.21 131.61 153.17 171.48 204.52 243.11 266.62 283.48 296.83 307.95 339.48 378.06 397.10 408.79 417.33 424.25 454.49 492.59 509.03 519.14	Pond Depth ft. 0.000 0.000 0.000 0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123 0.140 0.160 0.180 0.200 0.218 0.236 0.256 0.280 0.304	0.000 0.000 0.013 0.069 0.302 0.621 1.037 1.515 2.029 2.562 3.288 4.233 5.206 6.154 7.062 7.928 8.987 10.293 11.610 12.869 14.055 15.167 16.470 18.032 19.597	0.000 0.000 0.114 0.263 0.550 0.788 1.019 1.231 1.424 1.601 1.813 2.057 2.282 2.481 2.658 2.816 2.998 3.208 3.407 3.587 3.749 3.895 4.058 4.246 4.427	Vol 1 out Pond cf 0.000 0.000 9.716 22.503 47.020 67.383 87.116 105.276 121.835 136.901 155.084 175.963 195.144 212.173 227.298 240.826 256.405 274.400 291.427 306.830 320.657 333.099 347.112 363.194 378.630	-106.26 -106.26 -106.25 -106.19 -105.96 -105.64 -105.22 -104.74 -105.22 -104.74 -105.22 -104.74 -105.22 -104.74 -105.22 -102.03 -102.97 -102.03 -101.05 -100.11 -99.20 -98.33 -97.27 -95.97 -94.65 -93.39 -92.20 -91.09 -88.23 -86.66	0.000 0.000	0.000 0.000	cf 0.00 0.00 1.20 5.25 21.71 29.67 38.83 44.50 47.90 49.64 67.62 88.03 90.65 88.34 87.62 88.03 90.65 121.65 122.70 117.36 110.50 103.59 121.39 145.48 145.84 140.51

Time Increm.	(2) Time	(3) Increm. Vol into Pond	(4) Starting Pond Depth	(6)	(7)	(8) Increm. Vol out Pond				(9) Delta Vol
	min.	CT	π.		-	Cf	-		-	CI
28	280	544.50	0.351	22.583	4.752	406.449	-83.68	0.000	0.000	138.0
29	290	592.01	0.374	24.064	4.906	419.571	-82.20	0.000	0.000	172.4
30	300	651.86	0.402	25.915	5.091	435.408	-80.34	0.000	0.000	216.4
31	310	683.70	0.438	28.238	5.314	454.506	-78.02	0.000	0.000	229.2
32	320	705.59	0.477	30.699	5.541	473.890	-75.56	0.000	0.000	231.7
33	330	723.60	0.515	33.185	5.761	492.711	-73.07	0.000	0.000	230.8
34	340	739.81	0.554	35.664	5.972	510.778	-70.60	0.000	0.000	229.0
35	350	796.05	0.592	38.122	6.174	528.088	-68.14	0.000	0.000	267.9
36	360	866.72	0.637	40.998	6.403	547.647	-65.26	0.000	0.000	319.0
37	370	902.11	0.690	44.423	6.665	570.062	-61.84	0.000	0.000	332.0
38	380	925.17	0.745	47.987	6.927	592.488	-58.27	0.000	0.000	332.6
39	390	943.61	0.801	51.558	7.180	614.137	-54.70	0.000	0.000	329.4
40	400	960.02	0.855	55.094	7.423	634.849	-51.17	0.000	0.000	325.1
41	410	1112.14	0.910	58.584	7.654	654.649	-47.68	0.000	0.000	457.4
42	420	1313.47	0.986	63,495	7.968	681.533	-42.77	0.000	0.000	631.9
43	430	1398.05	1.091	70.277	8.383	717.012	-35.98	0.000	0.000	681.0
44	440	1613.52	1,205	77.587	8.808	753.379	-28.67	0.000	0.000	860.1
45	450	1877.56	1.348	86.819	9.318	796,942	-19.44	0.000	0.000	1080.6
46	460	2613.84	1.528	98.418	9,921	848,508	-7.84	0.000	0.000	1765.3
47	470	4344 37	1 822	117 366	10.834	926 594	11.11	3 333	942,254	2475.5
48	480	4722 30	2 235	143 936	11 997	********	37 68	6 138	1735 512	1960.6
40	400	3438 74	2 562	164 981	12 844	********	58 72	7 663	2166 651	173.5
50	500	2463 42	2 591	166 843	12 917	*********	60.58	7 784	2200 738	-842.0
51	510	1955 35	2 450	157 804	12 562	********	51.54	7 179	2029 945	-1149.0
52	520	1704 14	2 250	145 472	12.002	********	39.21	6 262	1770 519	-1007.9
52	520	1540 71	2.200	134 653	11 604	002 400	28 30	5 328	1506 595	-040 3
55	540	1075 17	1 033	124 463	11 156	054 108	18 20	4 266	1206 317	-885 3
54	540	1196.92	1.335	114.960	10 722	917 048	8 70	2 950	833 075	-564.2
55	550	1160.02	1.705	109.004	10.722	802 568	2.64	1.626	450 773	-101 8
50	500	1164.67	1.091	106.904	10.450	994 097	0.59	0 765	216 107	54.3
50	570	1154.07	1.009	107.428	10.355	886 400	1.17	1 081	305 620	36 4
50	500	1153.07	1.000	107.420	10.305	884 883	0.78	0.882	240 252	24.7
59	590	1162.00	1.002	107.037	10.340	885.070	1.04	1 021	288 697	11 0
00	600	1102.70	1.000	107.302	10.359	995 440	0.04	0.056	270 321	10.0
01	610	1100.09	1.004	107.174	10.352	003.449	1.02	1.016	297 127	2.4
62	620	1170.07	1.000	107.291	10.350	005.933	1.03	1.010	207.137	5.2
63	630	1174.58	1.000	107.200	10.357	000.027	1.01	1.003	203.330	1.0
64	640	1178.40	1.000	107.322	10.300	000.000	1.00	1.030	291.322	69.7
65	650	1110.17	1.007	107.333	10.300	000.103	1.07	1.030	162 550	-00.7
66	660	1017.48	1.055	106.595	10.324	003.032	0.33	0.140	103.550	-29.1
67	670	988.17	1.650	106.282	10.309	881.750	0.02	0.148	41.941	142 5
68	680	979.94	1.661	106.974	10.343	884.622	0.71	0.845	238.910	-143.5
69	690	978.72	1.63/	105.433	10.268	8/8.22/	-0.83	0.000	0.000	100.4
70	700	979.80	1.654	106.511	10.320	882.707	0.25	0.501	141.758	-44.0
71	710	981.62	1.646	106.032	10.297	880.719	-0.23	0.000	0.000	100.9
72	720	983.66	1.663	107.115	10.350	885.205	0.85	0.925	201.436	-162.9
73	730	985.75	1.636	105.366	10.265	8/7.94/	-0.89	0.000	0.000	107.8
74	740	987.82	1.654	106.523	10.321	882.754	0.26	0.513	144.920	-39.8
75	750	989.87	1.647	106.095	10.300	880.980	-0.17	0.000	0.000	108.8
76	760	991.89	1.666	107.264	10.357	885.820	1.00	1.002	283.275	-177.2
77	770	924.66	1.636	105.362	10.265	877.931	-0.90	0.000	0.000	46.7
78	780	834.09	1.644	105.863	10.289	880.018	-0.40	0.000	0.000	-45.9
79	790	804.69	1.636	105.370	10.265	877.966	-0.89	0.000	0.000	-73.2
80	800	795.67	1.624	104.584	10.227	874.683	-1.68	0.000	0.000	-79.0
81	810	793.44	1.611	103.736	10.185	871.130	-2.52	0.000	0.000	-77.6

(1) Time Increm.	(2) Time	(3) Increm. Vol into Pond	(4) Starting Pond Deoth	(6)	(7)	(8) Increm. Vol out Pond				(9) Delta Vol
	min.	cf	ft.			cf				cf
82	820	793.46	1.598	103.736	10.185	871.130	-3.36	0.000	0.000	-77.67
83	830	794.21	1.585	102.068	10.103	864.100	-4.19	0.000	0.000	-69.89
84	840	795.20	1.573	101.318	10.066	860.919	-4.94	0.000	0.000	-65.71
85	850	796.26	1.562	100.613	10.031	857.917	-5.65	0.000	0.000	-61.65
86	860	797 34	1.552	99 951	9 998	855.091	-6.31	0.000	0.000	-57.75
87	870	798.40	1.542	99.331	9,966	852,435	-6.93	0.000	0.000	-54.03
88	880	799.46	1 533	98,751	9,937	849,943	-7.51	0.000	0.000	-50.48
89	890	767 67	1.525	98,209	9,910	847.608	-8.05	0.000	0.000	-79.93
90	900	724 85	1.512	97.351	9 867	843 898	-8.91	0.000	0.000	-119.05
91	910	711.10	1.492	96.074	9.802	838.341	-10.19	0.000	0.000	-127.25
92	920	707 02	1 471	94 708	9.732	832.361	-11.55	0.000	0.000	-125.34
93	930	706 17	1 450	93 363	9 662	826.428	-12.90	0.000	0.000	-120.26
94	940	706 39	1 430	92 072	9 595	820 695	-14.19	0.000	0.000	-114 31
95	950	706.95	1 411	90.845	9 531	815 209	-15.42	0.000	0.000	-108 25
96	060	707.63	1 393	89 683	9 470	809 979	-16.58	0.000	0.000	-102.35
07	970	708 34	1 376	88 584	9 412	805.003	-17 68	0.000	0.000	-96.66
08	080	709.06	1 359	87 547	9 357	800 275	-18 71	0.000	0.000	-91 22
90	990	709 77	1 344	86 568	9 304	795 787	-19 69	0.000	0.000	-86.02
100	1000	710 47	1.330	85 645	9 254	791.532	-20.62	0.000	0.000	-81.06
101	1010	663.69	1 316	84 774	9 207	787 501	-21 49	0.000	0.000	-123.81
102	1020	601.00	1 296	83 446	9 135	781 304	-22.81	0.000	0.000	-180.31
102	1020	580.39	1 266	81 510	9 028	772 191	-24 75	0.000	0.000	-191.80
104	1040	573.81	1 234	79 452	8 914	762 377	-26.81	0.000	0.000	-188.57
105	1050	571.90	1 202	77 428	8 799	752 604	-28 83	0.000	0.000	-180.71
105	1060	571.54	1 172	75 488	8 688	743 118	-30 77	0.000	0.000	-171 58
107	1070	571 70	1 144	73 646	8 582	733 997	-32.61	0.000	0.000	-162 29
108	1080	572.03	1 117	71 904	8 480	725 265	-34.36	0.000	0.000	-153 23
100	1090	572 42	1 091	70,260	8 382	716 922	-36.00	0.000	0.000	-144.50
110	1100	572.82	1.067	68 709	8 289	708 965	-37.55	0.000	0.000	-136 15
111	1110	573 22	1.044	67 247	8 200	701 385	-39.01	0.000	0.000	-128 16
112	1120	573 62	1.023	65 872	8 116	694 174	-40.39	0.000	0.000	-120 55
112	1130	574.02	1 003	64 578	8.036	687 323	-41.68	0.000	0.000	-113 30
114	1140	574.02	0.984	63 362	7 960	680,820	-42.90	0.000	0.000	-106.40
115	1150	574.81	0.966	62 220	7 888	674 657	-44 04	0.000	0.000	-99 85
116	1160	575 20	0.950	61 148	7 820	668 821	-45.11	0.000	0.000	-93 62
117	1170	575 58	0.034	60 143	7 755	663 303	-46.12	0.000	0.000	-87 72
110	1180	575 07	0.010	59 202	7 694	658 090	-47.06	0.000	0.000	-82 12
110	1100	576 35	0.915	58 320	7 637	653 173	-47 94	0.000	0.000	-76 83
120	1200	576 72	0.903	57 496	7 583	648 539	-48.76	0.000	0.000	-71 82
120	1210	577.00	0.881	56 725	7 532	644 177	-49 54	0.000	0.000	-67.08
120	1220	577 46	0.870	56 005	7 484	640 075	-50.26	0.000	0.000	-62 61
122	1220	577 82	0.859	55 333	7 430	636 223	-50 93	0.000	0.000	-58 30
123	1240	578 10	0.840	54 706	7 306	632 610	-51 55	0.000	0.000	-54 43
124	1240	578 55	0.840	54 122	7 357	629 223	-52 14	0.000	0.000	-50.67
120	1250	578.01	0.040	53 578	7 320	626.054	-52.68	0.000	0.000	47.15
120	1200	570.31	0.032	53 072	7 285	623 090	-53 19	0.000	0.000	43.83
120	12/0	570 61	0.024	52 601	7 253	620.323	-53.66	0.000	0.000	40.71
120	1200	570.00	0.810	52.001	7 200	617 741	-54 10	0,000	0.000	37 79
129	1290	579.90	0.010	52.104	7 104	615 335	-54.10	0.000	0.000	35.02
130	1300	500.31	0.004	51.709	7 469	613.006	-54.00	0.000	0.000	-35.03
131	1310	580.65	0.798	51.383	7.108	611.015	-04.00	0.000	0.000	-32.45
132	1320	580.99	0.792	51.035	7.144	600.022	-33.23	0.000	0.000	-30.03
133	1330	581.32	0.787	50.712	7.121	607 201	-00.00	0.000	0.000	-21.10
134	1340	581.60	0.783	50.415	7.100	007.291	-55.85	0.000	0.000	-20.00

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(1) Time Increm.	(2) Time min.	(3) Increm. Vol into Pond cf	(4) Starting Pond Depth ft.	(6)	(7)	(8) Increm. Vol out Pond cf				(9) Delta Vol
135	1350	581.99	0.779	50,139	7.081	605.631	-56.12	0.000	0.000	-23.64
136	1360	582.32	0.775	49,886	7.063	604.097	-56.37	0.000	0.000	-21.78
137	1370	582.64	0.771	49.652	7.046	602.680	-56.61	0.000	0.000	-20.04
138	1380	582.97	0.768	49.437	7.031	601.373	-56.82	0.000	0.000	-18.41
139	1390	583.29	0.765	49.239	7.017	600.170	-57.02	0.000	0.000	-16.88
140	1400	583.60	0.762	49.058	7.004	599.065	-57.20	0.000	0.000	-15.46
141	1410	583.92	0.759	48.892	6.992	598.050	-57.37	0.000	0.000	-14.13
142	1420	584.23	0.757	48.740	6.981	597.122	-57.52	0.000	0.000	-12.89
143	1430	584.54	0.755	48.602	6.972	596.274	-57.66	0.000	0.000	-11.73
144	1440	584.85	0.753	48.476	6.962	595.501	-57.78	0.000	0.000	-10.65

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(10) Remain Total Vol in.	(11) Remain Pond Depth ft	(12) CFS Discharge
0.0 0.0 1.2 6.4 28.2 57.8 96.7 141.2 189.0 238.7 306.3 394.3 485.0 573.3 658.0 738.6 837.3 959.0 1081.6 1199.0 1309.5 1413.1 1534.5	0.000 0.000 0.001 0.005 0.010 0.016 0.024 0.032 0.040 0.051 0.066 0.081 0.096 0.110 0.123 0.140 0.123 0.140 0.180 0.200 0.218 0.236 0.256	0.00 0.00 0.02 0.04 0.08 0.11 0.15 0.18 0.20 0.23 0.26 0.29 0.33 0.35 0.38 0.40 0.43 0.40 0.43 0.46 0.49 0.51 0.53 0.56

(10) Remain Total Vol in.	(11) Remain Pond Depth ft	(12) CFS Discharge	
2242.0 2414.5 2630.9 2860.1 3091.8 3322.7 3551.7 3819.7 4138.8 4470.8 4803.5 5133.0 5458.1 5915.6 6547.6 7228.6 8088.7 9169.4 10934.7 13410.2 15370.9 10544.4 44702.3 13553.3 12545.3 11595.9 10710.6 10146.4 9954.5 10008.9 9972.4 9997.1 9985.2 9996.1 9997.1 9998.9 9997.1 9998.9 9999.9 9992.0 9996.5 9822.9 9992.0 9996.5 9822.9 9923.4 9878.8 9979.7 9924.5 9846.3 9847.1	0.374 0.402 0.438 0.477 0.515 0.554 0.592 0.637 0.690 0.745 0.801 0.855 0.910 0.986 1.091 1.205 1.348 1.528 1.625 2.591 2.450 2.259 2.091 1.933 1.785 1.691 1.659 1.666 1.666 1.666 1.666 1.666 1.666 1.666 1.655 1.655 1.650 1.655 1.650 1.655 1.650 1.654 1.654 1.664 1.654 1.666 1.654 1.666 1.654 1.666 1.654 1.654 1.666 1.654 1.666 1.654 1.666 1.654 1.624 1.636 1.624 1.624 1.598	0.68 0.70 0.73 0.76 0.79 0.82 0.85 0.88 0.91 0.95 0.99 1.02 1.02 1.06 1.09 1.14 1.20 1.26 1.33 1.41 1.54 1.71 1.83 1.84 1.79 1.72 1.65 1.59 1.53 1.49 1.47 1.48 1.47 1.48 1.48 1.48 1.47 1.48 1.48 1.47 1.48 1.47 1.48 1.47 1.48 1.47 1.48 1.47 1.47 1.48 1.47 1.47 1.48 1.47 1.47 1.48 1.47 1.47 1.48 1.47 1.47 1.48 1.47 1.47 1.48 1.47 1.47 1.48 1.47 1.47 1.48 1.47 1.47 1.48 1.46 1.47	

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(10) Remain Total Vol in.	(11) Remain Pond Depth ft	(12) CFS Discharge
9509.5 9439.6 9373.9 9312.2 9254.4 9200.4 9149.9 9070.0 8951.0 8823.7 8698.4 8578.1 8463.8 8355.6 8253.2 8156.5 8065.3 7979.3 7898.2 7774.4 7594.1 7402.3 7213.7 7033.0 6861.5 6699.2 6545.9 6401.4 6265.3 6137.1 6016.6 5903.3 5796.9 5697.0 5697.0 5697.0 5697.0 5697.0 5697.0 5697.0 5697.0 5697.0 5697.0 5697.0 5697.0 5603.4 5515.7 5284.9 5217.8 5155.2 5096.8 5155.2 5042.4 4991.7 4944.6 4900.8 4860.0 4822.3 4754.8 4724.8 4697.0 4671.4	1.585 1.573 1.562 1.552 1.552 1.512 1.525 1.512 1.492 1.471 1.450 1.471 1.450 1.430 1.411 1.393 1.376 1.394 1.300 1.316 1.296 1.234 1.202 1.172 1.144 1.003 0.984 0.906 0.934 0.919 0.906 0.893 0.881 0.870 0.840 0.841 0.824 0.817 0.804 0.798 0.792 0.783 0.779	$1.45 \\ 1.44 \\ 1.43 \\ 1.43 \\ 1.43 \\ 1.42 \\ 1.42 \\ 1.41 \\ 1.41 \\ 1.40 \\ 1.39 \\ 1.38 \\ 1.37 \\ 1.36 \\ 1.35 \\ 1.34 \\ 1.33 \\ 1.32 \\ 1.31 \\ 1.30 \\ 1.29 \\ 1.27 \\ 1.25 \\ 1.24 \\ 1.22 \\ 1.21 \\ 1.19 \\ 1.18 \\ 1.17 \\ 1.16 \\ 1.15 \\ 1.13 \\ 1.12 \\ 1.11 \\ 1.10 \\ 1.09 \\ 1.08 \\ 1.07 \\ 1.06 \\ 1.05 \\ 1.04 \\ 1.03 \\ 1.03 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.01 \\ 1.01 \\ 1.02 \\ 1.02 \\ 1.02 \\ $

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(10) Remain Total Vol in.	(11) Remain Pond Depth ft	(12) CFS Discharge
4647.7 4625.9 4605.9 4587.5 4570.6 4555.2 4541.0 4528.1 4516.4 4505.7	0.775 0.771 0.768 0.765 0.762 0.759 0.757 0.755 0.753 0.751	1.01 1.01 1.00 1.00 1.00 1.00 1.00 0.99 0.99
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Water Quality



2.3 Technical Specifications

The Stormceptor dimensions vary with the size of unit that is specified. Dimensions of the fiberglass and concrete Stormceptor units that are being manufactured are provided in Table 2.

	Table 2. Stormcepto	r Dimensions *
Model	Treatment Bowl Diameter	Pipe Invert to Bottom of Concrete Stormceptor **
450i	4'	68"
900	6'	74"
1200	6'	86"
1800	6'	122"
2400	8'	122"
3600	8'	158"
4800	10'	146"
6000	10'	170"
7200	12'	158"

* Depths are approximate

** Inlet invert to bottom of base slab

Storage capacities and maximum treatment flowrate for Stormceptor are provided in Table 3. These flow rates indicate the threshold when bypassing begins to occur. At flow rates greater than the maximum treatment flow rate, treatment is still provided in the unit at 80% to 90% of the maximum treatment flow rate (NWRI, 1993). The treatment rate decreases once the unit begins to bypass since the overflow regulates the head differential between the inlet and outlet from the lower chamber (Figure 2).

Table 3. Stormceptor Capacities *										
Model	Maximum Treatment* Flow Rate gpm (l/s)	Down Pipe Diameter/ Orifice	Sediment Capacity (ft ³)	Oil Capacity (USG)	Total Holding Capacity (USG)	RES. TIME (MI)				
450i	79 (5)	12**	45	85	470					
900	285 (18)	6	84	242	1143	30.5				
1200	285 (18)	6	115	242	1354	4.8				
1800	285 (18)	6	200	242	1988					
2400	476 (30)	8	217	778	2886	6.00				
3600	476 (30)	8	368	778	4014	112				
4800	793 (50)	10	497	922	5331	4.7				
6000	793 (50)	10	654	922	6508					
7200	1110 (70)	12	828	1096	8245	74				

approximate flow rate without by-passing

** standard 4" diameter riser outlet pipe

Technical Manual

Appendix A

STC 900 Precast Concrete Stormceptor® (900 US Gallon Capacity)



#5725760, #5753115, #5849181.



Hydro Conduit Division

800 N.E. Tenney Road, Suite 413 Vancouver, WA 98685 Telephone (503) 572-9894 Facsimile (503) 296-2023 pvantilburg@rinker.com

Hydro Conduit

April 28, 2004

Matt Johnson SJO Consulting Engineers 1500 S.E. 12th Portland, OR 97201 mjohnson@sjoeng.com

Re: Stormceptor Removal Rates

Dear Matt:

Stormceptor has conducted several field studies to evaluate the removal rates of various pollutants. When our units have been sized based on 80% annual TSS removal, field monitoring has shown that we have been able to achieve removal rates in the ranges indicated below.

90-99%	Total Petroleum Hydrocarbons (TPH)
10-30%	Total Phosphorus (TP)
40-60%	Total Kjeldahl Nitrogen (TKN)
40-50%	Lead (Pb)
35-40%	Zinc (Zn)
15-25%	Biochemical Oxygen Demand (BOD)

This letter should not be taken as a guarantee of performance, but as an indication to what level our units have been proven to be able to perform. If you have any questions, please call me at 1-800-909-7763. Thank you.

Sincerely,

Peter Van Tilburg (via email)

Hydro Conduit, Area Manager



ATTACHMENT A

Comparison Table Of Field Studies and Lab Studies

3J Note: Not Included & Not Relevant to this Project

OPERATIONS & MAINTENANCE (O&M) PLAN

(Will be included with Final Storm Drainage Report)



ATTACHMENT B Light Fixture Specifications

gotham° I N C I T O™

Multiple Layers of Light





Luminaire Type:



High Center Beam Wall Mount Cylinder

•

Feature Set

OVERVIEW

- Thirteen optimized distribution patterns allow designers to achieve tailored objectives
- Bounding Ray[™] optical design
- 50° Cutoff to source and source image
- Field interchangeable optic
- Driver and LED light engine fully serviceable from below ceiling
- 70% lumen maintenance at 60,000 hours
 - 2.5 SDCM; 85 CRI typical, 90+ CRI optional
- Fixtures are wet location, covered ceiling (WL option)
- ENERGY STAR[®] Certified product
- 20 standard colors in textured and gloss finish; custom or RAL colors also available



Distribution



Coordinated Apertures | Multiple Layers of Light



ICO2WC page 1 of 7 GOTHAM ARCHITECTURAL DOWNLIGHTING | 1400 Lester Road Conyers, GA 30012 | P 800-705-SERV (7378) | gothamlighting.com © 2014-2020 Acuity Brands Lighting Inc. All Rights Reserved. Rev. 03/09/20 Specifications subject to change without notice. The product images shown are for illustration purposes only and may not be an exact representation of the product.



ORDERING INFORMATION

A+ Capable options indicated \mathbf{A} by this color background.



Design2Ship Quick Ship Program: Options in green text qualify for Design2Ship — 5 business days from order entry to ship. Refer to Design2Ship Brochure for complete program details. Maximum Order Quantity: 50 units.

Luminaire Type:

Catalog Number:

EXAMPLE: ICO2WC 35/10 AR LSS 20D MVOLT UGZ RGH DWHG

Series Color Temperature		Lumens	Reflector Color	Reflector Finish	Beam			
ICO2WC Incito 2in Round Wall Mount Cylinder Open Downlight	27/ 2700 K 30/ 3000 K 35/ 3500 K 40/ 4000 K 50/ ¹ 5000 K	02 250 lumens 05 500 lumens 07 750 lumens 10 1000 lumens 15 1500 lumens 20 2000 lumens	ARClearPRPewterWTRWheatGRGoldWR2White paintedBR2BlackBZR2Dark Bronze painted	LSS Semi-specular LD Matte diffuse	 15D 15° beam angle 20D 20° beam angle 25D 25° beam angle 30D 30° beam angle 35D 35° beam angle 40D 40° beam angle 45D 45° beam angle 50D 50° beam angle 55D 55° beam angle 3515D Elliptical 35° x 15° beam angle 5020D Elliptical 50° x 20° beam angle 5060D Elliptical 60° x 70° beam angle 			

Z

Voltage Driver		Mountii	Mounting		face ⁵		
MVOLT 120 277	120V - 277V 120V 277V	UGZ ³	Universal dimming to 1% (0-10V, 120V TRIAC or ELV)	RGH⁴ SGB	Recessed Gear Housing Surface Gear Box	(blank) NLT NLTER ⁶ NLTAIR2 NLTAIRER2 ⁶ NLTAIREM2	nLight [®] dimming pack. nLight [®] dimming pack for fixtures on emergency circuit nLight [®] AIR dimming pack. nLight [®] AIR dimming pack for fixtures on emergency circuit nLight [®] AIR dimming pack for fixtures on emergency circuit

Options	Architectural Colors - Powder Paint ⁹	
90CRI ¹ High CRI (90+)	DDB Gloss Dark Bronze I	DDBT Textured Dark Bronze
N80 ⁷ nLight Lumen Compensation	DBL Gloss Black I	DBLB Matte Black
WL ⁸ Wet Location	DWH Gloss White I	DWHG Textured White
	DMB Gloss Medium Bronze I	DBNH Textured Bronze
	DNA Gloss Natural Aluminum I	DNAT Textured Natural Aluminum
	DSS Gloss Sandstone I	DSST Textured Sandstone
	DGC Gloss Charcoal Grey I	DSPD Textured Dark Grey
	DTG Gloss Tennis Green I	DSPE Textured Green
	DBR Gloss Bright Red I	DSPH Textured Light Red
	DSB Gloss Steel Blue	DWHAMF Gloss White with Anti-microbial finish
	1	

ACCESSORIES — order as separate catalog numbers (shipped separately)							
ICO2OPTC XXD	Additional optics for field installation. Replace "XX" with beam angle.						
ICO2OPTC KIT	Kit including a field interchangeable optic for each of the 13 preset beam distribution patterns						
HS234FL	Hole saw for RGH option						
SDT 347/120 75VA	347V/120V, 75VA step down transformer. Must be remote mounted.						

ORDERING NOTES

- 1. 5000K CCT not available with 90CRI.
- 2. Not available with Reflector Finish.
- 3. Refer to Tech 240 for compatible dimmers.
- 4. RGH with 2000LM option requires 120 or 277 (non-IC).
- 5. Field installed. Access required to location of remote mounted device.
- 6. ER for use with generator supply power. Will require an emergency hot feed and normal hot feed.
- 7. Requires NLT or NLTER.
- 8. Must be mounted in down orientation in wet location applications.
- For details on RAL and Custom colors please see Architectural colors. 9.

GOTHAM ARCHITECTURAL DOWNLIGHTING | 1400 Lester Road Conyers, GA 30012 | P 800-705-SERV (7378) | gothamlighting.com © 2014-2020 Acuity Brands Lighting Inc. All Rights Reserved. Rev. 03/09/20 Specifications subject to change without notice. The product images shown are for illustration purposes only and may not be an exact representation of the product.



ATTACHMENT C Reader Board Sign Specifications

GALAXY® GS6 15.85 MM PRODUCT SPECIFICATIONS

The GS6 is the best full-feature, high-quality Galaxy series yet. This product provides users a display that runs outstanding graphics and animations using the best contrast in the industry. The 15.85 mm pixel pitch is the tighest resolution 16 mm LED display in the industry.

15.85 MM TECHNICAL SPECIFICATIONS

Character Height: 4.4" (7 pixel font) Line Spacing: 15.85 mm (0.62") Pixel Configuration: Monochrome: 1 red or 1 amber RGB:1 red, 1 green, 1 blue

Maximum Brightness: Monochrome red: 4,500 nits Monochrome amber: 6,000 nits RGB: 12,000 nits

Monochrome Color Capability: 4,096 shades of red or amber Full Color Capability: RGB: 281 trillion colors Optimal Viewing Angle: 140 degrees horizontal x 70 degrees vertical Readability Angle: 160 degrees horizontal x 90 degrees vertical Min Viewing Distance: 37'

PRODUCT FEATURES

- All sealed components
- Quick connects
- Mounting clips
- High-contrast louvers
- Redundant module signal
- Large sections for fast installation
- Front ventilation on displays less than seven feet tall
- No spreader beam required for displays greater than seven feet tall
- Same module size and cabinet size for all pixel pitches
- Single-step module removal
- Shallow cabinet depth
- Narrow cabinet borders

MODEL NUMBER GUIDE

GS6	-	100	х	250	-	15.85	- RGB -	SF
Series		High		Wide		pacing	Color or RGB	View
		Line		Columns		Line S	LED Red, Amber, (ingle Face or Two

201 Daktronics Drive PO Box 5128 Brookings, SD 57006-5128 tel 888-325-7446 605-692-0200 ext. 57220 fax 605-692-0381 www.daktronics.com email commercial@daktronics.com Copyright © 2017 Daktronics DD3148704 Rev02 090915 Page 1 of 8



GS6 SERIES SPECIFICATIONS

Estimated LED Lifetime: 100,000+ hours **Contrast Enhancement:** Non-reflective black louvers and module face grooves disperse light **Message Capability:** Text, graphics, logos, basic animation, video clips, multiple font styles, and sizes **Control Software:** Venus[®] Control Suite Power: 120, 120/240 VAC Single Phase **Display Dimming:** 64 levels (Automatic, scheduled or manual control) **Communication Options:** Ethernet Fiber Optic, Ethernet Bridge Radio, Remote Cellular, Ethernet CAT5 **Operating Temperature:** -40°F to 120°F with 99% RH non-condensing **Compliance Information:**

UL and cUL Listed, UL-Energy Verified, FCC compliance

DISPLAY CONFIGURATIONS



Available in all sizes





GALAXY® GS6 15.85 MM PRODUCT SPECIFICATIONS

Lines x Columns	Sections/ Ventilated	Cabinet Dimensions Feet-Inches H x W x D	Cabinet Dimensions Meters H x W x D	Cabinet Square Feet (Sauare Meters)	Active Area Square Feet (Sauare Meters)	Cabinet Weight Pounds (kiloarams)	Lines/ Characters per line	Character Height	Max Amber	Maximum Watts Amber Red R(
20x100	Sina/Ft	1'7'' x 5'6'' x 5''	0.47 x 1.67 x 0.13	8.4 (0.8)	5.5 (0.6)	65 (30)	2/20	4''-12''	230	230	305
20x125	Sing/Ft	1'7'' x 6'9'' x 5''	0.47 x 2.06 x 0.13	10.4 (1.0)	6.8 (0.8)	75 (35)	2/25	4''-12''	275	275	370
20x150	Sing/Ft	1'7'' x 8'1'' x 5''	0.47 x 2.46 x 0.13	12.4 (1.2)	8.2 (1.0)	90 (41)	2/30	4''-12''	320	320	345
20x175	Sing/Ft	1'7'' x 9'5'' x 5''	0.47 x 2.85 x 0.13	14.4 (1.3)	9.5 (1.1)	105 (48)	2/35	4''-12''	365	365	500
20x200	Sing/Ft	1'7'' x 10'8'' x 5''	0.47 x 3.25 x 0.13	16.4 (1.5)	10.9 (1.3)	120 (55)	2/40	4''-12''	405	405	565
20x225	Sing/Ft	1'7'' x 12'0'' x 5''	0.47 x 3.65 x 0.13	18.4 (1.7)	12.2 (1.4)	135 (62)	2/45	4''-12''	450	450	630
20x250	Sing/Ft	1'7'' x 13'3'' x 5''	0.47 x 4.04 x 0.13	20.4 (1.9)	13.6 (1.6)	150 (69)	2/50	4''-12''	495	495	695
20x275	Sing/Ft	1'7'' x 14'7'' x 5''	0.47 x 4.44 x 0.13	22.4 (2.1)	14.9 (1.8)	165 (75)	2/55	4''-12''	540	540	755
20x300	Sing/Ft	1'7" x 15'11" x 5"	0.47 x 4.84 x 0.13	24.4 (2.3)	16.3 (1.9)	180 (82)	2/60	4''-12''	585	585	820
20x325	Sing/Ft	1'7'' x 17'2'' x 5''	0.47 x 5.23 x 0.13	26.4 (2.5)	17.6 (2.1)	195 (89)	2/65	4''-12''	630	630	885
20x350	Sing/Ft	1'7'' x 18'6'' x 5''	0.47 x 5.63 x 0.13	28.4 (2.6)	19.0 (2.2)	205 (93)	2/70	4"-12"	675	675	950
20x3/5	Sing/Ft	1'/" x 19'9" x 5"	0.4/ x 6.02 x 0.13	30.4 (2.8)	20.3 (2.4)	220 (100)	2/75	4"-12"	/20	/20	1015
20x400	Sing/Ft	1'7'' x 21'1'' x 3''	0.4/ x 0.42 x 0.13	32.4 (3.0)	21.7 (2.0)	235 (107)	2/80	4"-12"	/05	/05	1080
20x425	Sing/Ft	17" X ZZ'S" X S"	0.47 x 0.82 x 0.13	<u>34.4 (3.2)</u>	23.0 (2.7)	250 (114)	2/83	4"-12"	810	810	1145
$\frac{20x430}{20x475}$	Sing/Ft	17 X Z3 6 X 3	$0.47 \times 7.21 \times 0.13$	38 4 (3.4)	24.4 (2.9)	203 (121)	2/90	4'-12'	000	000	1205
$\frac{20x473}{20x500}$	Sing/Ft	17 x 25 0 x 5	0.47 x 7.01 x 0.13	40 4 (3.8)	271 (3.0)	200 (120)	2/100	4 -12	900	900	1270
$\frac{20\times 300}{40\times 75}$	Sing/Ft	2'7'' x 4'2'' x 5''	0.47 x 0.01 x 0.13	10.7 (1.0)	8.2 (0.8)	80 (37)	5/15	4 -12	255	255	360
40x100	Sing/Ft	2'7'' x 5'6'' x 5''	0.79 x 1.67 x 0.13	14.1 (1.3)	10.9 (1.1)	10.5 (48)	5/20	4"-24"	30.5	305	46.5
40x125	Sing/Ft	2'7'' x 6'9'' x 5''	0.79 x 2.06 x 0.13	17.4 (1.6)	13.6 (1.4)	130 (59)	5/25	4''-24''	370	370	570
40x150	Sing/Ft	2'7'' x 8'1'' x 5''	0.79 x 2.46 x 0.13	20.8 (1.9)	16.3 (1.7)	150 (69)	5/30	4''-24''	435	435	670
40x175	Sing/Ft	2'7'' x 9'5'' x 5''	0.79 x 2.85 x 0.13	24.1 (2.3)	19.0 (2.0)	175 (80)	5/35	4''-24''	500	500	775
40x200	Sing/Ft	2'7'' x 10'8'' x 5''	0.79 x 3.25 x 0.13	27.5 (2.6)	21.7 (2.2)	200 (91)	5/40	4''-24''	565	565	880
40x225	Sing/Ft	2'7'' x 12'0'' x 5''	0.79 x 3.65 x 0.13	30.8 (2.9)	24.4 (2.5)	225 (103)	5/45	4''-24''	630	630	980
40x250	Sing/Ft	2'7'' x 13'3'' x 5''	0.79 x 4.04 x 0.13	34.2 (3.2)	27.1 (2.8)	250 (114)	5/50	4''-24''	695	695	1085
40x275	Sing/Ft	2'7'' x 14'7'' x 5''	0.79 x 4.44 x 0.13	37.5 (3.5)	29.8 (3.1)	275 (125)	5/55	4''-24''	755	755	1190
40x300	Sing/Ft	2'7'' x 15'11'' x 5''	0.79 x 4.84 x 0.13	40.9 (3.8)	32.5 (3.4)	295 (134)	5/60	4''-24''	520	520	1295
40x325	Sing/Ft	2'7'' x 17'2'' x 5''	0.79 x 5.23 x 0.13	44.2 (4.1)	35.2 (3.6)	320 (146)	5/65	4''-24''	885	885	1395
40x350	Sing/Ft	2'7'' x 18'6'' x 5''	0.79 x 5.63 x 0.13	47.6 (4.4)	37.9 (3.9)	345 (157)	5/70	4''-24''	950	950	1500
40x375	Sing/Ft	2'7'' x 19'9'' x 5''	0.79 x 6.02 x 0.13	51.0 (4.8)	40.6 (4.2)	370 (168)	5/75	4''-24''	1015	1015	1605
40x400	Sing/Ft	2'7'' x 21'1'' x 5''	0.79 x 6.42 x 0.13	54.3 (5.1)	43.3 (4.5)	395 (180)	5/80	4''-24''	1080	1080	1705
40x425	Sing/Ft	2'/'' x 22'5'' x 5''	0.79 x 6.82 x 0.13	5/./ (5.4)	46.0 (4.8)	420 (191)	5/85	4"-24"	1145	1145	1810
$\frac{40x450}{40}$	Sing/Ft	2'7'' x 23'8'' x 5''	0.79 x 7.21 x 0.13	01.0 (5.7)	48.7 (5.0)	440 (200)	5/90	4"-24"	1205	1205	1915
$\frac{40x475}{40x500}$	Sing/Ft		0.79 x 7.01 x 0.13	677 (6.2)	541 (5.3)	403 (211)	5/95	4"-24"	1225	1225	2020
40x300 60x75	Sing/Ft	$27 \times 203 \times 3$	$1.11 \times 1.27 \times 0.13$	150(14)	12.2 (1.2)	110 (50)	7/15	4 -24	300	300	/80
60x75 60x100	Sing/Ft	3'8'' x 5'6'' x 5''	1.11 x 1.27 x 0.13	10.7 (1.4)	16.3 (1.6)	145 (66)	7/20	4 - 37	385	385	620
60x125	Sing/Ft	3'8'' x 6'9'' x 5''	1 11 x 2 06 x 0 13	24.4 (2.3)	20.3 (2.0)	180 (82)	7/25	4"-37"	470	470	765
60x150	Sing/Ft	3'8" x 8'1" x 5"	1.11 x 2.46 x 0.13	29.1 (2.7)	24.4 (2.4)	210 (96)	7/30	4''-37''	555	555	905
60x175	Sing/Ft	3'8'' x 9'5'' x 5''	1.11 x 2.85 x 0.13	33.8 (3.2)	28.4 (2.8)	245 (112)	7/35	4''-37''	640	640	1050
60x200	Sing/Ft	3'8'' x 10'8'' x 5''	1.11 x 3.25 x 0.13	38.6 (3.6)	32.5 (3.2)	280 (128)	7/40	4''-37''	720	720	1195
60x225	Sing/Ft	3'8'' x 12'0'' x 5''	1.11 x 3.65 x 0.13	43.3 (4.1)	36.6 (3.6)	315 (143)	7/45	4''-37''	805	805	1335
60x250	Sing/Ft	3'8'' x 13'3'' x 5''	1.11 x 4.04 x 0.13	48.0 (4.5)	40.6 (4.0)	350 (159)	7/50	4''-37''	890	890	1480
60x275	Sing/Ft	3'8'' x 14'7'' x 5''	1.11 x 4.44 x 0.13	52.7 (4.9)	44.7 (4.4)	380 (173)	7/55	4''-37''	975	975	1620
60x300	Sing/Ft	3'8'' x 15'11'' x 5''	1.11 x 4.84 x 0.13	57.4 (5.4)	48.7 (4.8)	415 (189)	7/60	4''-37''	1055	1055	1765
60x325	Sing/Ft	3'8'' x 17'2'' x 5''	1.11 x 5.23 x 0.13	62.1 (5.8)	52.8 (5.2)	450 (205)	7/65	4''-37''	1140	1140	1905
60x350	Sing/Ft	3'8'' x 18'6'' x 5''	1.11 x 5.63 x 0.13	66.8 (6.2)	56.8 (5.6)	485 (220)	7/70	4"-37"	1225	1225	2050
60x375	Sing/Ft	3'8'' x 19'9'' x 5''	1.11 x 6.02 x 0.13	71.5 (6.7)	60.9 (6.0)	515 (234)	7/75	4"-37"	1310	1310	2195
60x400	Sing/Ft	3'8'' x 21'1'' x 5''	1.11 x 6.42 x 0.13	/6.2 (/.1)	64.9 (6.4)	550 (250)	7/80	4"-3/"	1395	1395	2335
60x425	Sing/Ft	3'8'' x 22'5'' x 5''	1.11 x 0.82 x 0.13	80.9 (7.6)	09.0 (0.8)	282 (200)	7/85	4"-3/"	14/5	14/5	2480
$\frac{00x430}{60x475}$	Sing/Ff	3.8. X Z3.8. X 3. 21011 x 251011 x 511	1.11 x 7.21 x 0.13		73.1 (7.2)	020 (282)	7/90	4"-3/"	1500	1500	2020
60x473	Sing/Ft		1.11 x 7.01 x 0.13	90.3 (8.4)	91.2 (8.0)	685 (211)	7/100	4 - 37	1730	1730	2703
80x75	Sing/Ft	1'8'' x 1'2'' x 5''	1 /3 x 1 27 x 0 13	193 (1.8)	16.3 (1.6)	140 (64)	10/15	4 -37 /''_/Q''	360	360	595
80x100	Sing/Ft	<u>4'8'' x 5'6'' x 5''</u>	$1.43 \times 1.27 \times 0.13$	25 4 (2 4)	21 7 (2 1)	185 (84)	10/20	<u>4''_49''</u>	465	465	780
80x125	Sing/Ft	4'8'' x 6'9'' x 5''	1.43 x 2.06 x 0.13	31.5 (2.9)	27.1 (2.6)	230 (105)	10/25	4''-49''	570	570	960
80x150	Sing/Ft	4'8'' x 8'1'' x 5''	1.43 x 2.46 x 0.13	37.5 (3.5)	32.5 (3.1)	275 (125)	10/30	4''-49''	670	670	1145
80x175	Sing/Ft	4'8'' x 9'5'' x 5''	1.43 x 2.85 x 0.13	43.6 (4.1)	37.9 (3.6)	315 (143)	10/35	4''-49''	775	775	1325
80x200	Sing/Ft	4'8'' x 10'8'' x 5''	1.43 x 3.25 x 0.13	49.6 (4.6)	43.3 (4.2)	360 (164)	10/40	4''-49''	880	880	1505
80x225	Sing/Ft	4'8'' x 12'0'' x 5''	1.43 x 3.65 x 0.13	55.7 (5.2)	48.7 (4.7)	405 (184)	10/45	4''-49''	980	980	1690
80x250	Sing/Ft	4'8'' x 13'3'' x 5''	1.43 x 4.04 x 0.13	61.7 (5.8)	54.1 (5.2)	445 (202)	10/50	4''-49''	1085	1085	1870
80x275	Sing/Ft	4'8'' x 14'7'' x 5''	1.43 x 4.44 x 0.13	67.8 (6.3)	59.5 (5.7)	490 (223)	10/55	4''-49''	1190	1190	2055
80x300	Sing/Ft	4'8'' x 15'11'' x 5''	1.43 x 4.84 x 0.13	73.9 (6.9)	64.9 (6.2)	535 (243)	10/60	4''-49''	1295	1295	2235
80x325	Sing/Ft	4'8'' x 17'2'' x 5''	1.43 x 5.23 x 0.13	79.9 (7.5)	70.4 (6.8)	580 (264)	10/65	4''-49''	1395	1395	2420
80x350	Sing/Ft	4'8'' x 18'6'' x 5''	1.43 x 5.63 x 0.13	86.0 (8.1)	75.8 (7.3)	620 (282)	10/70	4''-49''	1500	1500	2600
80x375	Sing/Ft	4'8'' x 19'9'' x 5''	1.43 x 6.02 x 0.13	92.0 (8.6)	81.2 (7.8)	665 (302)	10/75	4''-49''	1605	1605	2780
80x400	Sina/Ft	4'8'' x 21'1'' x 5''	1.43 x 6.42 x 0.13	98.1 (9.2)	86.6 (8.3)	710 (323)	10/80	4''-49''	1705	1705	2965
Lines x Columns	Sections/ Ventilated	Cabinet Dimensions Feet-Inches H x W x D	Cabinet Dimensions Meters H x W x D	Cabinet Square Feet (Square Meters)	Active Area Square Feet (Square Meters)	Cabinet Weight Pounds (kilograms)	Lines/ Characters per line	Character Height	Maximum Watts Amber Red RGB		
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80x425	Sing/Ft	4'8'' x 22'5'' x 5''	$143 \times 682 \times 013$	104 2 (9.8)	92.0 (8.8)	750 (341)	10/85	4''_49''	1810 1810 3145		
80x450	Sina/Ft	4'8'' x 23'8'' x 5''	1.43 x 7.21 x 0.13	110.2 (10.3)	97.4 (9.4)	795 (361)	10/90	4''-49''	1915 1915 3330		
80x475	Sing/Ft	4'8'' x 25'0'' x 5''	1.43 x 7.61 x 0.13	116.3 (10.9)	102.8 (9.9)	840 (382)	10/95	4''-49''	2020 2020 3510		
80x500	Sing/Ft	4'8'' x 26'3'' x 5''	1.43 x 8.01 x 0.13	122.3 (11.5)	108.2 (10.4)	885 (402)	10/100	4''-49''	2120 2120 3695		
100x75	Sing/Ft	5'9'' x 4'2'' x 5''	1.74 x 1.27 x 0.13	23.7 (2.2)	20.3 (1.9)	175 (80)	12/15	4''-62''	420 420 790		
100x100	Sing/Ft	5'9'' x 5'6'' x 5''	1.74 x 1.67 x 0.13	31.1 (2.9)	27.1 (2.6)	225 (103)	12/20	4''-62''	545 545 1035		
100x125	Sing/Ft	5'9'' x 6'9'' x 5''	1.74 x 2.06 x 0.13	38.5 (3.6)	33.8 (3.2)	280 (128)	12/25	4''-62''	665 665 1280		
100x150	Sing/Ft	5'9'' x 8'1'' x 5''	1.74 x 2.46 x 0.13	45.9 (4.3)	40.6 (3.8)	335 (152)	12/30	4"-62"	790 790 1530		
$\frac{100 \times 1/5}{100,000}$	Sing/Ft	5'9'' x 9'5'' x 5''	1./4 x 2.85 x 0.13	53.3 (5.0)	4/.4 (4.5)	385 (1/5)	12/35	4"-62"	915 915 1775		
100x200	Sing/Ft	5'9'' x 10'8'' x 5''	1.74 x 3.25 x 0.13	60.7 (5.7)	<u> </u>	440 (200)	12/40	4"-02"	1035 1035 2020		
$\frac{100x223}{100x250}$	Sing/Ft	5'0'' v 13'3'' v 5''	$1.74 \times 3.03 \times 0.13$	75.5 (70)	676 (5.8)	545 (223)	12/45	4 -02	1280 1280 2515		
$\frac{100 \times 230}{100 \times 275}$	Sing/Ft	5'9'' x 14'7'' x 5''	$1.74 \times 4.04 \times 0.13$	82.9 (7.7)	74.4 (7.0)	600 (273)	12/55	4"-62"	1405 1405 2760		
100x300	Sing/Ft	5'9'' x 15'11'' x 5''	1.74 x 4.84 x 0.13	90.3 (8.4)	81.2 (7.7)	655 (298)	12/60	4"-62"	1530 1530 3005		
100x325	Sing/Ft	5'9'' x 17'2'' x 5''	1.74 x 5.23 x 0.13	97.8 (9.1)	87.9 (8.3)	705 (320)	12/65	4''-62''	1650 1650 3255		
100x350	Sing/Ft	5'9'' x 18'6'' x 5''	1.74 x 5.63 x 0.13	105.2 (9.8)	94.7 (9.0)	760 (345)	12/70	4''-62''	1775 1775 3500		
100x375	Sing/Ft	5'9'' x 19'9'' x 5''	1.74 x 6.02 x 0.13	112.6 (10.5)	101.4 (9.6)	815 (370)	12/75	4''-62''	1900 1900 3745		
100x400	Sing/Ft	5'9'' x 21'1'' x 5''	1.74 x 6.42 x 0.13	120.0 (11.2)	108.2 (10.2)	865 (393)	12/80	4''-62''	2020 2020 3995		
100x425	Sing/Ft	5'9'' x 22'5'' x 5''	1.74 x 6.82 x 0.13	127.4 (11.9)	115.0 (10.9)	920 (418)	12/85	4''-62''	2145 2145 4240		
100x450	Sing/Ft	5'9'' x 23'8'' x 5''	1.74 x 7.21 x 0.13	134.8 (12.5)	121.7 (11.5)	975 (443)	12/90	4''-62''	2270 2270 4485		
100x475	Sing/Ft	5'9'' x 25'0'' x 5''	1.74 x 7.61 x 0.13	142.2 (13.2)	128.5 (12.2)	1025 (465)	12/95	4"-62"	2390 2390 4730		
100x500	Sing/Ft	5'9'' x 26'3'' x 5''	1./4 x 8.01 x 0.13	149.6 (13.9)	135.2 (12.8)	1080 (490)	12/100	4"-62"	2515 2515 4980		
120x/3	Sing/Ft	0.9" x 4"Z" x 5"	2.00 x 1.27 x 0.13	28.0 (2.0)	24.4 (2.4)	205 (93)	15/15	4"-/4"	480 480 905		
120x100	Sing/Ft	<u> </u>	2.00 x 1.07 x 0.13	45.5 (4.2)	<u> </u>	330 (121)	15/20	4 -/4	765 765 1480		
$\frac{120 \times 120}{120 \times 150}$	Sing/Ft	6'9'' x 8'1'' x 5''	2.00 x 2.00 x 0.13	54.3 (5.1)	48.7 (4.8)	395 (180)	15/30	<u>4'-74</u> <u>4''_74''</u>	905 905 1765		
120x175	Sing/Ft	6'9'' x 9'5'' x 5''	2.06 x 2.85 x 0.13	63.0 (5.9)	56.8 (5.6)	455 (207)	15/35	4''-74''	1050 1050 2050		
120x200	Sing/Ft	6'9'' x 10'8'' x 5''	2.06 x 3.25 x 0.13	71.8 (6.7)	64.9 (6.4)	520 (236)	15/40	4''-74''	1195 1195 2335		
120x225	Sing/Ft	6'9'' x 12'0'' x 5''	2.06 x 3.65 x 0.13	80.5 (7.5)	73.1 (7.2)	580 (264)	15/45	4''-74''	1335 1335 2620		
120x250	Sing/Ft	6'9'' x 13'3'' x 5''	2.06 x 4.04 x 0.13	89.3 (8.3)	81.2 (8.0)	645 (293)	15/50	4''-74''	1480 1480 2905		
120x275	Sing/Ft	6'9'' x 14'7'' x 5''	2.06 x 4.44 x 0.13	98.1 (9.1)	89.3 (8.8)	710 (323)	15/55	4''-74''	1620 1620 3195		
120x300	Sing/Ft	6'9'' x 15'11'' x 5''	2.06 x 4.84 x 0.13	106.8 (10.0)	97.4 (9.6)	770 (350)	15/60	4''–74''	1765 1765 3480		
120x325	Sing/Ft	6'9'' x 17'2'' x 5''	2.06 x 5.23 x 0.13	115.6 (10.8)	105.5 (10.4)	835 (379)	15/65	4''-74''	1905 1905 3765		
120x350	Sing/Ft	<u>6'9'' x 18'6'' x 5''</u>	2.06 x 5.63 x 0.13	124.4 (11.6)	113.6 (11.2)	900 (409)	15/70	4"-74"	2050 2050 4050		
120x3/5	Sing/Ft	6'9'' x 19'9'' x 5''	2.06 x 6.02 x 0.13	133.1 (12.4)	121.7 (12.0)	960 (436)	15/75	4"-/4"	2195 2195 4335		
120x400	Sing/Ft	<u> </u>	2.00 x 0.42 x 0.13	141.9 (13.2)	129.0 (12.0)	1025 (403)	15/85	4 -/4	2333 2333 4020		
120x425 120x450	Sing/Ft	6'9'' x 23'8'' x 5''	2.00 x 0.02 x 0.13	1.59 4 (14.9)	146 1 (14 4)	11.50 (522)	15/90	4''-74''	2620 2620 5195		
120x475	Sina/Ft	6'9'' x 25'0'' x 5''	2.06 x 7.61 x 0.13	168.2 (15.7)	154.2 (15.2)	1215 (552)	15/95	4''-74''	2765 2765 5480		
120x500	Sing/Ft	6'9'' x 26'3'' x 5''	2.06 x 8.01 x 0.13	176.9 (16.5)	162.3 (16.0)	1275 (579)	15/100	4''-74''	2905 2905 5765		
140x100	Sing/Bk	7'10'' x 5'9'' x 11''	2.38 x 1.74 x 0.28	44.3 (4.1)	37.9 (3.7)	495 (225)	17/20	4''-87''	755 755 1355		
140x125	Sing/Bk	7'10'' x 7'0'' x 11''	2.38 x 2.14 x 0.28	54.5 (5.1)	47.4 (4.6)	605 (275)	17/25	4''-87''	950 950 1700		
140x150	Sing/Bk	7'10'' x 8'4'' x 11''	2.38 x 2.53 x 0.28	64.6 (6.0)	56.8 (5.5)	720 (327)	17/30	4''-87''	1150 1150 2050		
140x175	Sing/Bk	7'10'' x 9'8'' x 11''	2.38 x 2.93 x 0.28	74.7 (7.0)	66.3 (6.4)	830 (377)	17/35	4"-87"	1300 1300 2350		
140x200	Sing/Bk	7'10'' x 10'11'' x 11''	2.38 x 3.33 x 0.28	84.8 (7.9)	/5.8 (/.4)	945 (429)	17/40	4"-8/"	1500 1500 2700		
140x225	Sing/BK	7'10" x 12'3" x 11"	2.38 X 3.72 X 0.28	94.9 (8.9)	85.2 (8.3)	1055 (479)	17/40	4"-8/"	1045 1045 2245		
$\frac{140x230}{140x275}$	Sing/Bk	7'10' x 13'0' x 11'	$2.38 \times 4.12 \times 0.28$	115.1 (10.8)	10/ 2 (10.1)	1280 (581)	17/55	4 -07	2045 2045 3695		
140x300	Sing/Bk	7'10'' x 16'2'' x 11''	2.38 x 4 91 x 0.28	125.3 (11.7)	113.6 (11.0)	1395 (633)	17/60	4''-87''	2240 2240 4040		
140x325	Sing/Bk	7'10'' x 17'5'' x 11''	2.38 x 5.31 x 0.28	135.4 (12.6)	123.1 (12.0)	1505 (683)	17/65	4''-87''	2390 2390 4340		
140x350	Sing/Bk	7'10'' x 18'9'' x 11''	2.38 x 5.7 x 0.28	145.5 (13.6)	132.5 (12.9)	1615 (733)	17/70	4''-87''	2590 2590 4690		
140x375	Sing/Bk	7'10'' x 20'0'' x 11''	2.38 x 6.1 x 0.28	155.6 (14.5)	142.0 (13.8)	1730 (785)	17/75	4''-87''	2790 2790 5040		
140x400	Sing/Bk	7'10'' x 21'4'' x 11''	2.38 x 6.5 x 0.28	165.7 (15.5)	151.5 (14.7)	1840 (835)	17/80	4''-87''	2940 2940 5340		
140x425	Sing/Bk	7'10'' x 22'8'' x 11''	2.38 x 6.89 x 0.28	175.8 (16.4)	160.9 (15.6)	1955 (887)	17/85	4''-87''	3135 3135 5685		
140x450	Sing/Bk	7'10" x 23'11" x 11"	2.38 x 7.29 x 0.28	185.9 (17.4)	170.4 (16.6)	2065 (937)	17/90	4''-87''	3335 3335 6035		
140x475	Sing/Bk	/'10" x 25'3" x 11"	2.38 x 7.69 x 0.28	196.1 (18.3)	179.9 (17.5)	2180 (989)	17/95	4"-87"	3485 3485 6335		
140x500	Sing/Bk	7'10'' x 26'6'' x 11''	2.38 x 8.08 x 0.28	206.2 (19.2)	189.3 (18.4)	2290 (1039)	1//100	4"-87"	3680 3680 6680		
140x525	Sing/Bk	7 10" x 27'10" x 11"	2.30 X 8.48 X 0.28	210.3 (20.2)	190.0 (19.3)	2405 (1091)	17/105	4"-8/"	3080 3880 /030		
140x330	Sing/BK	7 10 x 29'2" x 11" 7'10" x 30'5" x 11"	2.30 X 0.0/ X U.28	220.4 (21.1)	200.3 (20.2)	2630 (1141)	17/110	4 - 8/ "	4030 4030 7330		
140x5/5	Sing/Bk	7'10'' x 31'9'' x 11''	2.30 × 7.27 × 0.20 2.38 × 9.67 × 0.28	246.6 (23.0)	217.7 (21.2)	2740 (1243)	17/120	4''-87''	4435 4435 8035		
140x625	Sing/Bk	7'10'' x 33'0'' x 11''	2.38 x 10.06 x 0.28	256.7 (23.9)	236.6 (23.0)	2850 (1293)	17/125	4''-87''	4585 4585 8335		
140x650	Sing/Bk	7'10'' x 34'4'' x 11''	2.38 x 10.46 x 0.28	266.9 (24.9)	246.1 (23.9)	2965 (1345)	17/130	4''-87''	4785 4785 8685		
140x675	Sing/Bk	7'10" x 35'8" x 11"	2.38 x 10.86 x 0.28	277.0 (25.8)	255.6 (24.6)	3075 (1395)	17/135	4''-87''	4980 4980 9030		
140x700	Sing/Bk	7'10'' x 36'11'' x 11''	2.38 x 11.25 x 0.28	287.1 (26.8)	265.0 (25.5)	3190 (1447)	17/140	4''-87''	5130 5130 9330		
140x725	Sing/Bk	7'10'' x 38'3'' x 11''	2.38 x 11.65 x 0.28	297.2 (27.7)	274.5 (26.5)	3300 (1497)	17/145	4''-87''	5330 5330 9680		
140x750	Sing/Bk	7'10" x 39'6" x 11"	2.38 x 12.04 x 0.28	307.3 (28.7)	284.0 (27.4)	3415 (1550)	17/150	4''-87''	5525 5525 10025		

Lines x Columns	Sections/ Ventilated	Cabinet Dimensions Feet-Inches H x W x D	Cabinet Dimensions Meters H x W x D	Cabinet Square Feet (Sauare Meters)	Active Area Square Feet (Sauare Meters)	Cabinet Weight Pounds (kiloarams)	Lines/ Characters per line	Character Height	Max Amber	kimum V Red	Vatts RGB
140x775	Sina/Bk	7'10'' x 40'10'' x 11''	2.38 x 12.44 x 0.28	317.4 (29.6)	293.4 (28.3)	3525 (1599)	17/155	4''-87''	5675	5675	10325
140x800	Sing/Bk	7'10'' x 42'2'' x 11''	2.38 x 12.84 x 0.28	327.5 (30.6)	302.9 (29.2)	3640 (1652)	17/160	4''-87''	5875	5875	10675
140x825	Sing/Bk	7'10" x 43'5" x 11"	2.38 x 13.23 x 0.28	337.7 (31.5)	312.4 (30.1)	3750 (1701)	17/165	4''-87''	6075	6075	11025
160x100	Sing/Bk	8'10" x 5'9" x 11"	2.69 x 1.74 x 0.28	50.3 (4.7)	43.3 (4.2)	560 (255)	20/20	4''-99''	840	840	1525
160x125	Sing/Bk	8'10'' x 7'0'' x 11''	2.69 x 2.14 x 0.28	61.7 (5.8)	54.1 (5.2)	690 (313)	20/25	4''-99''	1060	1060	1915
160x150	Sing/Bk	8'10'' x 8'4'' x 11''	2.69 x 2.53 x 0.28	73.2 (6.8)	64.9 (6.2)	815 (370)	20/30	4''-99''	1280	1280	2310
160x175	Sing/Bk	<u>8'10" x 9'8" x 11"</u>	2.69 x 2.93 x 0.28	84.7 (7.9)	75.8 (7.3)	940 (427)	20/35	4"-99"	1450	1450	2650
160x200	Sing/Bk	8'10'' x 10'11'' x 11''	2.69 x 3.33 x 0.28	96.1 (9.0)	86.6 (8.3)	10/0 (486)	20/40	4"-99"	16/0	16/0	3040
160x223 160x250	Sing/Bk	8'10'' x 13'6'' x 11''	$2.09 \times 3.72 \times 0.28$		108.2 (10.4)	1325 (602)	20/43	4 -99 /''_QQ''	2060	2060	3775
160x275	Sing/Bk	8'10'' x 14'10'' x 11''	2.69 x 4.52 x 0.28	130.5 (12.2)	119.0 (11.4)	1450 (658)	20/55	4"-99"	2280	2280	4165
160x300	Sing/Bk	8'10'' x 16'2'' x 11''	2.69 x 4.91 x 0.28	142.0 (13.2)	129.8 (12.5)	1580 (717)	20/60	4''-99''	2500	2500	4555
160x325	Sing/Bk	8'10'' x 17'5'' x 11''	2.69 x 5.31 x 0.28	153.5 (14.3)	140.7 (13.5)	1705 (774)	20/65	4''-99''	2670	2670	4900
160x350	Sing/Bk	8'10'' x 18'9'' x 11''	2.69 x 5.7 x 0.28	164.9 (15.3)	151.5 (14.6)	1835 (833)	20/70	4''-99''	2890	2890	5290
160x375	Sing/Bk	8'10'' x 20'0'' x 11''	2.69 x 6.1 x 0.28	176.4 (16.4)	162.3 (15.6)	1960 (890)	20/75	4''-99''	3110	3110	5680
160x400	Sing/Bk	8'10'' x 21'4'' x 11''	2.69 x 6.5 x 0.28	187.9 (17.5)	173.1 (16.6)	2090 (949)	20/80	4"-99"	3280	3280	6025
160x425	Sing/Bk	8'10'' x 22'8'' x 11''	2.69 x 6.89 x 0.28	199.3 (18.5)	183.9 (17.7)	2215 (1005)	20/85	4"-99"	3500	3500	6415
$\frac{160x430}{160x475}$	Sing/Bk	8'10'' x 25'3'' x 11''	2.09 x 7.29 x 0.20	210.6 (19.0)	205.6 (19.8)	2340 (1082)	20/90	4°-99° /''_00''	3/20	3/20	7150
$\frac{100x473}{160x500}$	Sing/Bk	8'10'' x 26'6'' x 11''	2.69 x 8.08 x 0.28	233 7 (21.7)	216.4 (20.8)	2595 (1121)	20/100	4 -77 4''_99''	4110	4110	7540
160x525	Sina/Bk	8'10" x 27'10" x 11"	2.69 x 8.48 x 0.28	245.2 (22.8)	227.2 (21.8)	2725 (1237)	20/105	4"-99"	4330	4330	7930
160x550	Sing/Bk	8'10'' x 29'2'' x 11''	2.69 x 8.87 x 0.28	256.7 (23.9)	238.0 (22.9)	2850 (1293)	20/110	4''-99''	4500	4500	8275
160x575	Sing/Bk	8'10'' x 30'5'' x 11''	2.69 x 9.27 x 0.28	268.1 (24.9)	248.8 (23.9)	2980 (1352)	20/115	4''-99''	4730	4730	8670
160x600	Sing/Bk	8'10'' x 31'9'' x 11''	2.69 x 9.67 x 0.28	279.6 (26.0)	259.6 (25.0)	3105 (1409)	20/120	4''-99''	4950	4950	9065
160x625	Sing/Bk	8'10'' x 33'0'' x 11''	2.69 x 10.06 x 0.28	291.1 (27.1)	270.4 (26.0)	3235 (1468)	20/125	4''-99''	5120	5120	9405
160x650	Sing/Bk	8'10'' x 34'4'' x 11''	2.69 x 10.46 x 0.28	302.5 (28.1)	281.3 (27.0)	3360 (1525)	20/130	4''-99''	5340	5340	9795
160x675	Sing/Bk	8'10'' x 35'8'' x 11''	2.69 x 10.86 x 0.28	314.0 (29.2)	292.1 (27.8)	3490 (1584)	20/135	4"-99"	5560	5560	10190
$\frac{160 \times 700}{160 \times 725}$	Sing/Bk	8'IU'' x 30'II'' x II''	2.69 x 11.25 x 0.28	325.5 (30.3)	302.9 (28.9)	3013 (1040)	20/140	4"-99"	5050	5050	10000
160x723	Sing/Bk	8'10'' x 30'5' x 11''	2.09 x 11.03 x 0.28	348 4 (32 4)	324 5 (30.9)	3740 (1097)	20/143	4 - 77	6170	6170	11310
160×775	Sing/Bk	8'10'' x 40'10'' x 11''	2.67 x 12.04 x 0.20	3.59.9 (33.5)	335 3 (32.0)	3995 (1813)	20/155	4''_99''	6340	6340	11655
160x800	Sing/Bk	8'10'' x 42'2'' x 11''	2.69 x 12.84 x 0.28	371.3 (34.5)	346.2 (33.0)	4125 (1872)	20/160	4''-99''	6560	6560	12045
160x825	Sing/Bk	8'10'' x 43'5'' x 11''	2.69 x 13.23 x 0.28	382.8 (35.6)	357.0 (34.1)	4250 (1928)	20/165	4''-99''	6780	6780	12435
180x100	Sing/Bk	9'11" x 5'9" x 11"	3.01 x 1.74 x 0.28	56.2 (5.2)	48.7 (4.6)	625 (284)	22/20	4''-112''	925	925	1695
180x125	Sing/Bk	9'11" x 7'0" x 11"	3.01 x 2.14 x 0.28	69.0 (6.4)	60.9 (5.8)	770 (350)	22/25	4''-112''	1165	1165	2130
180×150	Sing/Bk	9'11" x 8'4" x 11"	3.01 x 2.53 x 0.28	81.8 (7.6)	73.1 (7.0)	910 (413)	22/30	4"-112"	1410	1410	2565
180x1/5	Sing/Bk	9'11'' x 9'8'' x 11''	3.01 x 2.93 x 0.28	94.7 (8.8)	85.2 (8.1)	1055 (4/9)	22/35	4"-112"	1600	1600	2950
180x200	Sing/Bk	9'11'' X 10'11'' X 11''	3.01 x 3.33 x 0.28	120.3 (10.0)	97.4 (9.3) 109.6 (10.4)	1340 (608)	22/40	4"-112" /"_112"	2080	2080	3820
180x250	Sing/Bk	9'11" x 13'6" x 11"	3.01 x 4.12 x 0.28	133.1 (12.4)	121.7 (11.6)	1480 (672)	22/45	4"-112"	2000	2275	4205
180x275	Sing/Bk	9'11" x 14'10" x 11"	3.01 x 4.52 x 0.28	145.9 (13.6)	133.9 (12.8)	1620 (735)	22/55	4''-112''	2515	2515	4635
180x300	Sing/Bk	9'11'' x 16'2'' x 11''	3.01 x 4.91 x 0.28	158.7 (14.8)	146.1 (13.9)	1765 (801)	22/60	4''-112''	2755	2755	5070
180x325	Sing/Bk	9'11'' x 17'5'' x 11''	3.01 x 5.31 x 0.28	171.6 (16.0)	158.2 (15.1)	1905 (865)	22/65	4''-112''	2950	2950	5455
180x350	Sing/Bk	9'11'' x 18'9'' x 11''	3.01 x 5.7 x 0.28	184.4 (17.2)	170.4 (16.2)	2050 (930)	22/70	4''-112''	3190	3190	5890
180x375	Sing/Bk	9'11'' x 20'0'' x 11''	3.01 x 6.1 x 0.28	197.2 (18.4)	182.6 (17.4)	2190 (994)	22/75	4"-112"	3430	3430	6325
180x400	Sing/Bk	9'11" x 21'4" x 11"	3.01 x 6.5 x 0.28	210.0 (19.6)	194.7 (18.6)	2335 (1060)	22/80	4"-112"	3625	3625	6/10
180x425	Sing/BK	9'II'' X ZZ'8'' X II''	3.01 x 0.89 x 0.28	222.8 (20.7)	200.9 (19.7)	24/3 (1123)	22/83	4"-112" 4" 112"	3803	3803	7575
$\frac{100x430}{180x475}$	Sing/Bk	9'11'' x 25'3'' x 11''	3.01 x 7.69 x 0.28	248 5 (23.1)	231.2 (22.0)	2760 (1252)	22/90	4 -112	4300	4300	7965
180x500	Sina/Bk	9'11'' x 26'6'' x 11''	3.01 x 8.08 x 0.28	261.3 (24.3)	243.4 (23.2)	2905 (1318)	22/100	4"-112"	4540	4540	8395
180x525	Sing/Bk	9'11" x 27'10" x 11"	3.01 x 8.48 x 0.28	274.1 (25.5)	255.6 (24.4)	3045 (1382)	22/105	4"-112"	4780	4780	8830
180x550	Sing/Bk	9'11'' x 29'2'' x 11''	3.01 x 8.87 x 0.28	286.9 (26.7)	267.7 (25.5)	3185 (1445)	22/110	4''-112''	4975	4975	9215
180x575	Sing/Bk	9'11'' x 30'5'' x 11''	3.01 x 9.27 x 0.28	299.7 (27.9)	279.9 (26.7)	3330 (1511)	22/115	4''-112''	5220	5220	9660
180x600	Sing/Bk	9'11'' x 31'9'' x 11''	3.01 x 9.67 x 0.28	312.6 (29.1)	292.1 (27.8)	3470 (1574)	22/120	4''-112''	5465	5465	10090
180x625	Sing/Bk	9'11" x 33'0" x 11"	3.01 x 10.06 x 0.28	325.4 (30.3)	304.2 (29.0)	3615 (1640)	22/125	4"-112"	5655	5655	10480
180x650	Sing/Bk	9'11" x 34'4" x 11"	3.01 x 10.46 x 0.28	338.2 (31.5)	316.4 (30.2)	3/55 (1704)	22/130	4"-112"	5895	5895	10910
180x6/5	Sing/Bk	9'11'' x 35'8'' x 11''	3.01 x 10.86 x 0.28	351.0 (32./)	328.6 (31.0)	3900 (1/70)	22/135	4"-112"	6140	6140	11345
180×725	Sing/Bk	9'11' x 30'11' X 11''	3 01 x 11.25 x 0.28	376 7 (35.1)	352 9 (22 1)	4185 (1800)	22/140	4 -112"	6570	6570	12165
180x750	Sing/Bk	9'11'' x 39'6'' x 11''	3.01 x 12.04 x 0.28	389.5 (36.2)	365.1 (34.5)	4325 (1962)	22/150	4"-112"	6810	6810	12600
180x775	Sing/Bk	9'11" x 40'10" x 11"	3.01 x 12.44 x 0.28	402.3 (37.4)	377.3 (35.7)	4470 (2028)	22/155	4"-112"	7005	7005	12985
180x800	Sing/Bk	9'11'' x 42'2'' x 11''	3.01 x 12.84 x 0.28	415.1 (38.6)	389.4 (36.8)	4610 (2092)	22/160	4''-112''	7245	7245	13420
180x825	Sing/Bk	9'11'' x 43'5'' x 11''	3.01 x 13.23 x 0.28	427.9 (39.8)	401.6 (38.0)	4750 (2155)	22/165	4''-112''	7485	7485	13850
200x100	Multi/Bk	10'11" x 5'9" x 11"	3.33 x 1.74 x 0.28	62.1 (5.8)	54.1 (5.1)	690 (313)	25/20	4''-124''	1165	1165	2020
200x125	Multi/Bk	10'11'' x 7'0'' x 11''	3.33 x 2.14 x 0.28	76.3 (7.1)	67.6 (6.4)	850 (386)	25/25	4"-124"	1475	1475	2545
200x150	Multi/Bk	10'11'' x 8'4'' x 11''	3.33 x 2.53 x 0.28	90.5 (8.4)	81.2 (/./)	1005 (456)	25/30	4"-124"	1/85	2000	30/0
ZUUXI/J	IVIUIII/ DK	1011 X70 X11	J.JJ X Z.7J X U.ZŎ	104.0 [7.0]	74./ (7.0)	1103 [329]	20/00	4 -124	2000	2000	2200

Lines x Columns	Sections/ Ventilated	Cabinet Dimensions Feet-Inches H x W x D	Cabinet Dimensions Meters H x W x D	Cabinet Square Feet (Square Meters)	Active Area Square Feet (Square Meters)	Cabinet Weight Pounds (kilograms)	Lines/ Characters	Character Height	Maximum Watts Amber Red RGB
200×200	Multi/Bk	10'11" x 10'11" x 11"	3 33 x 3 33 x 0 28		108.2 (10.2)	1320 (599)	25/40	1121	2310 2310 4025
200x200	Multi/Bk	10'11" x 12'3" x 11"	3 33 x 3 72 x 0 28	133.0 (12.4)	121 7 (11.5)	1480 (672)	25/45	4"-124"	2620 2620 4550
200x250	Multi/Bk	10'11" x 13'6" x 11"	3.33 x 4.12 x 0.28	147.2 (13.7)	135.2 (12.8)	1635 (742)	25/50	4"-124"	2835 2835 4975
200x275	Multi/Bk	10'11" x 14'10" x 11"	3.33 x 4.52 x 0.28	161.3 (15.1)	148.8 (14.1)	1795 (815)	25/55	4''-124''	3145 3145 5500
200x300	Multi/Bk	10'11'' x 16'2'' x 11''	3.33 x 4.91 x 0.28	175.5 (16.4)	162.3 (15.4)	1950 (885)	25/60	4''-124''	3455 3455 6025
200x325	Multi/Bk	10'11" x 17'5" x 11"	3.33 x 5.31 x 0.28	189.7 (17.7)	175.8 (16.6)	2110 (958)	25/65	4''-124''	3670 3670 6455
200x350	Multi/Bk	10'11'' x 18'9'' x 11''	3.33 x 5.7 x 0.28	203.8 (19.0)	189.3 (17.9)	2265 (1028)	25/70	4''-124''	3980 3980 6980
200x375	Multi/Bk	10'11'' x 20'0'' x 11''	3.33 x 6.1 x 0.28	218.0 (20.3)	202.8 (19.2)	2420 (1098)	25/75	4''-124''	4290 4290 7505
200x400	Multi/Bk	10'11'' x 21'4'' x 11''	3.33 x 6.5 x 0.28	232.2 (21.6)	216.4 (20.5)	2580 (1171)	25/80	4''-124''	4505 4505 7930
200x425	Multi/Bk	10'11" x 22'8" x 11"	3.33 x 6.89 x 0.28	246.3 (22.9)	229.9 (21.8)	2735 (1241)	25/85	4''-124''	4815 4815 8455
200x450	Multi/Bk	10'11" x 23'11" x 11"	3.33 x 7.29 x 0.28	260.5 (24.3)	243.4 (23.0)	2895 (1314)	25/90	4"-124"	5125 5125 8980
200x4/5	Multi/Bk	10'11" x 25'3" x 11"	3.33 x 7.69 x 0.28	2/4./ (25.6)	256.9 (24.3)	3050 (1384)	25/95	4"-124"	5340 5340 9410
200x500	Multi/Bk	10'11'' x 20'0'' x 11''	3.33 x 8.08 x 0.28	288.9 (20.9)	270.4 (25.6)	3210 (1457)	25/100	4"-124"	5050 5050 9935
200x525 200x550	/VIUITI/DK		3.33 X 0.40 X 0.20	2172 (20.2)	204.0 (20.9)	2525 (1527)	25/105	4"-124"	<u>4175</u> <u>4175</u> <u>10400</u>
200x550	Multi/Bk	1011 x 27 2 x 11	3 33 × 0 27 × 0 28	331 / (30.0)	311.0 (20.2)	3680 (1670)	25/115	4 -124	6500 6500 11/30
$\frac{200x575}{200x600}$	Multi/Bk	10'11" x 31'9" x 11"	3.33 x 9.67 x 0.28	345 5 (32 2)	324 5 (30 7)	3840 (1742)	25/120	4''-124''	6810 6810 11955
200x625	Multi/Bk	10'11" x 33'0" x 11"	3.33 x 10.06 x 0.28	359.7 (33.5)	338.0 (32.0)	3995 (1813)	25/125	4"-124"	7025 7025 12380
200x650	Multi/Bk	10'11'' x 34'4'' x 11''	3.33 x 10.46 x 0.28	373.9 (34.8)	351.6 (33.3)	4150 (1883)	25/130	4"-124"	7335 7335 12905
200x675	Multi/Bk	10'11" x 35'8" x 11"	3.33 x 10.86 x 0.28	388.0 (36.2)	365.1 (34.2)	4310 (1955)	25/135	4''-124''	7645 7645 13430
200x700	Multi/Bk	10'11" x 36'11" x 11"	3.33 x 11.25 x 0.28	402.2 (37.5)	378.6 (35.5)	4465 (2026)	25/140	4''-124''	7860 7860 13860
200x725	Multi/Bk	10'11'' x 38'3'' x 11''	3.33 x 11.65 x 0.28	416.4 (38.8)	392.1 (36.8)	4625 (2098)	25/145	4''-124''	8170 8170 14385
200x750	Multi/Bk	10'11" x 39'6" x 11"	3.33 x 12.04 x 0.28	430.6 (40.1)	405.6 (38.1)	4780 (2169)	25/150	4''-124''	8480 8480 14910
200x775	Multi/Bk	10'11'' x 40'10'' x 11''	3.33 x 12.44 x 0.28	444.7 (41.4)	419.2 (39.4)	4940 (2241)	25/155	4''-124''	8695 8695 15340
200x800	Multi/Bk	10'11" x 42'2" x 11"	3.33 x 12.84 x 0.28	458.9 (42.8)	432.7 (40.6)	5095 (2312)	25/160	4''-124''	9005 9005 15860
200x825	Multi/Bk	10'11" x 43'5" x 11"	3.33 x 13.23 x 0.28	473.1 (44.1)	446.2 (41.9)	5255 (2384)	25/165	4"-124"	9315 9315 16385
220x100	Multi/Bk	12'0" x 5'9" x 11"	3.64 x 1./4 x 0.28	68.1 (6.3)	59.5 (5.6)	/60 (345)	2//20	4"-13/"	1250 1250 2195
220x125	Multi/Bk	12'0'' x /'0'' x 11''	3.64 x 2.14 x 0.28	83.6 (7.8)	/4.4 (/.0)	930 (422)	27/25	4"-13/"	1585 1585 2/60
220x150	/VIUITI/ BK	12:0" x 8:4" x 11"	3.04 X 2.53 X 0.28	99.1 (9.2)	89.3 (8.4)	100 (499)	27/30	4"-13/"	1915 1915 3325
220x1/3	/VIUITI/BK	12:0" x 9:8" x 11"	3.04 X 2.93 X 0.28	114.0 (10.7)	104.2 (9.8)	12/3 (3/9)	27/33	4"-137"	2130 2130 3800
220x200	Multi/Bk	120 X 10 11 X 11	$3.04 \times 3.33 \times 0.28$	145 7 (12.1)	133.0 (12.6)	1620 (735)	27/40	4 -137	2400 2400 4303
220×250	Multi/Bk	12'0'' x 13'6'' x 11''	3 64 x 4 12 x 0 28	161 2 (15.0)	148.8 (14.0)	1790 (812)	27/50	4"-137"	3050 3050 5405
220x275	Multi/Bk	12'0" x 14'10" x 11"	3.64 x 4.52 x 0.28	176.7 (16.5)	163.6 (15.4)	1965 (892)	27/55	4"-137"	3380 3380 5975
220x300	Multi/Bk	12'0'' x 16'2'' x 11''	3.64 x 4.91 x 0.28	192.2 (17.9)	178.5 (16.8)	2135 (969)	27/60	4''-137''	3710 3710 6540
220x325	Multi/Bk	12'0" x 17'5" x 11"	3.64 x 5.31 x 0.28	207.8 (19.3)	193.4 (18.2)	2310 (1048)	27/65	4''-137''	3945 3945 7010
220x350	Multi/Bk	12'0'' x 18'9'' x 11''	3.64 x 5.7 x 0.28	223.3 (20.7)	208.3 (19.6)	2480 (1125)	27/70	4''-137''	4280 4280 7580
220x375	Multi/Bk	12'0'' x 20'0'' x 11''	3.64 x 6.1 x 0.28	238.8 (22.2)	223.1 (21.0)	2655 (1205)	27/75	4''-137''	4610 4610 8145
220x400	Multi/Bk	12'0'' x 21'4'' x 11''	3.64 x 6.5 x 0.28	254.3 (23.7)	238.0 (22.4)	2825 (1282)	27/80	4''-137''	4845 4845 8620
220x425	Multi/Bk	12'0'' x 22'8'' x 11''	3.64 x 6.89 x 0.28	269.8 (25.1)	252.9 (23.8)	3000 (1361)	27/85	4"-137"	5180 5180 9185
220x450	Multi/Bk	12'0" x 23'11" x 11"	3.64 x 7.29 x 0.28	285.4 (26.5)	267.7 (25.2)	3170 (1438)	27/90	4"-137"	5510 5510 9755
220x475	Multi/Bk	12'0" x 25'3" x 11"	3.64 x 7.69 x 0.28	300.9 (28.0)	282.6 (26.6)	3340 (1515)	27/95	4"-137"	5745 5745 10225
220x500	Multi/Bk	12'0'' x 26'6'' x 11''	3.64 x 8.08 x 0.28	316.4 (29.4)	297.5 (28.0)	3515 (1595)	27/100	4"-13/"	60/5 60/5 10/90
220x525	/VIUITI/BK	12:0" x 27:10" x 11"	3.04 X 8.48 X 0.28	331.9 (30.9)	312.4 (29.4)	3083 (10/2)	27/105	4"-137"	6645 6645 11920
220x550	Multi/Bk	12 0 X 29 2 X 11	3.04 x 0.07 x 0.28	363 0 (33 7)	3/2 1 (32.2)	4030 (1231)	27/110	4 -137	6005 6005 12/15
$\frac{220x575}{220x600}$	Multi/Bk	12'0'' x 31'9'' x 11''	3.64 x 9.67 x 0.28	378 5 (35.2)	3570 (33.6)	4205 (1908)	27/120	4"-137"	7325 7325 12980
220x625	Multi/Bk	12'0'' x 33'0'' x 11''	3.64 x 10.06 x 0.28	394.0 (36.6)	371.8 (35.0)	4375 (1985)	27/125	4"-137"	7560 7560 13455
220x650	Multi/Bk	12'0" x 34'4" x 11"	3.64 x 10.46 x 0.28	409.5 (38.1)	386.7 (36.4)	4550 (2064)	27/130	4"-137"	7890 7890 14020
220x675	Multi/Bk	12'0'' x 35'8'' x 11''	3.64 x 10.86 x 0.28	425.1 (39.5)	401.6 (37.5)	4720 (2141)	27/135	4''-137''	8225 8225 14590
220x700	Multi/Bk	12'0" x 36'11" x 11"	3.64 x 11.25 x 0.28	440.6 (41.0)	416.5 (38.9)	4895 (2221)	27/140	4''-137''	8460 8460 15060
220x725	Multi/Bk	12'0'' x 38'3'' x 11''	3.64 x 11.65 x 0.28	456.1 (42.4)	431.3 (40.3)	5065 (2298)	27/145	4''-137''	8790 8790 15625
220x750	Multi/Bk	12'0'' x 39'6'' x 11''	3.64 x 12.04 x 0.28	471.6 (43.8)	446.2 (41.7)	5240 (2377)	27/150	4''-137''	9125 9125 16195
220x775	Multi/Bk	12'0" x 40'10" x 11"	3.64 x 12.44 x 0.28	487.2 (45.3)	461.1 (43.1)	5410 (2454)	27/155	4''-137''	9360 9360 16665
220x800	Multi/Bk	12'0" x 42'2" x 11"	3.64 x 12.84 x 0.28	502.7 (46.7)	476.0 (44.5)	5580 (2532)	27/160	4''-137''	9690 9690 17235
220x825	Multi/Bk	12'0'' x 43'5'' x 11''	3.64 x 13.23 x 0.28	518.2 (48.2)	490.8 (45.9)	5755 (2611)	27/165	4''-137''	10020 10020 17800
240x100	Multi/Bk	13'0'' x 5'9'' x 11''	3.96 x 1.74 x 0.28	74.0 (6.9)	64.9 (6.2)	825 (375)	30/20	4"-149"	1335 1335 2365
240x125	Multi/Bk	13'0" x /'0" x 11"	3.96 x 2.14 x 0.28	90.9 (8.5)	81.2 (7.8)	1010 (459)	30/25	4"-149"	1695 1695 2975
240x150	Multi/Bk	13'0'' x 8'4'' x 11''	3.90 x 2.53 x 0.28	107.7 (10.0)	<u> </u>	1200 (545)	30/30	4"-149"	2040 2040 3585
240x1/3	/VIUITI/BK	130 X 9'8' X 11''	3.70 X 2.73 X U.28	124.0 (11.0)	1208 (10.9)	1505 (029)	30/35	4 -149"	2500 2500 4100
240x200	Multi /RL	13'0'' x 12'3'' v 11''	$3.70 \times 3.33 \times 0.20$	158 / (1/ 7)	1461 (14.0)	1760 (700)	30/40	4 -149 <u>4''_1/0''</u>	3005 3005 5300
240x250	Multi/Rk	13'0" x 13'6" x 11"	3.96 x 4 12 x 0.28	175.2 (16.3)	162.3 (15.6)	1950 (885)	30/50	4''-149''	3260 3260 5835
240x275	Multi/Bk	13'0" x 14'10" x 11"	3.96 x 4.52 x 0.28	192.1 (17.9)	178.5 (17.2)	2135 (969)	30/55	4"-149"	3615 3615 6445
240x300	Multi/Bk	13'0'' x 16'2'' x 11''	3.96 x 4.91 x 0.28	209.0 (19.4)	194.7 (18.7)	2320 (1053)	30/60	4''-149''	3970 3970 7055
240x325	Multi/Bk	13'0" x 17'5" x 11"	3.96 x 5.31 x 0.28	225.9 (21.0)	211.0 (20.3)	2510 (1139)	30/65	4''-149''	4225 4225 7570
240x350	Multi/Bk	13'0'' x 18'9'' x 11''	3.96 x 5.7 x 0.28	242.7 (22.6)	227.2 (21.8)	2695 (1223)	30/70	4"-149"	4580 4580 8180

Lines x Columns	Sections/ Ventilated	Cabinet Dimensions Feet-Inches H x W x D	Cabinet Dimensions Meters H x W x D	Cabinet Square Feet (Square Meter	Active Square	Area e Feet Meters)	Cabinet Pou (kiloo	Weight Inds Irams)	Lines/ Characters	Character Height	Ma Amber	ximum V Red	latts RGB
240x375	Multi/Bk	13'0'' x 20'0'' x 11''	396 x 61 x 0.28	2.59.6 (24	2) 243.4	(23.4)	288.5	(1309)	30/75	4''_149''	4930	4930	8790
240x400	Multi/Bk	13'0" x 21'4" x 11"	3.96 x 6.5 x 0.28	276.5 (24.	7) 259.6	(25.0)	3070	(1393)	30/80	4"-149"	5190	5190	9305
240x425	Multi/Bk	13'0'' x 22'8'' x 11''	3.96 x 6.89 x 0.28	293.3 (27.3	3) 275.9	(26.5)	3260	(1479)	30/85	4''-149''	5540	5540	9915
240x450	Multi/Bk	13'0" x 23'11" x 11"	3.96 x 7.29 x 0.28	310.2 (28.9) 292.1	(28.1)	3445	(1563)	30/90	4''-149''	5895	5895	10525
240x475	Multi/Bk	13'0'' x 25'3'' x 11''	3.96 x 7.69 x 0.28	327.1 (30.	5) 308.3	(29.6)	3635	(1649)	30/95	4''-149''	6150	6150	11040
240x500	Multi/Bk	13'0'' x 26'6'' x 11''	3.96 x 8.08 x 0.28	344.0 (32.0	0) 324.5	(31.2)	3820	(1733)	30/100	4''-149''	6505	6505	11650
240x525	Multi/Bk	13'0" x 27'10" x 11"	3.96 x 8.48 x 0.28	360.8 (33.)	6) 340.8	(32.8)	4010	(1819)	30/105	4''-149''	6860	6860	12260
240x550	Multi/Bk	13'0'' x 29'2'' x 11''	3.96 x 8.87 x 0.28	377.7 (35.	1) 357.0	(34.3)	4195	(1903)	30/110	4''-149''	7115	7115	12775
240x575	Multi/Bk	13'0" x 30'5" x 11"	3.96 x 9.27 x 0.28	394.6 (36.	7) 373.2	(35.9)	4380	(1987)	30/115	4''-149''	7485	7485	13400
240x600	Multi/Bk	13'0'' x 31'9'' x 11''	3.96 x 9.67 x 0.28	411.5 (38.	3) 389.4	(37.4)	4570	(2073)	30/120	4"-149"	7840	7840	14010
240x625	Multi/Bk	13'0" x 33'0" x 11"	3.96 x 10.06 x 0.28	428.3 (39.8	3) 405.6	(39.0)	4755	(2157)	30/125	4"-149"	8095	8095	14525
240x650	Multi/Bk	13'0'' x 34'4'' x 11''	3.96 x 10.46 x 0.28	445.2 (41.4	4) 421.9	(40.6)	4945	(2244)	30/130	4"-149"	8450	8450	15135
240x0/3	/VIUITI/BK	13.0" x 33.8" x 11"	3.90 X 10.80 X 0.28	402.1 (43.)	() 438.1 () 454.2	(41.7)	5220	(2327)	30/135	4"-149"	8800	8800	15/45
$\frac{240x}{240x}$	Multi/Bk		3.90 x 11.23 x 0.28	479.0 (44.	0 434.3 1) 470.5	(43.3)	5505	(2414)	30/140	4 -149	9080	9080	16200
$\frac{240x723}{240x750}$	Multi/Bk	13'0" x 30'5" x 11"	3.96 x 12.04 x 0.28	512 7 (47)	7) 486.8	(44.7)	5695	(2470)	30/143	<u>4 -147</u> <u>/''_1/9''</u>	9765	9765	17/80
240x775	Multi/Bk	13'0'' x 40'10'' x 11''	$3.96 \times 12.04 \times 0.20$	529.6 (49.)	3) 503.0	(48.0)	5880	(2668)	30/155	4"_149"	10020	10020	17995
240x800	Multi/Bk	13'0'' x 42'2'' x 11''	3.96 x 12.84 x 0.28	546.5 (50.)	8) 519.2	(49.5)	6070	(2754)	30/160	4"-149"	10375	10375	18605
240x825	Multi/Bk	13'0'' x 43'5'' x 11''	3.96 x 13.23 x 0.28	563.3 (52.4	4) 535.4	(51.1)	6255	(2838)	30/165	4"-149"	10730	10730	19215
260x100	Multi/Bk	14'1" x 5'9" x 11"	4.28 x 1.74 x 0.28	79.9 (7.4)	70.4	(6.7)	890	(404)	32/20	4''-162''	1420	1420	2535
260x125	Multi/Bk	14'1'' x 7'0'' x 11''	4.28 x 2.14 x 0.28	98.1 (9.2)	87.9	(8.4)	1090	(495)	32/25	4''-162''	1800	1800	3190
260x150	Multi/Bk	14'1'' x 8'4'' x 11''	4.28 x 2.53 x 0.28	116.4 (10.8	3) 105.5	(10.1)	1295	(588)	32/30	4''-162''	2170	2170	3840
260x175	Multi/Bk	14'1" x 9'8" x 11"	4.28 x 2.93 x 0.28	134.6 (12.5	5) 123.1	(11.8)	1495	(679)	32/35	4''-162''	2450	2450	4400
260x200	Multi/Bk	14'1" x 10'11" x 11"	4.28 x 3.33 x 0.28	152.8 (14.3	3) 140.7	(13.4)	1700	(772)	32/40	4''-162''	2825	2825	5050
260x225	Multi/Bk	14'1" x 12'3" x 11"	4.28 x 3.72 x 0.28	171.0 (15.9	9) 158.2	(15.1)	1900	(862)	32/45	4''-162''	3200	3200	5695
260x250	Multi/Bk	14'1" x 13'6" x 11"	4.28 x 4.12 x 0.28	189.3 (17.6	5) 175.8	(16.8)	2105	(955)	32/50	4"-162"	3475	3475	6260
260x275	Multi/Bk	14'1" x 14'10" x 11"	4.28 x 4.52 x 0.28	207.5 (19.3	3) 193.4	(18.5)	2305	(1046)	32/55	4"-162"	3850	3850	6915
260x300	Multi/Bk	14'1" x 16'2" x 11"	4.28 x 4.91 x 0.28	225.7 (21.0	211.0	(20.2)	2510	(1139)	32/60	4"-162"	4225	4225	/5/0
200X323	/VIUITI/ BK	14'1'' x 17'3'' x 11''	4.28 x 5.31 x 0.28	243.9 (22.	/) <u>ZZ8.3</u>	(21.8)	2/10	(1230)	32/03	4"-102"	4303	4303	0700
200x330	/VIUITI/BK	14'1" X 18'9" X 11"	4.28 x 5.7 x 0.28	202.2 (24.	4) <u>240.1</u> 1) <u>262.7</u>	(23.3)	2915	(1323)	32/70	4"-102"	4880	4880	8/80
$\frac{200x373}{260x400}$	Multi/Bk	14 1 X 20 0 X 11	4.28 x 0.1 x 0.28	200.4 (20.	$\frac{1}{203.7}$	(23.2)	3115	(1413) (1504)	32/73	4 -102	5530	5530	9430
260x400	Multi/Bk	14'1" x 22'4 x 11	4.20 × 0.3 × 0.20	316.9 (29)	5) 298.8	(20.7)	3520	(1504) (1597)	32/85	4"-162"	5905	5905	10640
260x450	Multi/Bk	14'1" x 23'11" x 11"	4.28 x 7.29 x 0.28	335.1 (31.2	2) 316.4	(30.2)	3720	(1688)	32/90	4"-162"	6280	6280	11295
260x475	Multi/Bk	14'1" x 25'3" x 11"	4.28 x 7.69 x 0.28	353.3 (32.9	7) 334.0	(31.9)	3925	(1781)	32/95	4''-162''	6560	6560	11850
260x500	Multi/Bk	14'1" x 26'6" x 11"	4.28 x 8.08 x 0.28	371.5 (34.	6) 351.6	(33.6)	4125	(1872)	32/100	4''-162''	6935	6935	12505
260x525	Multi/Bk	14'1" x 27'10" x 11"	4.28 x 8.48 x 0.28	389.8 (36.)	3) 369.1	(35.3)	4330	(1965)	32/105	4''-162''	7310	7310	13160
260x550	Multi/Bk	14'1" x 29'2" x 11"	4.28 x 8.87 x 0.28	408.0 (38.	0) 386.7	(37.0)	4530	(2055)	32/110	4''-162''	7585	7585	13715
260x575	Multi/Bk	14'1'' x 30'5'' x 11''	4.28 x 9.27 x 0.28	426.2 (39.)	7) 404.3	(38.6)	4735	(2148)	32/115	4''-162''	7980	7980	14385
260x600	Multi/Bk	14'1" x 31'9" x 11"	4.28 x 9.67 x 0.28	444.4 (41.4	4) 421.9	(40.3)	4935	(2239)	32/120	4''-162''	8355	8355	15040
260x625	Multi/Bk	14'1" x 33'0" x 11"	4.28 x 10.06 x 0.28	462.7 (43.	1) 439.4	(42.0)	5140	(2332)	32/125	4"-162"	8630	8630	15595
260x650	Multi/Bk	14'1" x 34'4" x 11"	4.28 x 10.46 x 0.28	480.9 (44.	8) 457.0	(43.7)	5340	(2423)	32/130	4"-162"	9005	9005	16250
260x6/5	Multi/Bk	14'1'' x 35'8'' x 11''	4.28 x 10.86 x 0.28	499.1 (46.	5) 4/4.6	(44.9)	5545	(2516)	32/135	4"-162"	9380	9380	16905
200X/00	/VIUITI/BK	14'1'' X 30'11'' X 11''	4.28 x 11.25 x 0.28	525 6 (40)	2) 492.2	(40.0)	5045	(2000)	32/140	4"-102"	9000	9000	1/400
260x723	Multi/Bk	14 1 X 30 3 X 11	4.28 x 11.03 x 0.28	553.8 (51)	51 5273	(40.3)	6150	(2097)	32/143	4 -102	10033	10033	18765
$\frac{200x730}{260x775}$	Multi/Bk	14'1 × 37'0 × 11'	4.20 × 12.04 × 0.20	572 0 (53)	21 5/10	(50.0) (51.7)	6350	(2881)	32/155	4 =102 /''_162''	10410	10410	19325
260x800	Multi/Bk	14'1" x 42'2" x 11"	4.28 x 12.84 x 0.28	590.2 (55.)	0) 562.5	(53.3)	6555	(2974)	32/160	4"-162"	11060	11060	19975
260x825	Multi/Bk	14'1'' x 43'5'' x 11''	4.28 x 13.23 x 0.28	608.5 (56.	6) 580.1	(55.0)	6755	(3065)	32/165	4"-162"	11435	11435	20630
280x100	Multi/Bk	15'1'' x 5'9'' x 11''	4.6 x 1.74 x 0.28	85.8 (8.0)	75.8	(7.2)	955	(434)	35/20	4''-174''	1505	1505	2705
280x125	Multi/Bk	15'1" x 7'0" x 11"	4.6 x 2.14 x 0.28	105.4 (9.8)	94.7	(9.0)	1175	(533)	35/25	4''-174''	1900	1900	3400
280x150	Multi/Bk	15'1" x 8'4" x 11"	4.6 x 2.53 x 0.28	125.0 (11.6	5) 113.6	(10.8)	1390	(631)	35/30	4''-174''	2300	2300	4100
280x175	Multi/Bk	15'1" x 9'8" x 11"	4.6 x 2.93 x 0.28	144.6 (13.5	5) 132.5	(12.6)	1605	(729)	35/35	4''-174''	2600	2600	4700
280x200	Multi/Bk	15'1" x 10'11" x 11"	4.6 x 3.33 x 0.28	164.2 (15.3	3) 151.5	(14.4)	1825	(828)	35/40	4''-174''	2995	2995	5395
280x225	Multi/Bk	15'1" x 12'3" x 11"	4.6 x 3.72 x 0.28	183.7 (17.1) 170.4	(16.2)	2040	(926)	35/45	4''-174''	3390	3390	6090
280x250	Multi/Bk	15'1" x 13'6" x 11"	4.6 x 4.12 x 0.28	203.3 (19.0) 189.3	(18.0)	2260	(1026)	35/50	4''-174''	3690	3690	6690
280x275	Multi/Bk	15'1" x 14'10" x 11"	4.6 x 4.52 x 0.28	222.9 (20.	8) 208.3	(19.8)	2475	(1123)	35/55	4"-174"	4085	4085	/385
280x300	Multi/Bk	15'1" x 16'2" x 11"	4.6 x 4.91 x 0.28	242.5 (22.	$\frac{0}{22/.2}$	(21.6)	2695	(1223)	35/60	4"-1/4"	4480	4480	8080
280x325	IVIUITI/BK	15'1" x 1/'5" x 11"	4.0 X 3.31 X U.28	202.0 (24.	4) <u>240.1</u>	(23.4)	2910	(1320)	35/05	4"-1/4"	4/8U	4/8U	0200
280-275	Multi/BK	15'1 × 10 9'' × 11''	$4.0 \times 3.7 \times 0.28$	301.2 (20.	203.U	12701	3130	(1420)	35/70	4 -1/4"	5575	5575	7300
280×100	Multi/RL	15'1" x 21'4" x 11"	$4.0 \times 0.1 \times 0.20$	320.8 (20)	204.0	128 81	3565	(1618)	35/80	4"-174	5875	5875	10675
280x400	Multi/Bk	15'1" x 22'8" x 11"	4.6 x 6.89 x 0.28	340.4 (31 3	7) 321.8	(30.6)	3780	(1715)	35/85	4"-174"	6270	6270	11370
280x450	Multi/Bk	15'1" x 23'11" x 11"	4.6 x 7.29 x 0.28	359.9 (33.	5) 340.8	(32.4)	4000	(1815)	35/90	4''-174''	6665	6665	12065
280x475	Multi/Bk	15'1" x 25'3" x 11"	4.6 x 7.69 x 0.28	379.5 (35.	4) 359.7	(34.2)	4215	(1912)	35/95	4''-174''	6965	6965	12665
280x500	Multi/Bk	15'1" x 26'6" x 11"	4.6 x 8.08 x 0.28	399.1 (37.2	2) 378.6	(36.0)	4430	(2010)	35/100	4''-174''	7360	7360	13360
280x525	Multi/Bk	15'1" x 27'10" x 11"	4.6 x 8.48 x 0.28	418.7 (39.0	397.5	(37.8)	4650	(2110)	35/105	4''-174''	7760	7760	14060

Lines x Columns	Sections/ Ventilated	Cabinet Dimensions Feet-Inches H x W x D	Cabinet Dimensions Meters H x W x D	Cabinet Square Feet (Square Meters)	Active Area Square Feet (Square Meters)	Cabinet Weight Pounds (kilograms)	Lines/ Characters per line	Character Height	Maximum Watts Amber Red RGB
280x550	Multi/Bk	15'1" x 29'2" x 11"	4.6 x 8.87 x 0.28	438.2 (40.8)	416.5 (39.6)	4865 (2207)	35/110	4''-174''	8060 8060 14660
280x575	Multi/Bk	15'1'' x 30'5'' x 11''	4.6 x 9.27 x 0.28	457.8 (42.6)	435.4 (41.4)	5085 (2307)	35/115	4''-174''	8470 8470 15370
280x600	Multi/Bk	15'1" x 31'9" x 11"	4.6 x 9.67 x 0.28	477.4 (44.5)	454.3 (43.2)	5300 (2405)	35/120	4''-174''	8870 8870 16070
280x625	Multi/Bk	15'1" x 33'0" x 11"	4.6 x 10.06 x 0.28	497.0 (46.3)	473.2 (45.0)	5520 (2504)	35/125	4''-174''	9170 9170 16670
280x650	Multi/Bk	15'1" x 34'4" x 11"	4.6 x 10.46 x 0.28	516.6 (48.1)	492.2 (46.8)	5735 (2602)	35/130	4''-174''	9565 9565 17365
280x675	Multi/Bk	15'1" x 35'8" x 11"	4.6 x 10.86 x 0.28	536.1 (50.0)	511.1 (48.2)	5955 (2702)	35/135	4''-174''	9960 9960 18060
280x700	Multi/Bk	15'1" x 36'11" x 11"	4.6 x 11.25 x 0.28	555.7 (51.8)	530.0 (50.0)	6170 (2799)	35/140	4''-174''	10260 10260 18660
280x725	Multi/Bk	15'1" x 38'3" x 11"	4.6 x 11.65 x 0.28	575.3 (53.6)	549.0 (51.8)	6390 (2899)	35/145	4"-174"	10655 10655 19355
280x/50	Multi/Bk	15'1" x 39'0" x 11"	4.6 x 12.04 x 0.28	594.9 (55.4)	507.9 (53.0)	6605 (2996)	35/150	4"-1/4"	11050 11050 20050
200x//5	Multi/Bk	151 X 4010 X 11	4.0 x 12.44 x 0.20	634.0 (50.1)	<u> </u>	7040 (3194)	35/155	4'-174''	11750 11750 20030
280x825	Multi/Bk	15'1" x 43'5" x 11"	4.0 x 12.04 x 0.20	653.6 (60.9)	624 7 (59.0)	7255 (3291)	35/165	4 -174	12145 12145 22045
300×100	Multi/Bk	16'2'' x 5'9'' x 11''	4.91 x 1.74 x 0.28	91.8 (8.5)	81.2 (7.7)	1020 (463)	37/20	4"-187"	1590 1590 2880
300x125	Multi/Bk	16'2'' x 7'0'' x 11''	4.91 x 2.14 x 0.28	112.7 (10.5)	101.4 (9.6)	1255 (570)	37/25	4''-187''	2010 2010 3615
300x150	Multi/Bk	16'2'' x 8'4'' x 11''	4.91 x 2.53 x 0.28	133.6 (12.4)	121.7 (11.5)	1485 (674)	37/30	4''-187''	2425 2425 4355
300×175	Multi/Bk	16'2'' x 9'8'' x 11''	4.91 x 2.93 x 0.28	154.6 (14.4)	142.0 (13.4)	1720 (781)	37/35	4''-187''	2750 2750 5000
300x200	Multi/Bk	16'2" x 10'11" x 11"	4.91 x 3.33 x 0.28	175.5 (16.4)	162.3 (15.4)	1950 (885)	37/40	4''-187''	3165 3165 5735
300×225	Multi/Bk	16'2'' x 12'3'' x 11''	4.91 x 3.72 x 0.28	196.4 (18.3)	182.6 (17.3)	2185 (992)	37/45	4''-187''	3585 3585 6475
300x250	Multi/Bk	16'2'' x 13'6'' x 11''	4.91 x 4.12 x 0.28	217.4 (20.2)	202.8 (19.2)	2415 (1096)	37/50	4''-187''	3905 3905 7120
<u>300x275</u>	Multi/Bk	16'2" x 14'10" x 11"	4.91 x 4.52 x 0.28	238.3 (22.2)	223.1 (21.1)	2645 (1200)	37/55	4"-187"	4320 4320 7860
<u>300x300</u>	Multi/Bk	16'2'' x 16'2'' x 11''	4.91 x 4.91 x 0.28	259.2 (24.1)	243.4 (23.0)	2880 (130/)	3//60	4"-18/"	4/40 4/40 8595
300x325	Multi/Bk	16'2'' X 17'3'' X 11''	4.91 x 5.31 x 0.28	280.1 (20.1)	263.7 (25.0)	3110 (1411)	37/00	4"-18/"	5490 5490 9240
300x330	Multi/Bk	16'2'' × 20'0'' × 11''	4.91 x 5.7 x 0.28	322 0 (30 0)	204.0 (20.7)	3575 (1622)	37/75	4 -107	5805 5805 10715
300x373	Multi/Bk	16'2'' x 21'/'' x 11''	4.91 x 6 5 x 0.28	3/29 (31.9)	324 5 (30.7)	3810 (1729)	37/80	4 -107	6215 6215 11360
300×425	Multi/Bk	16'2'' x 22'8'' x 11''	4 91 x 6 89 x 0 28	363.9 (33.8)	344.8 (32.6)	4040 (1833)	37/85	4"-187"	6635 6635 12100
300x450	Multi/Bk	16'2'' x 23'11'' x 11''	4.91 x 7.29 x 0.28	384.8 (35.8)	365.1 (34.6)	4275 (1940)	37/90	4"-187"	7050 7050 12840
300x475	Multi/Bk	16'2'' x 25'3'' x 11''	4.91 x 7.69 x 0.28	405.7 (37.8)	385.4 (36.5)	4505 (2044)	37/95	4''-187''	7375 7375 13480
300x500	Multi/Bk	16'2'' x 26'6'' x 11''	4.91 x 8.08 x 0.28	426.7 (39.7)	405.6 (38.4)	4740 (2151)	37/100	4''-187''	7790 7790 14220
300x525	Multi/Bk	16'2'' x 27'10'' x 11''	4.91 x 8.48 x 0.28	447.6 (41.6)	425.9 (40.3)	4970 (2255)	37/105	4''-187''	8210 8210 14960
<u>300x550</u>	Multi/Bk	16'2'' x 29'2'' x 11''	4.91 x 8.87 x 0.28	468.5 (43.6)	446.2 (42.2)	5205 (2361)	37/110	4''-187''	8530 8530 15600
300x575	Multi/Bk	16'2" x 30'5" x 11"	4.91 x 9.27 x 0.28	489.4 (45.5)	466.5 (44.2)	5435 (2466)	37/115	4''-187''	8965 8965 16355
<u>300x600</u>	Multi/Bk	16'2" x 31'9" x 11"	4.91 x 9.67 x 0.28	510.4 (47.5)	486.8 (46.1)	5670 (2572)	37/120	4"-187"	9380 9380 17095
300x625	Multi/Bk	16'2'' x 33'0'' x 11''	4.91 x 10.06 x 0.28	531.3 (49.4)	507.0 (48.0)	5900 (26/7)	37/125	4"-18/"	9/05 9/05 1//40
300x630 300x675	Aulti /BL	16'2" x 34'4" x 11	4.91 x 10.40 x 0.28	573.2 (51.4)	5476 (51 4)	6365 (2261)	37/130	4'-10/	10120 10120 10460
300x0/3	Multi/Bk	16'2'' x 36'11'' x 11''	4.91 x 11 25 x 0.28	594 1 (55 2)	5679 (53.3)	6595 (2000)	37/140	4''-187''	103401034019213
300x725	Multi/Bk	16'2" x 38'3" x 11"	4.91 x 11.65 x 0.28	615.0 (57.2)	588.2 (55.2)	6830 (3099)	37/145	4"-187"	11275 11275 20600
300x750	Multi/Bk	16'2'' x 39'6'' x 11''	4.91 x 12.04 x 0.28	636.0 (59.1)	608.4 (57.1)	7060 (3203)	37/150	4"-187"	11695 11695 21335
300x775	Multi/Bk	16'2" x 40'10" x 11"	4.91 x 12.44 x 0.28	656.9 (61.1)	628.7 (59.0)	7295 (3309)	37/155	4''-187''	12015 12015 21980
300x800	Multi/Bk	16'2" x 42'2" x 11"	4.91 x 12.84 x 0.28	677.8 (63.0)	649.0 (61.0)	7525 (3414)	37/160	4''-187''	12435 12435 22720
300x825	Multi/Bk	16'2'' x 43'5'' x 11''	4.91 x 13.23 x 0.28	698.7 (65.0)	669.3 (62.9)	7760 (3520)	37/165	4''-187''	12850 12850 23460
320x100	Multi/Bk	17'2'' x 5'9'' x 11''	5.23 x 1.74 x 0.28	97.7 (9.1)	86.6 (8.2)	1085 (493)	40/20	4"-199"	1680 1680 3050
320x125	Multi/Bk	17'2" x 7'0" x 11"	5.23 x 2.14 x 0.28	120.0 (11.2)	108.2 (10.2)	1335 (606)	40/25	4"-199"	2120 2120 3830
320x150	Multi/Bk	17'2'' x 8'4'' x 11''	5.23 x 2.53 x 0.28	142.3 (13.2)	129.8 (12.2)	1580 (/1/)	40/30	4"-199"	2000 2000 5200
320x1/3	Multi/Bk	17 2 X 7 0 X 11	5.23 x 2.93 x 0.28	186.8 (17.4)	173 1 (16.3)	2075 (042)	40/33	4 -199	3340 3340 6080
320x220	Multi/Bk	17'2'' x 12'3'' x 11''	5 23 x 3 72 x 0 28	2091 (19.5)	194 7 (18.4)	2325 (1055)	40/40	4"-199"	3775 3775 6860
320x250	Multi/Bk	17'2'' x 13'6'' x 11''	5.23 x 4.12 x 0.28	231.4 (21.5)	216.4 (20.4)	2570 (1166)	40/50	4"-199"	4120 4120 7550
320x275	Multi/Bk	17'2" x 14'10" x 11"	5.23 x 4.52 x 0.28	253.7 (23.6)	238.0 (22.4)	2820 (1280)	40/55	4''-199''	4560 4560 8330
320x300	Multi/Bk	17'2" x 16'2" x 11"	5.23 x 4.91 x 0.28	276.0 (25.7)	259.6 (24.5)	3065 (1391)	40/60	4''-199''	5000 5000 9110
320x325	Multi/Bk	17'2'' x 17'5'' x 11''	5.23 x 5.31 x 0.28	298.2 (27.8)	281.3 (26.5)	3315 (1504)	40/65	4''-199''	5340 5340 9800
320x350	Multi/Bk	17'2" x 18'9" x 11"	5.23 x 5.7 x 0.28	320.5 (29.8)	302.9 (28.6)	3560 (1615)	40/70	4''-199''	5780 5780 10580
320x375	Multi/Bk	17'2" x 20'0" x 11"	5.23 x 6.1 x 0.28	342.8 (31.9)	324.5 (30.6)	3810 (1729)	40/75	4''-199''	6220 6220 11360
320x400	Multi/Bk	1/'2" x 21'4" x 11"	5.23 x 6.5 x 0.28	365.1 (34.0)	346.2 (32.6)	4055 (1840)	40/80	4"-199"	6560 6560 12045
320x425	Multi/Bk	1/'2'' x 22'8'' x 11''	5.23 x 6.89 x 0.28	38/.4 (36.0)	36/.8 (34./)	4300 (1951)	40/85	4"-199"	7000 7000 12830
320x450	/VIUIti/Bk	17'2'' x 23'11'' x 11''	5.23 x 7.29 x 0.28	409.0 (38.1)	307.4 (30./)	4550 (2064)	40/90	4"-199"	7440 7440 13610
320x4/3	Multi/BK	17 2 X 23'3'' X 11''	5.23 × 8.08 × 0.28	451.9 (40.2)	411.1 (38.8) 132 7 110 91	4/95 (21/5) 50/15 (2280)	40/93	4 -199"	8220 8220 15090
320x500	Multi /RL	17'2'' x 27'10'' x 11''	5 23 x 8 48 v 0 28	476.5 (41.1)	454.3 (42.8)	5290 (2400)	40/105	4"_199"	8660 8660 15860
320x550	Multi/Bk	17'2'' x 29'2'' x 11''	5.23 x 8.87 x 0.28	498.8 (46.4)	476.0 (44.9)	5540 (2513)	40/110	4"-199"	9000 9000 16545
320x575	Multi/Bk	17'2'' x 30'5'' x 11''	5.23 x 9.27 x 0.28	521.1 (48.5)	497.6 (46.9)	5785 (2625)	40/115	4''-199''	9460 9460 17340
320x600	Multi/Bk	17'2" x 31'9" x 11"	5.23 x 9.67 x 0.28	543.3 (50.6)	519.2 (49.0)	6035 (2738)	40/120	4''-199''	9895 9895 18125
320x625	Multi/Bk	17'2'' x 33'0'' x 11''	5.23 x 10.06 x 0.28	565.6 (52.6)	540.8 (51.0)	6280 (2849)	40/125	4''-199''	10240 10240 18810
320x650	Multi/Bk	17'2'' x 34'4'' x 11''	5.23 x 10.46 x 0.28	587.9 (54.7)	562.5 (53.0)	6530 (2962)	40/130	4''-199''	10680 10680 19590
320x675	Multi/Bk	17'2'' x 35'8'' x 11''	5.23 x 10.86 x 0.28	610.2 (56.8)	584.1 (54.6)	6775 (3074)	40/135	4"-199"	11115 11115 20375
320x700	Multi/Bk	1/'2'' x 36'11'' x 11''	5.23 x 11.25 x 0.28	032.5 (58.8)	605./ (56.6)	7025 (3187)	40/140	4"-199"	11460 11460 21060

Lines x Columns	Sections/ Ventilated	Cabinet Dimensions Feet-Inches H x W x D	Cabinet Dimensions Meters H x W x D	Cabinet Square Feet (Square Meters)	Active Area Square Feet (Square Meters)	Cabinet Weight Pounds (kilograms)	Lines/ Characters per line	Character Height	Maximum Watts Amber Red RGB
320x725	Multi/Bk	17'2" x 38'3" x 11"	5.23 x 11.65 x 0.28	654.7 (60.9)	627.4 (58.7)	7270 (3298)	40/145	4''-199''	11900 11900 21840
320x750	Multi/Bk	17'2'' x 39'6'' x 11''	5.23 x 12.04 x 0.28	677.0 (63.0)	649.0 (60.7)	7515 (3409)	40/150	4''-199''	12340 12340 22620
320x775	Multi/Bk	17'2" x 40'10" x 11"	5.23 x 12.44 x 0.28	699.3 (65.1)	670.6 (62.7)	7765 (3523)	40/155	4"-199"	12680 12680 23310
320x800	Multi/Bk	17'2'' x 42'2'' x 11''	5.23 x 12.84 x 0.28	712.0 (67.2)	692.3 (64.8)	8010 (3634)	40/160	4"-199"	13120 13120 24090
3/0x100	Multi/Bk	17.2 × 43.5 × 11"	$5.23 \times 13.23 \times 0.26$ 5.55 x 1.74 x 0.28	103.6 (97)	92.0 (8.6)	1155 (524)	40/103	4 –199 /''_212''	1765 1765 3220
340x125	Multi/Bk	18'3'' x 7'0'' x 11''	5.55 x 2.14 x 0.28	127.3 (11.9)	115.0 (10.8)	1415 (642)	42/25	4"-212"	2225 2225 4045
340x150	Multi/Bk	18'3'' x 8'4'' x 11''	5.55 x 2.53 x 0.28	150.9 (14.0)	138.0 (13.0)	1675 (760)	42/30	4''-212''	2685 2685 4870
340x175	Multi/Bk	18'3" x 9'8" x 11"	5.55 x 2.93 x 0.28	174.5 (16.3)	160.9 (15.1)	1940 (880)	42/35	4''-212''	3050 3050 5600
340x200	Multi/Bk	18'3" x 10'11" x 11"	5.55 x 3.33 x 0.28	198.2 (18.5)	183.9 (17.3)	2200 (998)	42/40	4"-212"	3510 3510 6425
340x225	Multi/Bk	18'3" x 12'3" x 11"	5.55 x 3.72 x 0.28	221.8 (20.6)	206.9 (19.4)	2465 (1119)	42/45	4"-212"	3970 3970 7250
$\frac{340 \times 250}{340 \times 275}$	Multi/Bk	18'3'' × 1/'10'' × 11''	$5.55 \times 4.12 \times 0.28$	243.4 (22.9)	229.9 (21.0)	2723 (1237)	42/50	4"-212"	4335 4335 7975
340x300	Multi/Bk	18'3" x 16'2" x 11"	5.55 x 4.91 x 0.28	292.7 (27.3)	275.9 (25.9)	3250 (1475)	42/60	4"-212"	5255 5255 9625
340x325	Multi/Bk	18'3'' x 17'5'' x 11''	5.55 x 5.31 x 0.28	316.3 (29.5)	298.8 (28.1)	3515 (1595)	42/65	4"-212"	5620 5620 10355
340x350	Multi/Bk	18'3'' x 18'9'' x 11''	5.55 x 5.7 x 0.28	340.0 (31.6)	321.8 (30.2)	3775 (1713)	42/70	4''-212''	6080 6080 11180
340x375	Multi/Bk	18'3" x 20'0" x 11"	5.55 x 6.1 x 0.28	363.6 (33.9)	344.8 (32.4)	4040 (1833)	42/75	4''-212''	6540 6540 12005
340x400	Multi/Bk	18'3'' x 21'4'' x 11''	5.55 x 6.5 x 0.28	387.2 (36.1)	367.8 (34.6)	4300 (1951)	42/80	4"-212"	6905 6905 12730
340x425	Multi/Bk	18'3'' x 22'8'' x 11''	5.55 x 6.89 x 0.28	410.9 (38.2)	390.8 (36.7)	4565 (20/1)	42/85	4"-212"	/365 /365 13555
$\frac{340\times450}{340\times475}$	Multi/BK	18'3'' x 23'11'' X 11''	5.55 x 7.29 x 0.28	434.5 (40.5)	413.8 (38.9)	4823 (2189)	42/90	4"-212"	8100 8100 15110
340x500	Multi/Bk	18'3'' x 26'6'' x 11''	5.55 x 8.08 x 0.28	481.8 (44.8)	459.7 (43.2)	5350 (2427)	42/100	4"-212"	8650 8650 15935
340x525	Multi/Bk	18'3" x 27'10" x 11"	5.55 x 8.48 x 0.28	505.4 (47.1)	482.7 (45.4)	5610 (2545)	42/105	4''-212''	9110 9110 16760
340x550	Multi/Bk	18'3'' x 29'2'' x 11''	5.55 x 8.87 x 0.28	529.0 (49.2)	505.7 (47.5)	5875 (2665)	42/110	4''-212''	9475 9475 17485
340x575	Multi/Bk	18'3'' x 30'5'' x 11''	5.55 x 9.27 x 0.28	552.7 (51.4)	528.7 (49.7)	6135 (2783)	42/115	4''-212''	9950 9950 18330
340x600	Multi/Bk	18'3'' x 31'9'' x 11''	5.55 x 9.67 x 0.28	576.3 (53.7)	551.7 (51.8)	6400 (2903)	42/120	4"-212"	10410 10410 19155
340x625	Multi/Bk	18'3'' x 33'0'' x 11''	5.55 x 10.06 x 0.28	599.9 (55.8)	5/4.6 (54.0)	6660 (3021)	42/125	4"-212"	10//5 10//5 19880
340x030 340x675	Multi/Bk	18'3'' x 35'8'' x 11''	$5.55 \times 10.46 \times 0.28$	6472 (60.3)	620.6 (57.8)	7185 (3260)	42/130	4"-212"	11235 11235 20705
340x700	Multi/Bk	18'3'' x 36'11'' x 11''	5.55 × 11.25 × 0.28	670.8 (62.4)	643 6 (59.9)	7450 (3380)	42/100	4''-212''	12060 12060 22260
340x725	Multi/Bk	18'3'' x 38'3'' x 11''	5.55 x 11.65 x 0.28	694.5 (64.7)	666.6 (62.1)	7710 (3498)	42/145	4''-212''	12520 12520 23085
340x750	Multi/Bk	18'3" x 39'6" x 11"	5.55 x 12.04 x 0.28	718.1 (66.8)	689.6 (64.3)	7975 (3618)	42/150	4''-212''	12980 12980 23910
340x775	Multi/Bk	18'3'' x 40'10'' x 11''	5.55 x 12.44 x 0.28	741.7 (69.0)	712.6 (66.4)	8235 (3736)	42/155	4''-212''	13345 13345 24635
340x800	Multi/Bk	18'3'' x 42'2'' x 11''	5.55 x 12.84 x 0.28	765.4 (71.3)	735.5 (68.6)	8500 (3856)	42/160	4"-212"	13805 13805 25460
340x825	Multi/Bk	18'3'' x 43'5'' x 11''	5.55 x 13.23 x 0.28	/89.0 (/3.4)	/58.5 (/0./)	8/60 (39/4)	42/165	4"-212"	14265 14265 26285
360x100	Multi/Bk	19'3" x 7'0" x 11"	5.86 x 2.14 x 0.28	134 5 (12 5)	121 7 (11.6)	1495 (679)	45/20	<u>4 -224</u> <u>4''_224''</u>	2330 2330 4260
360x150	Multi/Bk	19'3" x 8'4" x 11"	5.86 x 2.53 x 0.28	159.5 (14.8)	146.1 (13.9)	1775 (806)	45/30	4"-224"	2815 2815 5130
360x175	Multi/Bk	19'3'' x 9'8'' x 11''	5.86 x 2.93 x 0.28	184.5 (17.2)	170.4 (16.2)	2050 (930)	45/35	4''-224''	3200 3200 5900
360x200	Multi/Bk	19'3" x 10'11" x 11"	5.86 x 3.33 x 0.28	209.5 (19.5)	194.7 (18.6)	2330 (1057)	45/40	4''-224''	3680 3680 6765
360x225	Multi/Bk	19'3'' x 12'3'' x 11''	5.86 x 3.72 x 0.28	234.5 (21.8)	219.1 (20.9)	2605 (1182)	45/45	4''-224''	4160 4160 7635
360x250	Multi/Bk	<u>19'3'' x 13'6'' x 11''</u>	5.86 x 4.12 x 0.28	259.5 (24.1)	243.4 (23.2)	2885 (1309)	45/50	4"-224"	4550 4550 8405
360x2/5	Multi/Bk	19'3'' x 14'10'' x 11''	5.86 x 4.52 x 0.28	284.5 (20.5)	207.7 (25.5)	3100 (1434)	45/55	4"-224"	5510 5510 10140
360x325	Multi/Bk	19'3'' x 17'5'' x 11''	5 86 x 5 31 x 0 28	334 4 (31 1)	316 4 (30 2)	3715 (1686)	45/65	4 -224	5900 5900 10910
360x350	Multi/Bk	19'3" x 18'9" x 11"	5.86 x 5.7 x 0.28	359.4 (33.4)	340.8 (32.5)	3990 (1810)	45/70	4"-224"	6380 6380 11780
360x375	Multi/Bk	19'3" x 20'0" x 11"	5.86 x 6.1 x 0.28	384.4 (35.7)	365.1 (34.8)	4270 (1937)	45/75	4''-224''	6860 6860 12645
360x400	Multi/Bk	19'3'' x 21'4'' x 11''	5.86 x 6.5 x 0.28	409.4 (38.1)	389.4 (37.1)	4545 (2062)	45/80	4''-224''	7245 7245 13420
360x425	Multi/Bk	19'3" x 22'8" x 11"	5.86 x 6.89 x 0.28	434.4 (40.4)	413.8 (39.4)	4825 (2189)	45/85	4''-224''	7730 7730 14285
$\frac{360 \times 450}{260}$	Multi/Bk	19'3" x 23'11" x 11"	5.86 x 7.29 x 0.28	459.4 (42.7)	438.1 (41.8)	5100 (2314)	45/90	4"-224"	8210 8210 15150
360x4/5	Multi/Bk	19'3'' x 25'3'' x 11''	5.86 x 7.09 x 0.28	484.3 (45.1)	402.4 (44.1)	5455 (25441)	45/95	4"-224"	8393 8393 13923
360x500	Multi/Bk	19'3'' x 27'10'' x 11''	5 86 x 8 48 x 0 28	534 3 (49.7)	511 1 (48.7)	5935 (2693)	45/105	4 -224	9560 9560 17660
360x550	Multi/Bk	19'3" x 29'2" x 11"	5.86 x 8.87 x 0.28	559.3 (52.0)	535.4 (51.0)	6210 (2817)	45/110	4"-224"	9945 9945 18430
360x575	Multi/Bk	19'3" x 30'5" x 11"	5.86 x 9.27 x 0.28	584.3 (54.3)	559.8 (53.4)	6490 (2944)	45/115	4''-224''	104401044019315
360x600	Multi/Bk	19'3" x 31'9" x 11"	5.86 x 9.67 x 0.28	609.3 (56.7)	584.1 (55.7)	6765 (3069)	45/120	4''-224''	10925 10925 20180
360x625	Multi/Bk	19'3'' x 33'0'' x 11''	5.86 x 10.06 x 0.28	634.3 (59.0)	608.4 (58.0)	7045 (3196)	45/125	4''-224''	11310 11310 20955
360x650	Multi/Bk	19'3" x 34'4" x 11"	5.86 x 10.46 x 0.28	659.2 (61.3)	632.8 (60.3)	7320 (3321)	45/130	4"-224"	11790 11790 21820
300x6/5	Multi/Bk	19'3'' x 35'8'' x 11''	5.86 x 11.25 x 0.28	084.2 (63.6)	03/.1 (62.1)	7575 (3446)	45/135	4"-224"	122/5 122/5 22690
360x700	Multi/Rk	19'3'' x 38'3'' v 11''	$5.86 \times 11.25 \times 0.28$	734.2 (68.3)	70.5 8 (66 7)	8150 (3697)	45/140	4 -224"	13140 13140 2/325
360x750	Multi/Bk	19'3'' x 39'6'' x 11''	5.86 x 12.04 x 0.28	759.2 (70.6)	730.1 (69.0)	8430 (3824)	45/150	4''-224''	13620 13620 25195
360x775	Multi/Bk	19'3'' x 40'10'' x 11''	5.86 x 12.44 x 0.28	784.2 (72.9)	754.5 (71.3)	8705 (3949)	45/155	4''-224''	14005 14005 25965
360x800	Multi/Bk	19'3'' x 42'2'' x 11''	5.86 x 12.84 x 0.28	809.2 (75.2)	778.8 (73.7)	8985 (4076)	45/160	4''-224''	14490 14490 26835
360x825	Multi/Bk	19'3'' x 43'5'' x 11''	5.86 x 13.23 x 0.28	834.1 (77.5)	803.1 (76.0)	9260 (4201)	45/165	4''-224''	14970 14970 27700



#	DETAIL DESCRIPTION										
1	DISPLAY	GS6 - AAA	AxBBB-CC (SE	E CHART ON TOP	'LEFT)						
2	LED COLOR	RED, AME	BER, OR RGB								
3	ACTIVE AREA	2' 15/16"	[634] X 7' 9-5/8	3" [2377]							
4	OVERALL SIZE	2' 6-15/16"	' [786] X 8' 5/8	3" [2454]							
5	CABINET	ALUMINU	M & STEEL								
6	VENTILATION	FRONT	-								
7	ACCESS	SERVICE	RVICE FROM FRONT OF DISPLAY								
8	WEIGHT	150 LBS [f	0 LBS [69 KG] (APPROX)								
9	SHIPPING	SHIPPED	AS A SINGLE	UNIT							
10	DIMENSIONS	FEET AND	D INCHES IMIL	LIMETERS1							
11	PAINTED	SEMI-GLC	DSS BLACK								
1	DESIGN WIND PRI										
2	STANDARD/COL	<u></u>	(0, (0) 1,)	IBC 2009/ASCE7	-05 IBC 2012/ASCE7-10						
3		S MUST B									
		ACE. FOR		CONT DIGI LA	מייה פווטאא						
	STER SINGLET				240VAC 1PH 50Hz						
			120VAC	TPH 50/60HZ FS + GND)	(2 WIRES + GND)						
CHNOLOGY	COLOR	MAX	DON	MESTIC							
		WAIIS		INF 1	LINE 1						
			(A	MPS)	(AMPS)						
	RED	434		3.62	1.81						
GS6	AMBER	434	:	3.62	1.81						
	RGB	670		5.59	2.79						
ENTILATION F	REQUIREMENTS										
	DISPLAY RE	LIES ON V	ENTILATION T	O FUNCTION PRO	OPERLY. INTAKES,						
1	LOCATED A	T THE FRO	NT OF THE DI	SPLAY, MUST BE	ABLE TO DRAW IN						
	AIR AT A TEMPERATURE NO GREATER THAN 120 F.										
2	IN ORDER TO ENSURE AMBIENT TEMPERATURE AIRFLOW IS MAINTAINED,										
۷	OF THE DISPLAY MAY BE COVERED OR OBSTRUCTED IN ANY WAY.										
	s										
	CABINET. THE	5 PRESERV	E BETWEEN 1	THE CABINET AND	D THE LIFTEYE MUST						
1	BE MAINTAINE	BE MAINTAINED - USING A SPREADER BEAM IS SUGGESTED. ALL EYEBOLTS									
	MUST BE USED WHEN LIFTING.										
2	1/2" LIFTEYES	TO ASSIST	F WITH DISPL	AY INSTALLATION	I. LIFTEYES MAY NOT						
	DE USED FUI			ATION. LIFTETES	WAT DE REMOVED.						
3	MECHANICAL	AND SIGN	AL CONNECTI	ONS OCCUR EXT	ERNAL TO DISPLAY.						
	CLIP ANGLE F	OR MOUNT	FING. CLIP AN	GLES CAN BE AD	JUSTED VERTICALLY						
4	1 - 3/16" AS NEE	DED DURI	NG INSTALLA	TION. CLIP ANGLE	E CAN BE WELDED OR						
			ER. ALL CLIP /								
5	T	HE INTEG	RITY OF THE I	MOUNTING STRU	CTURE.						
6	DAKTRO	NICS IS NO	OT RESPONSI	BLE FOR THE MA	IN ELECTRICAL						
0		DISCONN	IECT. SEE PO	WER RATINGS AE	BOVE.						
7	SEE DWC	3-03097	'583 FOR	SIGNAL &	MTG DETAILS						

-SEE INSTALL NOTE #7

	THE CONCEP ARE CONF	PTS EXPRESSED	THIRD ANGLE PROJECTIO					
DAKTR	DAKTR	ONICS, INC. OR I COPYRIGHT 20						
PROJECT: GALAXY GS6 SERIES								
TITLE:	SHOP DWG, GS	6-R, 2' 7"	x8' 1" (2x6 MODS)					
DATE:	14-AUG-17	DIM UNITS:	INCHES [MILLIME	ETERS]	SHEET	REV		
SCALE:	1/15	DO N	OT SCALE DRAW	ING	1 OF 1	04		
DESIGN:	TWHITEH	JOB NO	FUNC - TYPE - SIZE	2	1111	20		
DRAWN:	DOSTRAA	P1817	E - 07 - B	J		90		